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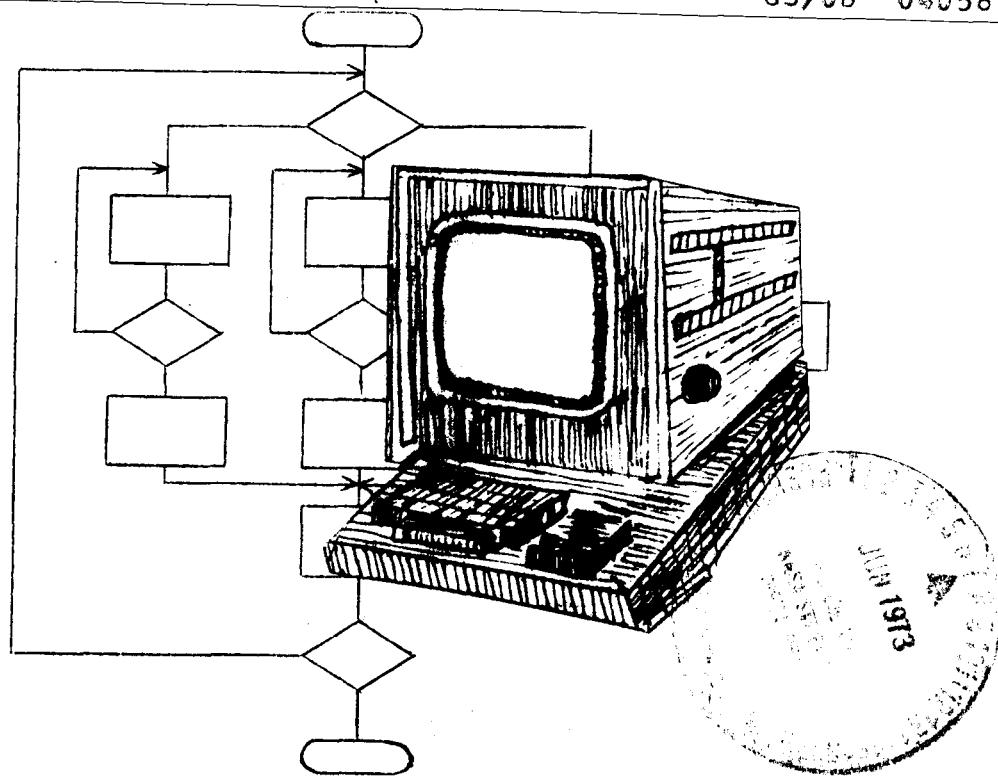
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DYNASOR II - A FINITE ELEMENT PROGRAM FOR THE
DYNAMIC NONLINEAR ANALYSIS OF SHELLS OF REVOLUTION

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USER MANUAL

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II

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APPENDIX J

SAMPLE DOCUMENTED PROGRAM

I

ABSTRACT

The DYNASOR II program is used for the DYnamic Nonlinear Analysis of Shells Of Revolution. The equations of motion of the shell are solved using Houbolt's numerical procedure. The displacements and stress resultants can be determined for both symmetrical and asymmetrical loading conditions. Asymmetrical dynamic buckling can be investigated. Solutions can be obtained for highly nonlinear problems utilizing as many as five of the harmonics generated by SAMMSOR program. A restart capability allows the user to restart the program at a specified time.

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System Overview

J-1.5

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SOR - Shell Of Revolution**Computer Programs**

A family of compatible computer codes for the analysis of the shell of revolution (SOR) structures has been developed by researchers at Texas A&M University. These analyses employ the matrix displacement method of structural analysis utilizing a curved shell element. Geometrically nonlinear static and dynamic analyses can be conducted using these codes. The important natural frequencies and mode shapes can also be determined by employing another of the codes. Efficient programming provides codes capable of performing these desired analyses in relatively small amounts of computer time.

Each of these programs has been extensively tested using problems the solutions to which have been reported by other researchers in order to establish the validity of the codes. In addition, the capabilities of the codes have been demonstrated in a number of publications by presenting solutions to problems which were unsolved by other researchers.

SAMMSOR II - Stiffness And Mass Matrices for Shells Of Revolution are generated utilizing the first member of this family. This program accepts a description of the structure in terms of the coordinates and slopes of the nodes and the properties of the elements joining the nodes. For shells with simple geometries (such as cylinders, shallow caps, hemispheres, etc.) the shell geometry can be internally generated. Utilizing the element properties, the structural stiffness and mass matrices are generated for as many as twenty harmonics and stored on magnetic tape. Each of the other SOR programs utilizes the output tape generated by SAMMSOR as input data for the respective analyses. One advantage of creating the stiffness and mass matrices in a separate program is that a variety of analyses can be performed on the same shell configuration without having to create the matrices more than once. Obviously, a variety of boundary and loading conditions can be employed without having to create new mass and stiffness matrices for each case.

SNASOR II - The Static Nonlinear analysis of Shells Of Revolution subjected to arbitrary mechanical and thermal loading is performed using the second computer code. Utilizing the stiffness matrices generated by SAMMSOR and the loading conditions and boundary conditions input to SNASOR II, the equilibrium equations for the structure are generated. The nonlinear strain energy terms result in pseudo generalized forces (as functions of the displacements) which are combined with the applied generalized forces. The resulting set of nonlinear algebraic equilibrium equations is solved by one of several methods: Newton-Raphson

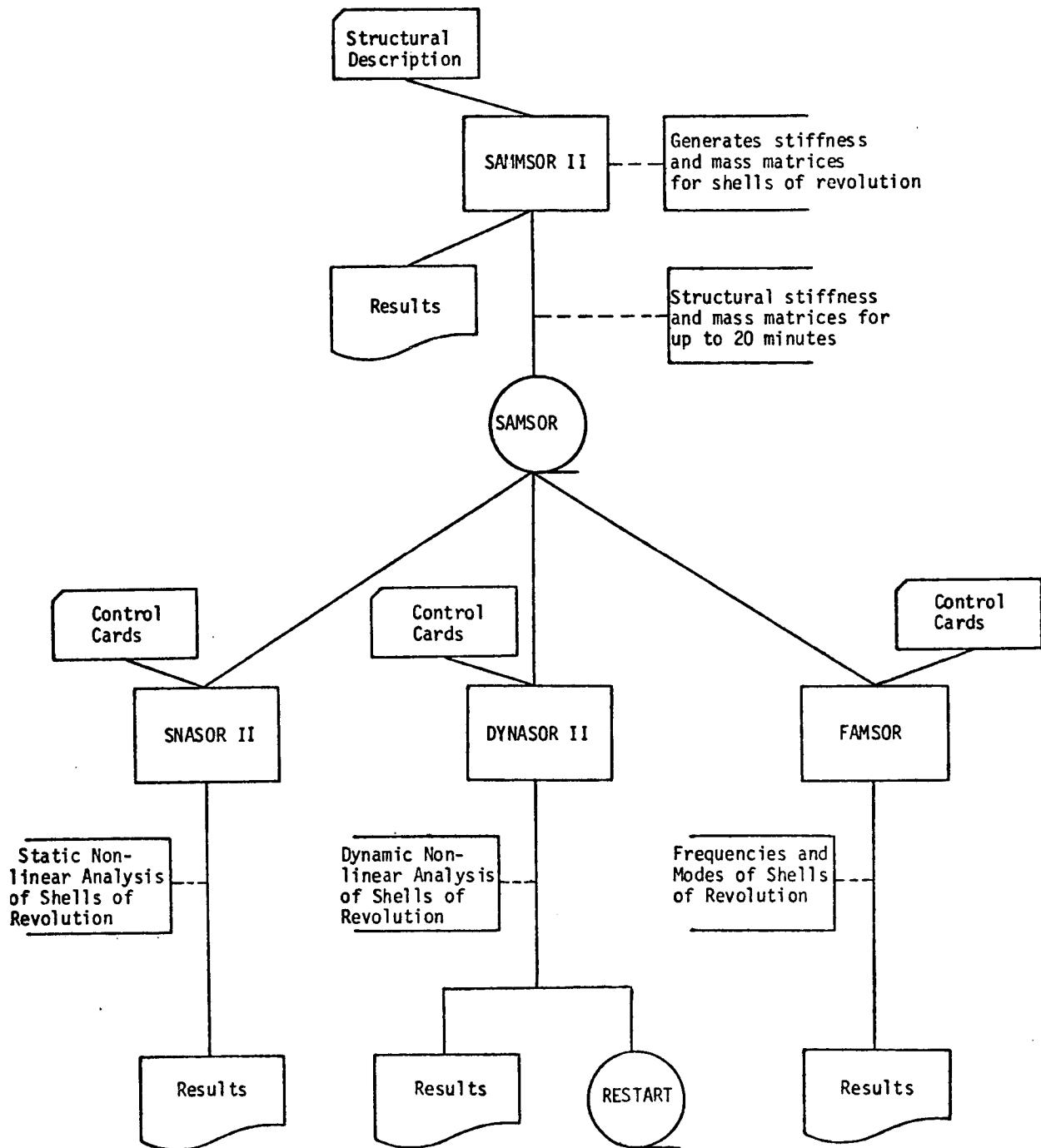
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type iteration, incremental stiffness method, or a modified incremental stiffness method. In general, the Newton-Raphson procedure is the best and yields accurate results for highly nonlinear problems.

DYNASOR II - The third code is used for the Dynamic Nonlinear Analysis of Shells Of Revolution. The equations of motion of the shell are solved using Houbolt's numerical procedure with the nonlinear terms being moved to the right-hand side of the equilibrium equations and again treated as generalized loads. The displacements and stress resultants can be determined for both symmetrical and asymmetrical loading conditions. Asymmetrical dynamic buckling can be investigated using this program. Solutions can be obtained for highly nonlinear problems in reasonable periods of time on the computer utilizing as many as five of the harmonics generated in SAMMSOR. A restart capability is incorporated in this code which allows the user to restart the program at a specified time without having to expend the computer time necessary to regenerate the prior response.

FAMSOR - Frequencies And Modes for Shells Of Revolution can be determined using the fourth code. Using the stiffness matrix generated by SAMMSOR and a lumped mass representation developed from the consistent mass matrix generated by SAMMSOR, a specified number of natural frequencies (beginning with the lowest or fundamental frequency) are obtained using the inverse iteration method. The mode shapes for each of the frequencies are also obtained.

SYSTEM FLOWCHART



ENVIRONMENT

The DYNASOR II program runs under OS/360 MFT or MVT and requires 220K of memory on an IBM S/360 computer. The system must also have a card reader, printer, 3 9-track tape drives and 2314 disk storage.

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INTRODUCTION

The DYNASOR II (Dynamic Nonlinear Analysis of Shells Of Revolution) code has been developed to determine the time varying response of shells of revolution to a variety of loading conditions. The code utilizes the stiffness and mass matrices created by the SANMSOR code for selected harmonics, generates generalized forces from a mechanical and thermal load history, and solves the resulting initial value problem. This report is a user's guide for the DYNASOR II code and is divided into four self-contained sections with an extended appendix.

The first section describes the method of analysis used to obtain the displacements, stresses, and stress resultants for the desired time increments. The formulation of the equations of motion is presented along with the numerical technique employed to obtain the solution these equations.

A section is then presented to enumerate the limitations of the code and to provide valuable guidelines to aid the user in performing the desired analyses. The limitations result partly from the procedures utilized in the method of analysis and partly from the storage capacity and programming procedures employed.

A description of the input data required by the DYNASOR II code is presented in the third section. Examples are provided in instances where the wording might, at first glance, appear to be unclear or insufficient. The limitations placed upon the input parameters are once again enumerated.

The final section contains selected example problems which are designed to illustrate the wide variety of input variations allowed by the code. A copy of the input data required for each of the cases is presented along with selected values of the output data. A thorough understanding of these example problems is mandatory if the user is to become adept at operating the code.

The extended appendix which follows the main report should prove to be extremely helpful if a thorough understanding of the program is desired. A description of the subroutines and the significant Fortran variables is supported by the presence of the subroutine call map and a flow chart of the basic operations of the code. The sections describing the restart capability and the specification of the loads should prove invaluable to users who desire to obtain optimum performance from the code. A discussion of the program output is then followed by a description of the changes necessary to modify the capacity of the code.

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SECTION I

METHOD OF ANALYSIS

Introduction

The purpose of this section is to provide theoretical documentation of the equations and procedures employed in the DYNASOR II code to perform the Dynamic Nonlinear Analysis of Shells Of Revolution. The matrix displacement method of a structural analysis is utilized. Since the documentation for the development of the stiffness and mass matrices has been adequately presented in the SAMMOSOR II user's manual,¹ this section will not attempt to duplicate the previous presentation. The dynamic equations of motion are derived and the numerical techniques utilized to effect the solution of these equations are discussed.

Equations of Motion

The matrix displacement method is an energy formulation and, consequently, the equations of equilibrium for the nonlinear dynamic response are obtained from Lagrange's equation:

$$\frac{d}{dt} \left(\frac{\partial T}{\partial q_i^n} \right) + \frac{\partial U}{\partial q_i^n} = Q_i^n \quad (1)$$

where

q_i^n = generalized degree of freedom i of harmonic n

T = kinetic energy

U = internal energy (2)

Q_i^n = generalized force for degree of freedom i of harmonic n

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Since the internal energy of a structure is a scalar quantity, the expression for this quantity may be separated into various parts. The formulation used in this analysis considers the internal energy as

$$U = U_L + U_{NL} - (U_L^t + U_{NL}^t) \quad (3)$$

where the superscript, t , denotes the inclusion of thermal effects and

U_L = strain energy based upon linear strain displacement relations

U_{NL} = strain energy due to the inclusion of nonlinear contributions in the strain displacement relations

By substituting Eq. 3 into Eq. 1 and taking the nonlinear strain energy terms to the right-hand side, the equations of motion for the nonlinear dynamic analysis of shells of revolution can be written in matrix form as

$$[M^n]\{q^n\} + [K^n]\{q^n\} = \{Q^n\} + \{Q_t^n\} - \left\{ \frac{\partial U_{NL}}{\partial q^n} \right\} + \left\{ \frac{\partial U_{NL}^t}{\partial q^n} \right\} \quad (4)$$

The column matrix, $\{Q_t^n\}$, of pseudo linear thermal loads is evaluated exactly from $\{\partial U_L^t / \partial q^n\}$. It should be noted that Eq. 4 is valid for any harmonic n with the coupling between the harmonics appearing on the right-hand side. In this formulation the nonlinear terms are treated as pseudo generalized forces which are applied to the structure. The obvious advantage of this formulation is that a tremendous savings in computer time can be realized since the stiffness matrix does not change as the displacements vary and must, therefore, be calculated only once. With most other formulations for geometric nonlinearities, the stiffness matrix must be updated at each time step.

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The DYNASOR II code utilizes the strain displacement equations given by Novozhilov² as restricted to shells of revolution with the additional assumption being made that the only important nonlinear contributions arise from rotations about the shell coordinate axes. The midsurface strain expressions can then be written as

$$\begin{aligned}\epsilon_s &= \hat{e}_s + \frac{1}{2} \hat{e}_{13}^2 \\ \epsilon_\theta &= \hat{e} + \frac{1}{2} \hat{e}_{23}^2 \\ \epsilon_{s\theta} &= \hat{e}_{s\theta} + \hat{e}_{13} \hat{e}_{23}\end{aligned}\tag{5}$$

The changes in curvature are those used in linear theory

$$\begin{aligned}x_s &= -\hat{e}_{13}/\partial s \\ x_\theta &= -(1/r)(\partial \hat{e}_{23}/\partial \theta) - (1/r)\sin\phi \hat{e}_{13} \\ x_{s\theta} &= -(1/r)(\partial \hat{e}_{13}/\partial \theta) + (\sin\phi/r)\hat{e}_{23} - \partial \hat{e}_{23}/\partial s\end{aligned}\tag{7}$$

Pseudo Nonlinear Forces

The nonlinear terms in this analysis are treated in the same way as the generalized forces due to external loading. The generalized forces due to the nonlinearities are evaluated for each element and are then combined at the nodes. A detailed presentation of the procedures utilized in calculating the nonlinear forces has been made in Ref. 3 with an overview of the same material being provided in Ref. 4.

The pseudo forces are obtained by retaining strain energy terms containing the rotations raised to the fourth power. The retention of the fourth order terms has been shown^s to be absolutely essential in cases where the nonlinear terms are substantial. The results presented in Ref. 6 for static shell analysis did not include the effects of the fourth order terms but results obtained after the incorporation of these terms revealed once again the necessity of retaining these contributions.

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The generalized forces due to nonlinearities are evaluated using linear displacement functions in the variables u , v , and w and employing strip integration over the length of the element. The integrals around the circumference are evaluated in closed form for the particular harmonics chosen. This procedure is simpler than the one employed in Ref. 6 and permits the nonlinear forces to be evaluated without the use of secondary storage on the computer. Detailed justification for this simplified procedure has been made in Ref. 3 so these arguments will not be enumerated again. It will suffice to note that due to the exact evaluation of the integrals in the circumferential direction, it is reasonable to expect rapid convergence as the number of harmonics is increased. Examples have shown (Ref. 3) that the use of the strip integration over the length of the element produces convergence quite rapidly as the number of elements is increased.

Thermal Terms

The temperature distribution and the temperature gradients in the normal direction for an element are expanded in a Fourier series in a manner similar to that used for the displacement functions. The temperatures and temperature gradients for an element are assumed constant over each element in the meridional direction with step variations allowed in the circumferential direction. In cases where the step variation in the circumferential direction is not considered accurate enough, the Fourier coefficients may be specified as input information.

The linear and nonlinear contributions are separated with the linear thermal loads for each harmonic being evaluated as

$$\{Q_t^n\} = \left\{ \frac{\partial U_L^t}{\partial q^n} \right\} \quad (8)$$

Employing a coordinate transformation to change to partial derivatives with respect to the generalized shell coordinates, the problem reduces to the evaluation of the partial derivatives of U_L^t with respect to the coefficients $\alpha_1, \alpha_2, \dots, \alpha_8$. These partial derivatives are presented in Eqs. 26 of Ref. 3, and the terms of $\{Q_t^n\}$ are listed in the appendix of the same report.

The nonlinear thermal loads are treated in essentially the same manner as the generalized forces due to nonlinearities are treated. Utilizing the same approximations as for the nonlinearities due to applied forces, the expression for the nonlinear thermal contribution is given by Eq. 28 of Ref. 3.

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Stress Resultants

In this code, the stress resultants are determined by the use of the assumed displacement functions and finite difference relations at the mid-point of each element.

For orthotropic shells the stress resultants may be written as

$$\begin{Bmatrix} N_s \\ N_\theta \\ N_{s\theta} \\ M_s \\ M_\theta \\ M_{s\theta} \end{Bmatrix} = \begin{bmatrix} C_1 & v_{s\theta}C_1 & 0 & 0 & 0 & 0 \\ v_{\theta s}C_2 & C_2 & 0 & 0 & 0 & 0 \\ 0 & 0 & G_1 & 0 & 0 & 0 \\ 0 & 0 & 0 & D_1 & v_{s\theta}D_1 & 0 \\ 0 & 0 & 0 & v_{\theta s}D_2 & D_2 & 0 \\ 0 & 0 & 0 & 0 & 0 & G_2 \end{bmatrix} \begin{Bmatrix} \epsilon_s \\ \epsilon_\theta \\ \epsilon_{s\theta} \\ x_s \\ x_\theta \\ x_{s\theta} \end{Bmatrix}$$

where

$$C_1 = E_s t / (1 - v_{s\theta} v_{\theta s})$$

$$C_2 = E_\theta t / (1 - v_{s\theta} v_{\theta s})$$

$$G_1 = Gt$$

$$G_2 = Gt^3 / 12 \quad (10)$$

$$D_1 = E_s t^3 / [12(1 - v_{s\theta} v_{\theta s})]$$

$$D_2 = E_\theta t^3 / [12(1 - v_{s\theta} v_{\theta s})]$$

The shear resultants are determined approximately from the equations

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of the undeformed shell as

$$\begin{aligned} Q_s &= \frac{1}{r} \left[\frac{\partial}{\partial s} (rM_s) + \frac{\partial M_{s\theta}}{\partial s} - M_\theta \sin\phi \right] \\ Q &= \frac{1}{r} \left[\frac{\partial}{\partial s} (rM_s) + \frac{\partial M_\theta}{\partial \theta} + M_s \theta \sin\phi \right] \end{aligned} \quad (11)$$

Numerical Solution of Equations of Motion

Since a closed-form solution of Eq. 4 is generally not available, a numerical method must be used to determine the solution to the equations of motion. A finite difference procedure developed by Houbolt (Ref. 7) has been selected for use in the DYNASOR II code.

The equations of motion, Eq. 4, can be reduced to a system of equations of the form

$$[M]\{\ddot{q}\} + [K]\{q\} = \{F(t,q)\} \quad (12)$$

The load matrix $\{F(t,q)\}$ is equivalent to the right-hand side of Eq. 4. The initial displacements and velocities of the nodes must be specified and can be written as

$$q_0 = \{q\}_0 \quad (13)$$

$$\dot{q}_0 = \{\dot{q}\}_0$$

Utilizing the Houbolt procedure, the accelerations of the nodes of the shell are approximated by a third-order backwards difference

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expression

$$\{\ddot{q}_{n+1}\} = \frac{1}{(\Delta t)^2} \{2q_{n+1} - 5q_n + 4q_{n-1} - q_{n-2}\} \quad (14)$$

Substitution of Eq. 14 into Eq. 12 yields the following expression which is utilized to solve for the displacements at the end of each time step, except the first one:

$$(2[M] + (\Delta t)^2[K])\{q_{n+1}\} = (\Delta t)^2\{F(t, q)\}_{n+1} \\ + [M]\{5q_n - 4q_{n-1} + q_{n-2}\} \quad (15)$$

To determine the displacements at the end of the first time step, the following equation is employed

$$(6[M] + (\Delta t)^2[K])\{q_1\} = (\Delta t)^2\{F(0, q_0)\} \\ + [M]\{2(\Delta t)^2\ddot{q}_0 + 6\Delta t\dot{q}_0 + 6q_0\} \quad (16)$$

It should be noted that the selection of the Houbolt procedure for inclusion in the code was made only after evaluating the advantages and disadvantages of a number of solution schemes (Ref. 8). The Houbolt procedure proved to be the only method capable of providing stable solutions for highly nonlinear problems while utilizing a reasonably large time increment. The significant observations made in Ref. 8 concerning Houbolt's procedure will now be presented.

It was found that double precision arithmetic is necessary if the code is utilized for highly nonlinear problems on an IBM 360/65 system (or comparable system). It is believed that if the DYNASOR II code is used on computers which have a longer word length than the 360/65 system (such as the CDC 6600) double precision arithmetic will not be necessary. Utilizing the Houbolt scheme, it has been shown that the solution converges as the number of elements is increased. Although the Houbolt procedure has been shown to be unconditionally stable for the linear problem, it has found that this is not the case with the nonlinear formulation. The damping inherent in the Houbolt procedure was noted in some instances, but the savings in computer time resulting

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from employing this procedure far outweighs this slight drawback. Solutions (without the damping) were obtained, in some instances, in one-eighth (1/8) the amount of time required by other procedures. In all cases which were run, stable, undamped solutions were obtained using larger time increments than could be used with the other methods.

Extrapolation of Forces

In order to employ Eq. 15, the loads at the end of the $(n+1)$ th time step must be known. These loads, because of the presence of the nonlinear terms, are a function of the displacements to be calculated and therefore cannot be evaluated exactly. The right-hand side of Eq. 12 is, therefore, evaluated using a first-order Taylor's series expanded about the n -th increment:

$$\{F(t,q)_{n+1}\} = \{F(t,q)_n\} + \frac{\partial}{\partial t} \{F(t,q)_n\} \Delta t + O(\Delta t)^2 \quad (17)$$

A second-order extrapolation process has been employed (Ref. 8), but the results indicated that the linear extrapolation procedure was more stable.

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SECTION II

USER GUIDELINES AND PROGRAM LIMITATIONS

Guidelines for the use of the DYNASOR II code along with the limitations placed upon the analysis are enumerated in this section. Some of these limitations are the result of the procedures used to program the equations while other limitations are inherent in the formulation of the equations. Since most of the limitations are minor in nature, the DYNASOR II code may be used to solve a wide variety of important shell dynamics problems.

The maximum number of elements which the program may use is fifty (50). The maximum number of harmonics which may be coupled for the analysis is five (5). It is believed that these limitations will not hinder the user in solving most problems. However, since undoubtedly some users will want to modify the program capacity, instructions for increasing or decreasing the allowable number of elements and/or harmonics are provided in appendix 8.

In all analyses using the DYNASOR II code, the zeroth (0) harmonic must be specified as one of the input harmonics.

The coefficients of thermal expansion are assumed to be constant in the two principal directions for any given element but may vary from element to element.

The number of nodal restraints must be less than or equal to the maximum number of degrees of freedom for each harmonic (204).

The displacements of the nodes may be calculated for as many as twenty (20) angles around the circumference of the shell element.

While the displacements are calculated at every time increment, it is necessary to calculate the stresses only at time steps where a printout of the stresses is desired. The stresses and stress resultants are calculated at the middle of the elements (s-direction) for up to twenty (20) angles in the circumferential direction. The angles at which the stresses are calculated are the same as those at which the displacements are determined. The stresses on both the inner and outer surfaces are determined.

The units used in the program must be consistent with those used in the SAMMOSR code. All calculations in the versions supplied to the users of the code are given inch-pounds-seconds units.

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The program accepts the mechanical and thermal load histories by accepting descriptions at discrete points in time. The difference between the times for which loads are specified must, in all cases, be greater than the value of the time increment used in solving the equations of motion. The load variation curve is approximated by assuming a linear variation of the generalized forces between the times at which the loads are specified. It may therefore be necessary to specify the loads and temperatures at a fairly large number of points in time if the loads vary rapidly with time.

If the loads and/or temperatures propagate in any direction (moving loads), it will also be necessary to specify the loads at a fairly large number of points in time.

Pressure loadings, temperatures, and temperature gradients are assumed to be constant over the meridional length of the element but may vary in the circumferential direction. The variation in the circumferential direction (except for shear loadings) must be symmetric about the meridian corresponding to $\theta = 0$ degrees. These loadings may be input either by specifying the values at a number of circumferential angles for each element or by specifying the values of the Fourier coefficients for each harmonic.

If the program is not being restarted, the loads and temperatures must be specified at time $t_1 = 0.0$. Times at which loads must be specified when restarting the program are noted in Appendix 8.

One of the most important considerations in any dynamic analysis is the selection of the time increment to be used in the analysis. Several criteria have been developed for use in selecting a time increment in analyses utilizing finite difference techniques. Most of these criteria require that the time increment be less than the time required for a signal to travel at the speed of sound from one difference point to the next. These criteria have been found (ref. 8) inadequate for use in this analysis. A "feel" for the selection of a time increment must be obtained by the user. To facilitate the development of this "feel" the time increments utilized in a number of problems have been carefully documented in Refs. 3 and 4. In addition, the input data for the example problems should prove helpful.

A restart capability is incorporated in the code to enable the user to calculate the response from a specified point in time without having to recalculate the response prior to this time. A most valuable use of this capability arises if, after evaluation of the results of a run, it is decided to extend the calculations to observe more cycles of response. If it is desired to employ a different time increment (either smaller or larger), the user should refer to the discussion in Appendix 5. Effective use of the restart capability can result in a substantial savings of computer time. In general, the information necessary for restarting the code should be placed on tape at least every 100-400 time

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increments to insure that the information will be available if it is deemed desirable to restart the program.

The pseudo loads due to the nonlinearities associated with the initial displacements are neglected when calculating the response at the end of the first time step. However, when restarting the code, the initial increment utilizes both the mechanical and pseudo forces.

An extended effort has been made to check all aspects of the code. Comparisons of the response obtained using DYNASOR II with the results obtained by other researchers are presented in Ref. 3 and 4. These comparisons firmly establish the validity of the code. Although the programming logic and the formulation have been thoroughly checked to insure the correctness of the code, the authors assume no responsibility for the results obtained using the code.

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SECTION III

PROGRAM INPUT

The DYNASOR II code has been written so that the code can be employed by researchers who are not familiar with the inner workings of the program. Utilizing the guidelines and adhering to the limitations presented in the previous section, it is believed that most users will find it relatively easy to employ the code.

The code is available in the FORTRAN IV language using double precision or single precision arithmetic. This double precision version requires a storage space of about 330K bytes on IBM 360/65 system while the single precision storage space is about 200K bytes. Efforts have been made to make this code compatible with a large number of computing systems. In particular, adaption of the code for use on a CDC 6600 computer requires only minor changes.

The input data for a run consists of one card I (card types will be explained on the following pages) followed by a complete set of data (cards II-X) for each case. The set of cards II-X is the input data required to generate the response of a shell for a given number of harmonics due to a particular loading. The cards comprising the data deck for both an initial run and a restart are schematically represented in Fig. 1. The cards specifying the Fourier harmonics, the initial conditions, and the boundary conditions are omitted from the input deck when using the restart mode. If more than one case is to be run, include a set of data for each of the cases. There is no limit on the number of cases which may be included in a run. A card must be placed at the end of the data for the final case.

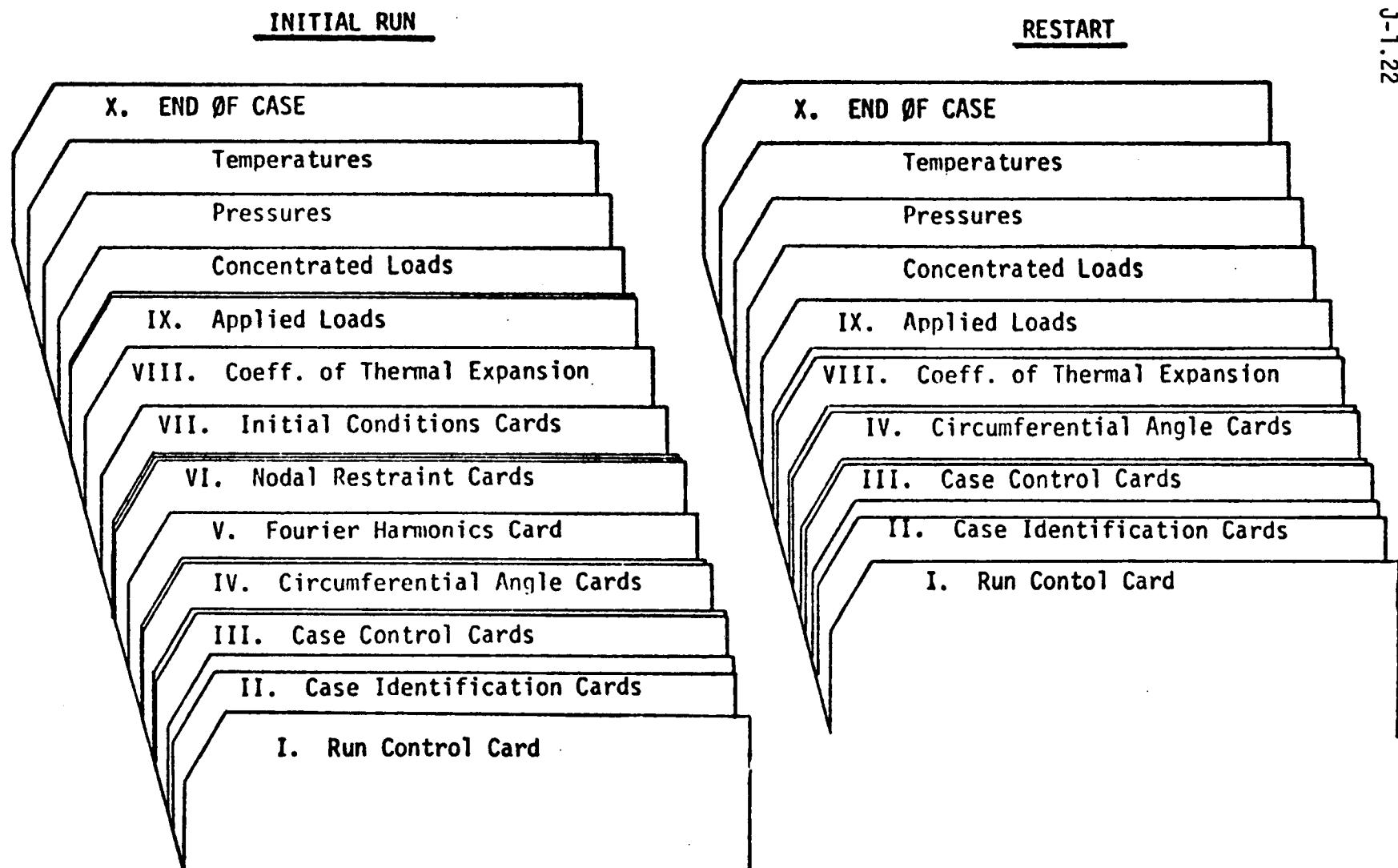


FIG. 1 CONSTITUTION OF DATA DECKS - INITIAL RUN AND RESTART MODES.

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I. RUN CONTROL CARD

This card is used to identify the number of cases to be run and the logical unit numbers of the scratch tapes used in the run. (ONLY ONE CARD I IS USED PER RUN.)

I Card Type I Format (3I5)

Columns	Variable	Description
1-5	NCASES	The number of different data sets utilized for this run.
6-10	ND	Logical unit number of the scratch tape onto which all the data is read at the start of the run.
11-15	NS	Logical unit number of a second scratch tape used by the program.

II. CASE IDENTIFICATION CARDS

These cards allow the user to print out comments which identify the problem being run.

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A. Control Card (ONE CARD II-A PER DATA SET)

Card Type II-A Format (2I5)		
Columns	Variable	Description
1-5	NCARDS	Number of comment cards (TYPE II-B) which follow.
6-10	NT	Logical unit number of the tape (prepared by SAMMSOR) from which the stiffness and mass matrices, element properties, and restart information, if needed, will be read.

- B. Identification Cards - The information punched on these cards is printed as output and should identify the problem being run. These comments should not duplicate those of the SAMMSOR case since the SAMMSOR comments will also appear as output. (IF NCARDS=0, OMIT CARDS II-B, OTHERWISE INCLUDE NCARDS OF TYPE II-B.)

Card Type II-B Format (20A4)		
Columns	Variable	Description
1-80	COMENT	Any desired alphanumeric information may be printed on these cards.

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III. CASE CONTROL CARDS

- A. Control Constants - Time parameters, restart information, and other miscellaneous control constants are input on this card. (INCLUDE ONE CARD III-A PER DATA SET.)**

Card Type III-A Format (2F10.0,4I5)		
Columns	Variable	Description
1-10	TOTIME	The maximum time (seconds) for which the calculations are to be performed.
11-20	DELTE	Time increment (seconds) used in solving the equations of motion.
21-25	IRSTRT	Control constant which indicates if the solution is being restarted. If the solution is being restarted set IRSTRT = 1. If not, set IRSTRT = 0.
26-30	INCRST	The number of the time increment at which the solution is to be restarted. INCRST must be an integer multiple of the value of NPRNIT used in the previous run. If IRSTRT = 0, set INCRST = 0.
31-35	NCLOSE	For a closed shell (such as a spherical cap or a hemisphere) where node 1 is at the apex, set NCLOSE = 1. Radial and rotational restraints will then be applied for the zeroth harmonic to aid the numerical stability of the solution. If the shell does not fit the above description, set NCLOSE = 0.
36-40	ITELF	If thermal loads are to be applied in the program, set ITELF = 1. Otherwise, set ITELF = 0.

- B. Print Control Card - The constants used to control the program output are punched on this card. (INCLUDE ONE CARD III-B PER DATA**

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SET.)

Card Type III-B Format (10I5)

Columns	Variable	Description
1-5	NPRNTQ	If the displacements are to be printed, set NPRNTQ = 1. If not, set NPRNTQ = 0.
6-10	IPRINT	If NPRNTQ = 1, the displacements will be printed every IPRINT time increments beginning with the first time step. If NPRNTQ = 0, set IPRINT = 0.
11-15	NCLCST	If the stresses and stress resultants are to be calculated, set NCLCST = 1. If not, set NCLCST = 0.
16-20	NSTRSS	If NCLCST = 1, the stress and stress resultants will be calculated and printed every NSTRSS time increments beginning with the first step. If NCLCST = 0, set NSTRSS = 0.
21-25	NPRNT	If restart information is to be placed on tape, set NPRNT = 1. If not, set NPRNT = 0.
26-30	NPRNIT	If NPRNT = 1, the restart information will be written on the output tape every NPRNIT time increments. If NPRNT = 0, set NPRNIT = 0. It is suggested that relatively large values of NPRNIT be used, say 200, 400,etc., if the total number of time steps is relatively large.
31-35	NPRNTL	If a printout of the applied loads is desired, set NPRNTL = 1. Otherwise, set NPRNTL = 0.
36-40	NPRNTF	If a printout of the generalized forces is desired, set NPRNTF = 1. Otherwise, set NPRNTF = 0.

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| 41-45 NPRNTH If the Fourier coefficients for the temperature
| and temperature gradient are to be printed, set
| NPRNTH = 1. Otherwise, set NPRNTH = 0.
|
|

| 46-50 NPRNMS If the mass and stiffness matrices are to be
| printed, set NPRNMS = 1. If not, set
| NPRNMS = 0.
|
|

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IV. CIRCUMFERENTIAL ANGLE CARDS

The circumferential angles at which the displacements and stresses are to be calculated are read from these cards.

A. Control Card - (ONE CARD IV-A PER DATA SET.)

Card Type IV-A Format (I5)		
Columns	Variable	Description
1-5	NTHETA	The number if circumferential angles at which the displacements and possibly stresses are to be calculated. ($1 \leq NTHETA \leq 20$)

B. Circumferential Angles - (INCLUDE 1-3 CARDS IV-B PER DATA SET
DEPENDING UPON THE VALUE OF NTHRETA.)

Card Type IV-B Format (8F10.0)		
Columns	Variable	Description
1-10	THETA(1)	Circumferential angles at which the displacements and possible stresses will be calculated.
11-20	THETA(2)	(If it is desired to calculate the displacements only along the line = 0, then include one card IV-B and set THETA(1) = 0.0)
"	"	
"	"	
"	THETA(NPHTETA)	
	

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V. FOURIER HARMONICS CARD

This card provides the number of Fourier cosine harmonics to be employed for this analysis and enumerates the specific harmonics to be used. (IF IRSTART = 1, OMIT CARD V. OTHERWISE, INCLUDE ONE CARD V PER DATA SET.)

Card Type V Format (6I5)		
Columns	Variable	Description
1-5	NH	The total number of Fourier cosine harmonics to be utilized in this analysis ($1 \leq NH \leq 5$).
6-10	IHARM(1)	Specific harmonics numbers to be employed. NH
11-15	IHARM(2)	values must be given and the zero harmonic
16-20	IHARM(3)	must always be specified as one of the input
21-25	IHARM(4)	harmonic numbers. The user should check to be
26-30	IHARM(5)	certain that the information for each of these harmonics has been created and stored on tape by the SAMMSOR code.

Example: Consider a case where it is desired to utilize harmonics 0, 2, 3, and 4. The input data for card V would then utilize the following values:

NH = 4

IHARM(1) = 0 NOTE: IHARM(1) should always
be set equal to zero.

IHARM(2) = 2

IHARM(3) = 3

IHARM(4) = 4

Columns 26-30 corresponding to IHARM(5) should be left blank for this example since only four harmonics are being run.

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VI. NODAL RESTRAINT CARDS (Boundary Conditions)

The displacement constraints applied to the shell are described utilizing these cards. (IF IRSTRT = 1, OMIT CARDS VI-A AND VI-B.)

A. Control Card - (ONE CARD VI-A PER DATA SET, UNLESS IRSTRT = 1.)

Card Type VI-A Format (I5)		
Columns	Variable	Description
1-5	NODRES	Total number of displacement constraints to be applied to the shell ($0 \leq \text{NODRES} \leq 204$)

B. Boundary Conditions - (THE NUMBER OF CARDS OF TYPE VI-B MUST EQUAL NODRES, UNLESS IRSTRT = 1. IF NODRES = 0, OMIT CARDS VI-B.)

Card Type VI-B Format (2I5)		
Columns	Variable	Description
1-5	NP	Number of the node where the restraint is to be applied.
6-10	NDIRCT	Key used to indicate the degree of freedom which is restrained. NDIRCT = 1 applies axial restraint NDIRCT = 2 applies circumferential restraint NDIRCT = 3 applies radial restraint NDIRCT = 4 applies rotational restraint

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VII. INITIAL CONDITIONS CARDS

The initial velocities and displacements of the nodes are specified on these cards. (IF IRSTART = 1, OMIT CARDS VII-Z, VII-B, AND VII-C.)

- A. Control Card - Utilization of this control card greatly simplifies the specification of the initial conditions if either the initial velocities or the initial displacements, or both, are equal to zero. (ONE CARD VII-A PER DATA SET)**

Card Type VII-A Format (2I5)		
Columns	Variable	Description
1-5	IQN	If the initial velocities at all the nodes are zero, set IQN = 0. If not, set IQN = 1.
6-10	IQN1	If the initial displacements at all the nodes are zero, set IQN1 = 0. If not, set IQN1 = 1.

- B. Initial Velocities - The initial nodal velocities must be specified for each node of the shell for each harmonic to be run. The logic used to input the nodal velocities is essentially the same as the procedure used to specify the element properties in the SAMMSOR code. The initial velocities for each of the nodes are specified for the first of the input harmonics, then for the second input harmonic, etc. This process is repeated until the nodal velocities for the first of the input harmonics, then for the second input harmonic, etc. This process is repeated until the nodal velocities for each harmonic have been specified. (IF IQN = 0, OMIT CARD)**

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VII-B.)

Card Type VII-B Format (2I5, 4F10.0)		
Columns	Variable	Description
1-5	IN1	First node to which the velocities specified on this card are applied.
6-10	IN2	Last node to which the velocities specified on this card are applied.
11-20	\dot{q}_1	Initial nodal velocity in the axial direction for a particular harmonic.
21-30	\dot{q}_2	Initial nodal velocity in the circumferential direction for a particular harmonic.
31-40	\dot{q}_3	Initial nodal velocity in the radial direction for a particular harmonic.
41-50	\dot{q}_4	Initial nodal rotational velocity in the meridional direction for a particular harmonic.

- C. Initial Displacements - In identically the same manner as is utilized for the initial velocities, the initial displacements are

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specified for each harmonic. (IF IQN1 = 0, OMIT CARDS VII-C)

Card Type VII-C Format (2I5, 4F10.0)

Columns	Variable	Description
1-5	IN1	First node to which the displacements specified on this card are applied.
6-10	IN2	Last node to which the displacements specified on this card are applied.
11-20	q ₁	Initial nodal displacement in the axial direction for a particular harmonic.
21-30	q ₂	Initial nodal displacement in the circumferential direction for a particular harmonic.
31-40	q ₃	Initial nodal displacement in the radial direction for a particular harmonic.
41-50	q ₄	Initial nodal rotation in the meridional direction for a particular harmonic.

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VIII. COEFFICIENTS OF THERMAL EXPANSION

If the thermal effects are to be included in the analysis, the coefficients of thermal expansion must be specified using these cards. These coefficients are assumed to be constant for a given element but may vary from element to element. These coefficients are read in the same manner as the element properties in the SAMMSOR code. (THE NUMBER OF CARDS VIII MUST BE \leq NELEMS FOR ANY GIVEN DATA SET. IF IIELF = 0, OMIT CARDS VIII.)

Card Type VIII Format (2I5, 2F10.0)

Columns	Variable	Description
1-5	IELM1	Number of the first element to which the properties on this card apply.
6-10	IELM2	Number of the last element to which the properties on this card apply.
11-20	ALSI1	Coefficient of thermal expansion in the meridional direction (in/in/deg).
21-30	ALTI1	Coefficient of thermal expansion in the circumferential direction (in/in/deg).

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IX. APPLIED LOADS, TEMPERATURES, AND TEMPERATURE GRADIENTS

Since the concentrated nodal loads, distributed pressures, temperatures, and temperature gradients may vary in time; it may be necessary to specify these loads at a number of points in time. If these loads and temperatures are input at times $T_{1,j}$ and $T_{1,j+1}$, the program will calculate generalized forces due to these loads at each of the input times. A linear variation of the generalized forces is then assumed between the times the loads are input. As soon as the value of the time reaches $T_{1,j+1}$, a new set of loads is read in at $T_{1,j+2}$ and the process of calculating the generalized forces is repeated. The time increment, DELTE (CARD III-A), used in the solution of the equations of motion must be less than the difference between any two of the times at which the loads are specified. If the loads and/or temperatures propagate in and direction (moving loads), it is advisable to specify the loads at more times than is necessary if they vary in intensity only.

Ring loads can be applied at the nodes and must be input for each of the harmonics. The ring loads utilize the same sign convention employed for the shell nodal displacements.

The pressure loadings, temperatures and temperature gradients are assumed constant over the meridional length of the element but variations in the circumferential direction are allowed. These loadings may be input in one of two ways. Either the Fourier coefficients can be specified for each harmonic or the values of the loads may be specified at a number of circumferential angles around the shell elements. Utilizing this second procedure a step function variation is assumed in the circumferential direction. That is, the load is assumed constant from 0_j to 0_{j+1} with the value of the loads being equal to those specified at 0_j . Sign conventions for the pressure loading are given in Figure 2.

A control card (Card Type IX-A) containing several key variables is used to guide the reading of the loading conditions. Proper selection of the values of these key variables results in a highly efficient procedure for specifying a wide variety of loading conditions. The key words and their meanings are explained in Figure 3.

Before attempting to input loads to the code the user is advised to study the guidelines presented in Section II, the example problems of Section II, and Appendix 6 which presents a thorough discussion of the various procedures necessary for specifying the loads.

A. Load Control Card

This control card is utilized to direct the input of the loads for a given time. This card indicates the presence or absence of concentrated

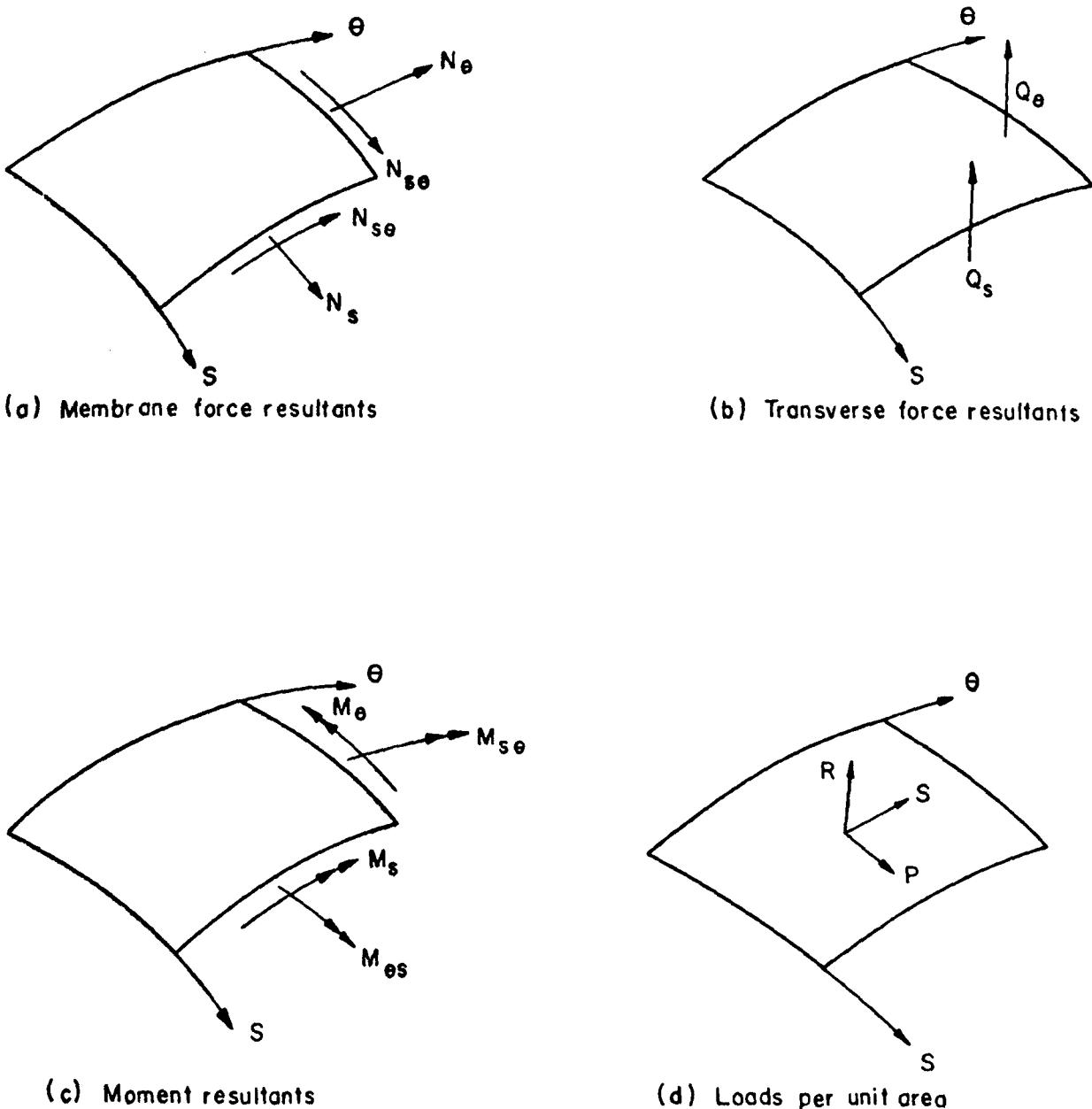
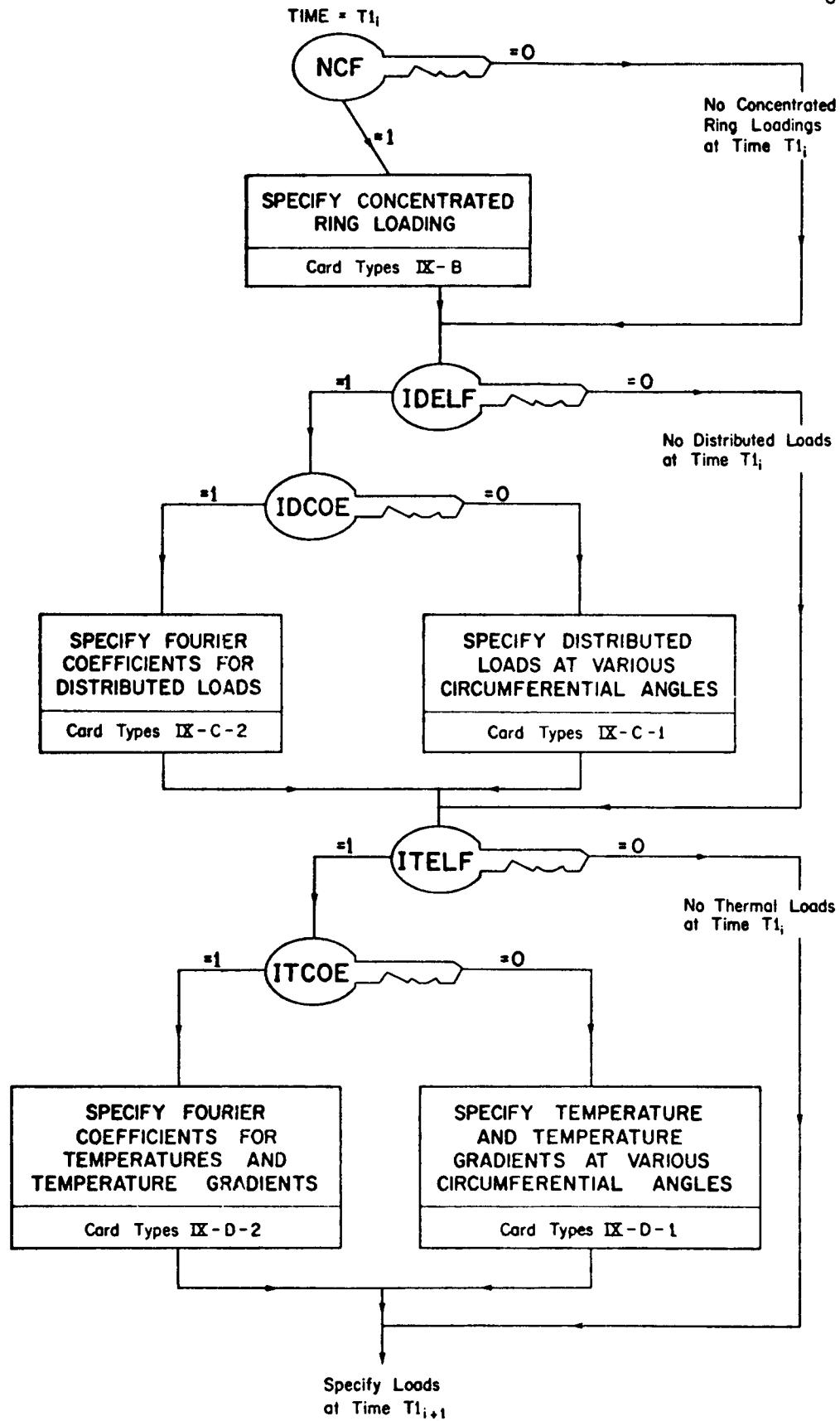


FIG 2 POSITIVE DIRECTION OF FORCES, MOMENTS,
AND LOADS ON SHELL SEGMENT

Fig. 3 LOAD SPECIFICATION AT TIME T_{1i}

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forces and distributed pressure loadings and indicates the procedure to be utilized for creating the generalized thermal forces. (ONE CARD IX-A IS NECESSARY FOR EACH TIME AT WHICH THE LOADS ARE BEING INPUT.)

Card Type IX-A Format (F10.0, 4I5, A8)

Columns	Variable	Description
1-10	T1	The time for which the loads are being input (sec).
11-15	NCP	If concentrated ring loads are applied to the structure at time T1, set NCP = 1. If not, set NCP = 0.
16-20	IDELF	If distributed loads are to be applied to the shell at time T1, set IDELF = 1. If not, set IDELF = 0.
21-25	IDCOE	If the Fourier cosine coefficients for the distributed loadings are to be read in at time T1, set IDCQE = 1. If not, set IDCQE = 0.
26-30	ITCOE	If the Fourier cosine coefficients for the temperatures and temperature gradients are to be read in at time T1, set ITCOE = 1. If not, set ITCOE = 0.
31-38	CONSTP	If the applied loads, temperatures and temperature gradients are constant from time, T1, to the final time, TOTIME (CARD III-A), punch the word CONSTANT in columns 31-38. If these parameters are not constant, leave columns 31-38 blank.

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B. Concentrated Ring Loads

The concentrated ring loads must be specified for each harmonic. (IF NCF = 0, OMIT CARDS IX-B.)

1. Control Card - This card indicates the presence or absence of concentrated ring loads for a particular harmonic. (ONE CARD IX-B-1 FOR EACH HARMONIC.)

Card Type IX-B-1 Format (I5)		
Columns	Variable	Description
1-5	NCF1	If there are concentrated ring loads for this particular harmonic, set NCF1 = 1. If not, set NCF1 = 0.
.....		

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2. Concentrated Ring Loads - For harmonics having ring loads associated with them, the loads are specified using these cards. (IF NCP1 = 0, OMIT CARDS IX-B-2 FOR THE HARMONIC BEING CONSIDERED.) ONE OR MORE CARDS IX-B-2 MAY BE USED, BUT NEVER UTILIZE MORE THAN 51 PER HARMONIC.

Card Type IX-B-2 Format (2I5, 4F10.0)

Columns	Variable	Description
1-5	IN1	First node to which this loading applies.
6-10	IN2	Last node to which this loading applies.
11-20	F1	Axial ring load applied at a node (lb).
21-30	F2	Circumferential ring load applied at a node (lb).
31-40	F3	Radial ring load applied at a node (lb).
41-50	F4	Concentrated moment applied at a node (in-lb).

Examples: The use of cards IX-B should become clear after considering the following examples:

1. Consider the case where a uniform tensile ring loading of 100 psi is being applied in the axial direction to the first node of a cylinder. The solution for this problem has been presented in Figure 20 of Reference 31. The thickness of the cylinder is 0.1

* The total value of the ring load for each harmonic is input, not the load per unit length of circumference. For complicated ring loads the value of the load input for each harmonic is obtained by integrating the product of the load and the corresponding displacement function around the circumference.

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inches with the radius being given as 6 inches. Consider that harmonics 0 and 2 are being run. The total ring load for the zero harmonic will be $(100) \times 2\pi(6) \times (0.1) = 376.9$ lb.

Five cards of type IX are required to input these loads assuming they are constant from time $T1 = 0.0$ to $TOTIME$ and assuming 50 elements are used to idealize the structure.

CARD	VARIABLE	VALUES
IX-A	$T1 = 0.0$	$NCF = 1$ $IDELF = IDCOE = ITCOE = 0$
IX-B	$NCF1 = 1$	(HARMONIC 0)
IX-C	$IN1=1 IN1=1$	$F1 = -376.9 F2 = F3 = F4 = 0$
IX-C	$IN1 = 2 IN1 = 51$	$F1 = F2 = F3 = F4 = 0$
IX-B	$NCF2 = 0$	(HARMONIC 2)

2. The second example considers a radial ring load of $F \cos\theta$ applied to a cylinder of radius r .

Performing the integration, one obtains the radial ring load for harmonic 1 as

$$F3 = \int_0^{2\pi} (F \cos\theta) r \cos\theta d\theta \\ = \pi r F$$

The Fourier coefficients for the other harmonics are zero.

C. Distributed Loads - (IF IDELF = 0, OMIT CARDS IX-C)

The distributed loadings may be input in one of two ways: the Fourier coefficients may be read in for each harmonic or the loadings may be specified at a desired number of circumferential angles (≤ 37). If the second option is used, the Fourier coefficients will then be generated internally. The user should note that it is possible to input distributed loads in only one of two ways.

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1. Distributed Loads - (Input at various circumferential angles)
Since the choice of the displacement functions utilized in this analysis necessitate the presence of loads symmetric about the meridian $\theta = 0$, it is necessary to specify the distributed loadings for angles from $0^\circ \rightarrow 180^\circ$. The code then assumes that the distribution from $180^\circ \rightarrow 360^\circ$ is the mirror image of the input distribution. (IF IDCQE = 1, OMIT CARDS IX-C-1)
 - a. Control Card - Utilize this card to indicate the number of angles for which the loads will be specified.

Card Type IX-C-1-a Format (3I5)

Columns	Variable	Description
1-5	IELM1	First element to be distributed loading applies.
6-10	IELM2	Last element to which this distributed loading applies.
11-15	NDP	Number of circumferential angles at which the distributed loads are to be specified ($1 \leq NDP \leq 37$). If the loadings are constant in the circumferential direction set NDP = 1.

- b. Distributed Loads at Specified Angles* This card specifies the angle at which the loads are being input and provides the values of the loads at that angle. (INCLUDE NDP CARDS OF

* The first loading must always be given for $\theta = 0^\circ$. The next loading is given at the angle where the load changes in value. If the load is constant with respect to θ , only one card will be necessary to input the load. Do not input values for the loads at $\theta = 180^\circ$ since the load at that angle will be equal in all cases to the load input at the previous value of THETAB.

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TYPE IX-C-1-b FOR EACH CARD IX-C-1-a.)

Card Type IX-C-1-b Format (4F10.0)		
Columns	Variable	Description
1-10	THETB	Circumferential angle (degrees) for which this data is given.
11-20	P	Distributed load in the meridional direction (psi).
21-30	R	Distributed load in the normal direction (psi).
31-40	S	Distributed load in the circumferential direction (psi).

Example: Consider the normal pressure distribution on an element depicted in Figure 4. To input the pressure on this element requires specification of the pressures for four values of θ .

THETB	R(I)
0.0	-Q1
30.0	-Q2
90.0	-Q3
2.0	0.0

2. Distributed Loads - (Fourier Coefficients) The Fourier coefficients for the distributed loads may be specified using these cards. The coefficients must be specified (even though they may be zero) for each harmonic being employed in the analysis. The coefficients are specified for each harmonic of the first group of elements, then for each harmonic of the second group, etc. until the values have been input for all the elements. (IF IDCOE = 0, OMIT CARDS IX-C-2)

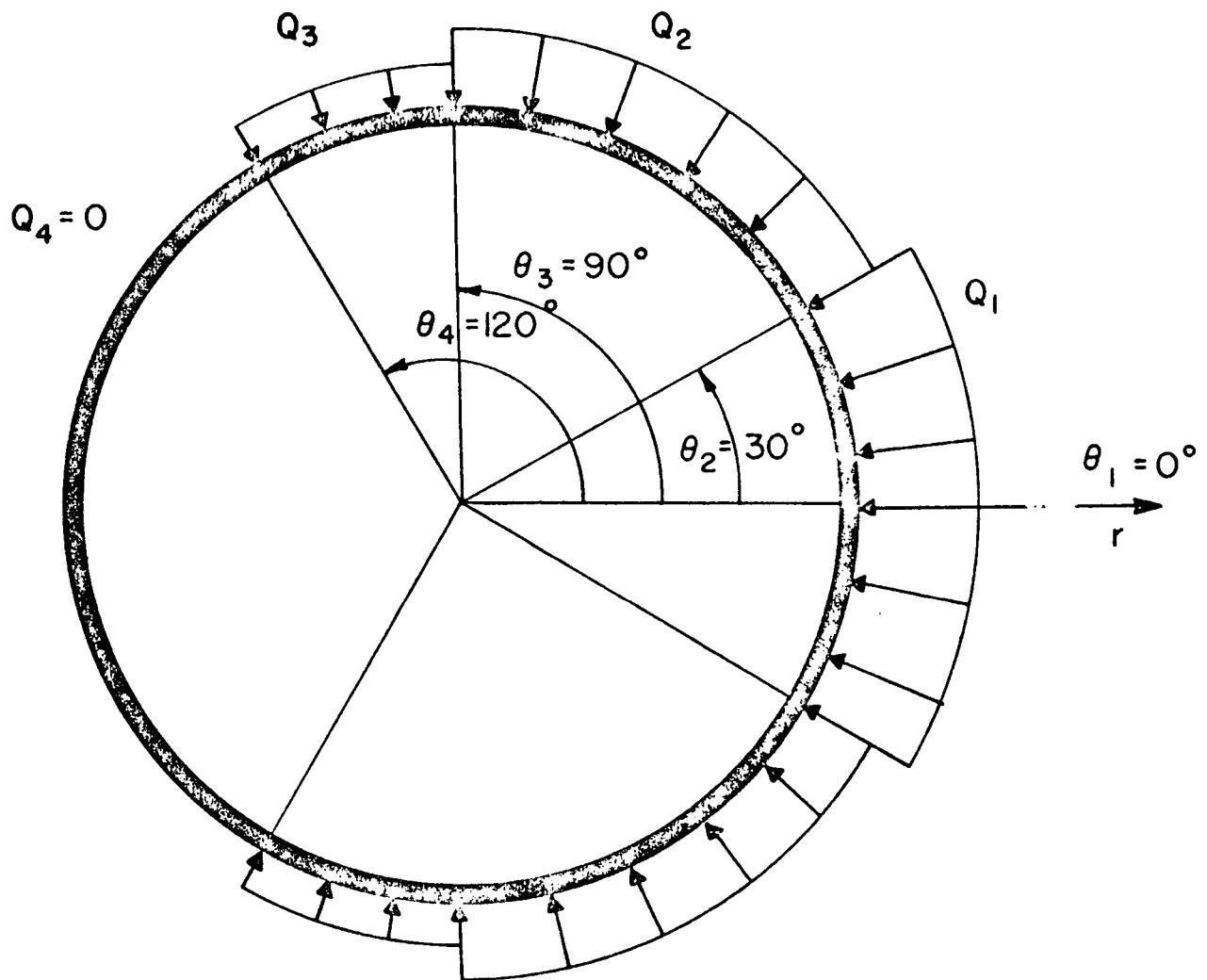


FIG 4 REPRESENTATIVE VARIATION OF DISTRIBUTED LOADS APPLIED TO A TYPICAL ELEMENT

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a. Control Card

Card Type IX-C-2-a Format (2I5)

Columns	Variable	Description
1-5	IELM1	First element to which these loads apply.
6-10	IELM2	Last element to which these loads apply.

b. Fourier Coefficients - (NH CARDS OF TYPE IX-C-2-b FOR EACH CARD IX-C-2-a.)

Card Type IX-C-2-b Format (3F10.0)

Columns	Variable	Description
1-10	P	Fourier coefficient of the distributed load in the meridional direction for a particular harmonic (psi).
11-20	R	Fourier coefficient of the distributed load in the normal direction for a particular harmonic (psi).
21-30	S	Fourier coefficient of the distributed load in the circumferential direction for a parti- cular harmonic (psi).

D. Temperature Distribution and Gradients

Essentially the same logic is employed for inputting the temperatures and gradients that was used for the specification of the distributed loads. The explanation of this procedure should therefore not need be repeated.

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The temperatures are specified for the midsurface of the shell. The temperature gradients (through the thickness) are considered positive if the temperature for the outer surface is greater than the temperature on the inner surface. (IF ITEL1 = 0, OMIT CARDS IX-D.)

1. Temperature Distribution and Gradients - (Input at various circumferential angles)

Again, the requirement of symmetry about the meridian $\theta = 0$, makes it necessary to specify the temperature distribution and thermal gradients only from $0^\circ \rightarrow 180^\circ$. The temperature distribution and gradients are input on the same cards for the various angles. (IF IFCOE = 1, OMIT CARDS IX-D-1.)

- a. Control Card - Utilize this card to indicate the number of angles for which the temperature and gradients will be specified.

Card Type IX-D-1-a Format (3I5)		
Columns	Variable	Description
1-5	IELM1	First element to which this data applies.
6-10	IELM2	Last element to which this data applies.
11-15	NDP	Number of circumferential angles at which the temperature distribution and gradient are to BE SPECIFIED ($1 \leq NDP \leq 37$). If the temperature is constant in the circumferential direction, set NDP = 1.

- b. Temperature and Temperature Gradient at Specified Angles -

This card specifies the angle at which the temperature and temperature gradient (through the thickness) is being input and provides the value of the temperature at that angle. (INCLUDE NDP CARDS OF TYPE IX-D-1b

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FOR EACH CARD IX-D-1-a.)

Card Type IX-D-1-b Format (3F10.0)

Columns	Variable	Description
1-10	THETB	Circumferential angle for which this temperature and gradient are given.
11-20	P	Distributed temperature at $\theta = \text{THETB}$ ($^{\circ}\text{F}$).
21-30	R	Temperature gradient (through the thickness) at $\theta = \text{THETB}$ ($^{\circ}\text{F/in}$).

2. Temperature Distribution and Gradient - (Fourier Coefficients)

If the user so desires, the Fourier coefficients for the temperature distribution and gradient may be specified for each of the harmonics being used. Again, the coefficients are specified for all harmonics for the first group of elements, then for the second group, etc., until all the element coefficients have been input. (IF ITCOE = 0, OMIT CARDS IX-D-2)

a. Control Card

Card Type IX-D-2-a Format (2I5)

Columns	Variable	Description
1-5	IELM1	First element to which these properties apply.
6-10	IELM2	Last element to which these properties apply.

b. Fourier Coefficients - (NH CARDS OF TYPE IX-D-2-b FOR EACH

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CARD IX-D-2-a.)

Card Type IX-D-2-b Format (2P10.0)

Columns	Variable	Description
1-10	TH1	Fourier coefficient of the temperature distribution ($^{\circ}$ F) for a particular harmonic.
11-20	DTH1	Fourier coefficient of the temperature gradient ($^{\circ}$ F/in) for a particular harmonic.

X. FINAL DATA CARD FOR A CASE

Place this card after the last card IX of each data set. This signifies the end of the input data for a case. (ONE CARD X PER DATA SET.)

Card Type X

Columns	Punch
1-11	END OF CASE

XI. FINAL DATA CARD FOR A RUN

This card must be placed after the card X of the last case to be run.

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It denotes the end of the input data for a run. (ONE CARD XI PER RUN)

Card Type XI	
Columns	Punch
1-10	END OF RUN

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SECTION IV

EXAMPLE PROBLEMS

The example problems which follow were chosen to demonstrate the versatility of the code and to further acquaint the users with the procedures for inputting the data to the code. The data presented herein is typical for the problems solved by the code and demonstrates many of the input procedures.

Since the most complex portion of the input data is the specification of the loading conditions, a variety of loadings are demonstrated. Response curves are presented so the user may check his output with the previously obtained curves. The first two example problems utilize the shells described in example problems 1 and 2 of the SAMMSOR user's guide (Ref. 1) while the third example problem demonstrates the two procedures for specifying distributed pressure loadings.

Example Problem 1

The first example problem was chosen to demonstrate the procedure for inputting a concentrated ring load and to demonstrate the program's capability to solve highly nonlinear problems. For the forty pound load applied in this problem, the static solution shows that the nonlinear displacement is more than four times as large as the linear solution.

The shell to which the load is applied is the shallow spherical cap ($\lambda=6$) utilized in the first example problem in the SAMMSOR user's guide. The edges of the shell are assumed to be clamped. Since the loading is symmetric, the displacements and stresses will be calculated only along the line $\theta = 0$. Only the response for the zeroth harmonic will be determined. A set of input data for this case is presented in Figure 5 with the displacement response of the apex of the shell being presented in Figure 6. This response curve should allow the user to check his version of the code.

Example Problem 2

The shell described in the second example problem in the SAMMSOR user's guide is now subjected to a 50 psi internal pressure. The load-in is applied at time $T_1 = 0.0$ and remains constant for the duration of the calculation.

Two sets of input data are provided for this example problem. The first set (Figure 7) allows the program to calculate the response for the first 300 time steps. The second set of input data (Figure 8) will

Fig. 5 INPUT DATA - EXAMPLE PROBLEM 1

NCASE= 1

PRINTOUT OF INPUT DATA

CARD TYPE	10	20	30	40	50	60	70	80
	12345678901234567890123456789012345678901234567890123456789012345678901234567890							
II - A	6	4						
- B	*****							
- B	EXAMPLE PROBLEM NO. 1 DYNASOR II USER'S MANUAL							
- B	THE SHELL DESCRIBED IN EXAMPLE PROBLEM 1 OF THE SAMMSOR USER'S GUIDE							
- B	IS SUBJECTED TO A 40 LB. APEX LOADING WITH THE SOLUTION BEING DETERMINED							
- B	FOR 400 TIME STEPS							
- B	*****							
III - A	0.0001	.00000025	0	0	1	0		
- B	1	4	1	8	1	100	1	1
IV - A	1							
- B	0.0							
V	1	0						
VI - A	4							
- B	31	1						
- B	31	2						
- B	31	3						
- B	31	4						
VII - A	0	0						
IX - A	0.0	1	0	0	OCONSTANT			
- B	1	1						
- 2	1	1	40.0	0.0	0.0	0.0		
- 2	2	31	0.0	0.0	0.0	0.0		
X	END OF CASE							

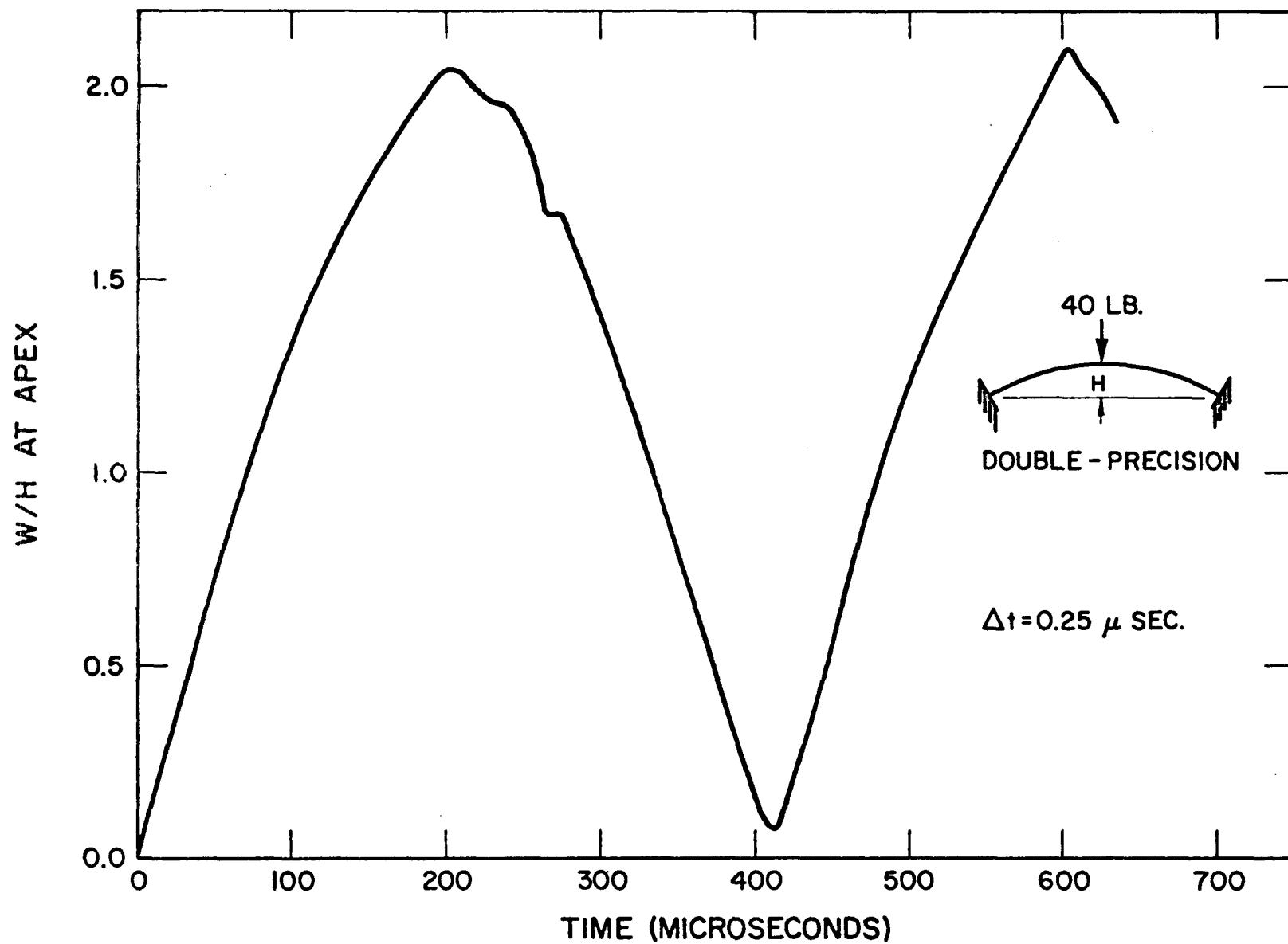


FIG. 6 APEX DISPLACEMENT RESPONSE UNDER CONCENTRATED AXIAL LOAD

Fig. 7 INPUT DATA - EXAMPLE PROBLEM 2

NCASE= 2

PRINTOUT OF INPUT DATA

CARD TYPE	10	20	30	40	50	60	70	80
	12345678901234567890123456789012345678901234567890123456789012345678901234567890							
II - A	6	8						
- B	*****							
- B	EXAMPLE PROBLEM NO. 2 DYNASOR II USER'S MANUAL							
- B	CAP-TORUS-CYLINDER CONFIGURATION							
- B	THE SHELL DEPICTED IN THE SECOND EXAMPLE PROBLEM OF THE SAMMOSR USER'S							
- B	MANUAL IS SUBJECTED TO A 50 PSI INTERNAL PRESSURE							
- B	*****							
III - A	0.0009	0.000003	0	0	1	0		
- B	1	10	1	20	1	100	1	1
IV - A	1							
- B	0.0							
V	1	0						
VI - A	4							
- B	51	1						
- B	51	2						
- B	51	3						
- B	51	4						
VII - A	0	0						
IX - A	0.0	0	1	0	OCONSTANT			
- C	-1-a	1	50	1				
	-b	0.0	0.0	50.0	0.0			
X	END OF CASE							

NCASE = 3

PRINTOUT OF INPUT DATA

CARD TYPE	10	20	30	40	50	60	70	80
	12345678901234567890123456789012345678901234567890123456789012345678901234567890							
II - A	6	8						
- B	***** EXAMPLE PROBLEM NO. 2 ***** DYNASOR II USER'S MANUAL							
- B	THE INPUT DATA NECESSARY TO RESTART THE CODE AT TIME INCREMENT 300							
- B	IS PROVIDED TO GUIDE THE USER IN HIS RESTART OPERATIONS. THE PROBLEM							
- B	IS TO BE RUN FOR AN ADDITIONAL 300 TIME INCREMENTS.							
- B	*****							
III - A	0.0018	0.000003	1	300	1	0		
- B	1	10	1	20	1	100	1	0
IV - A	1							
- B	0.0							
IX - A	0.0009	0	1	0	OCONSTANT			
- C - 1 - a ¹	50	1						
- b	0.0	0.0	50.0		0.0			
X	END OF CASE							

Fig. 8 INPUT DATA - EXAMPLE PROBLEM 2 - RESTART MODE

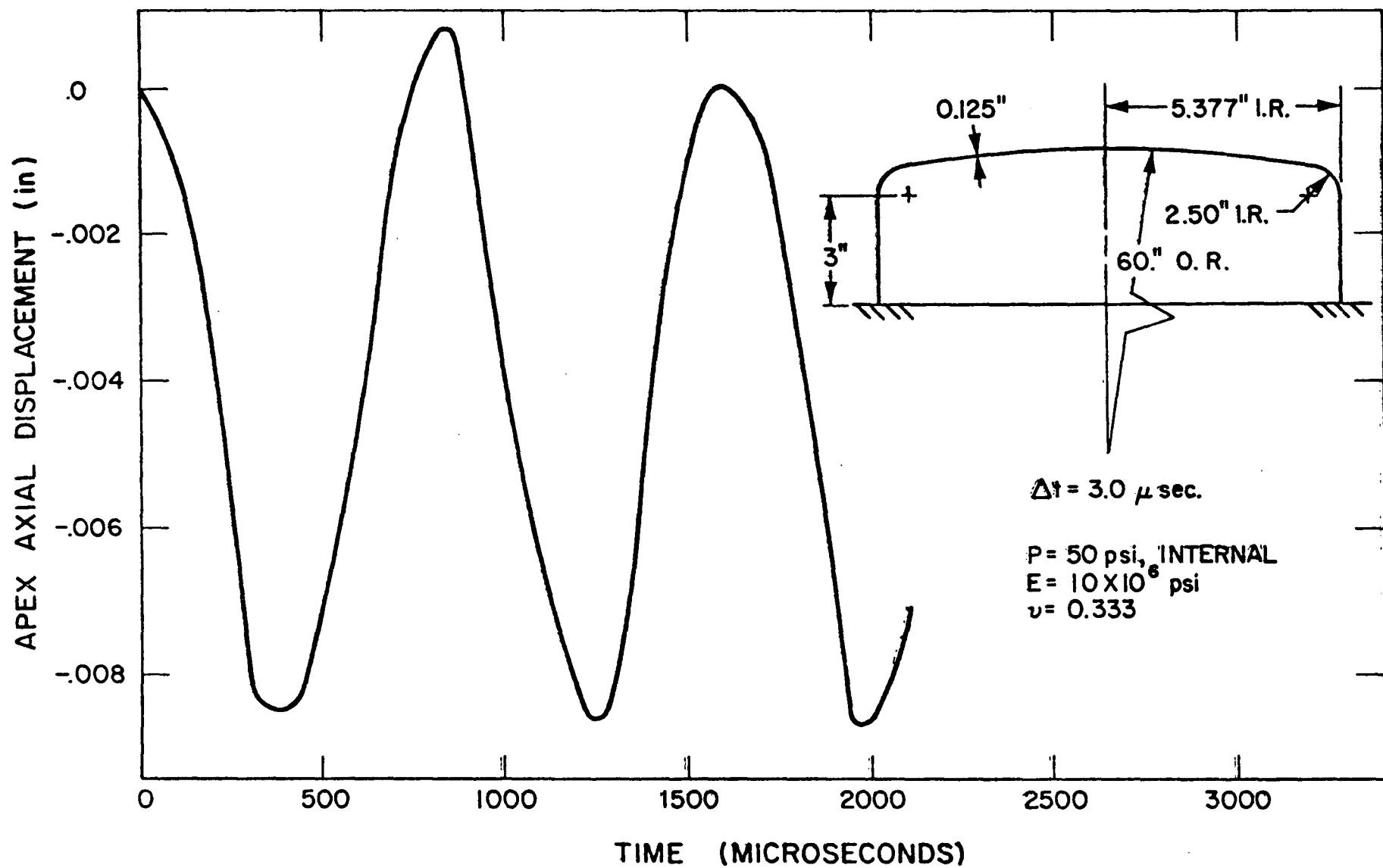


FIG. 9 DISPLACEMENT RESPONSE UNDER INTERNAL PRESSURE

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restart the code at the end of the 300th time step and will then allow the program to calculate the response for an additional 300 increments.

Since this problem is only moderately nonlinear, it is interesting to note that a much larger time step can be used for this problem than was employed in the previous example problem. The displacement response obtained for this problem is presented in Figure 9.

Example Problem 3

This example problem was selected to demonstrate the procedures for inputting the distributed loadings on a shell. A cylindrical shell (figure 10) is subjected to a half cosine loading which is symmetric about the meridian = 0. This load is applied along the entire length of the shell. The pressure loading may be specified in one of two ways:

- 1) The Fourier coefficients may be input for each harmonic.
- 2) The pressure may be specified at various circumferential angles with the Fourier coefficients then being internally generated.

The first set of input data (Figure 11) utilizes the first of the above procedures and inputs the Fourier coefficients. The input data presented in Figure 12 describes the loading by specifying the value of the pressure at the various angles. The same procedure is employed to describe the temperature and temperature gradient distributions.

Considering the symmetry of the loading and the boundary conditions applied to this shell, it can easily be recognized that the displacements and stresses will be symmetric about the center of this cylindrical tube. Therefore, only one-half of the shell needs to be analyzed. The plane of symmetry is assured by applying an axial and a rotational restraint at node one (1).

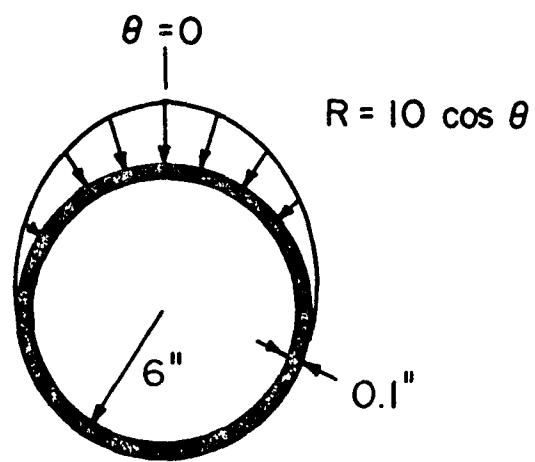
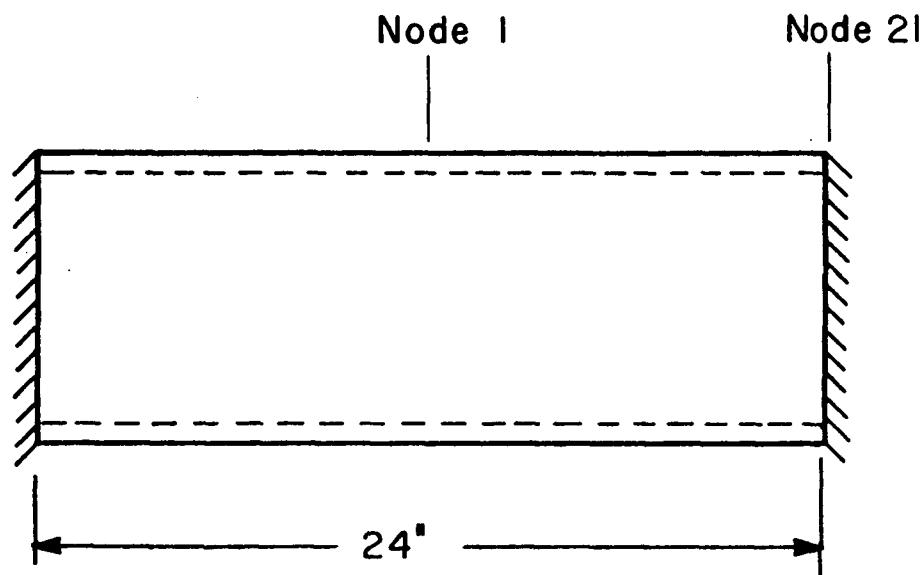


FIG 10 CYLINDRICAL SHELL SUBJECTED TO HALF COSINE PRESSURE LOADING

NCASE= 5

PRINTOUT OF INPUT DATA

CARD TYPE	10	20	30	40	50	60	70	80
	1	2	3	4	5	6	7	8
II - A	6	4						
- B	***** EXAMPLE PROBLEM NO. 3 DYNASOR II USER'S MANUAL							
- B	CYLINDRICAL SHELL IDEALIZED USING 30 ELEMENTS IS SUBJECTED TO A HALF COSINE							
- B	LOADING TO DEMONSTRATE THE OPTIONS FOR INPUTTING DISTRIBUTED LOADS.							
- B	** IN THIS CASE THE PRESSURE IS SPECIFIED BY INPUTTING THE FOURIER COEFFICIENTS							
- B	*****							
III - A	0.0005	0.00001	0	0	0	0		
- B	1	5	1	10	1	50	1	1
IV - A	2							
- B	0.0		30.0					
V	5	0	1	2	3	4		
VI - A	6							
- B	1	1						
- B	1	4						
- B	21	1						
- B	21	2						
- B	21	3						
- B	21	4						
VII - A	0	0						
IX - A	0.0	0	1	1	OCONSTANT			
- C - 2- a1	20							
- b	0.0	-3.1831		0.0				
- b	0.0	-5.0000		0.0				
- b	0.0	-2.1221		0.0				
- b	0.0	0.0000		0.0				
- b	0.0	0.4244		0.0				
X	END OF CASE							

Fig. 11 INPUT DATA - (SET #1) - EXAMPLE PROBLEM 3

NCASE = 4

PRINTOUT OF INPUT DATA

Fig. 12 INPUT DATA - (SET #2) - EXAMPLE PROBLEM 3

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REFERENCES

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3. Stricklin, J. A., Martinez, J. E., Tillerson, J. R., Hong, J. H., and Haisler, W. E., "Nonlinear Dynamic Analysis of Shells of Revolution by Matrix Displacement Method," Sandia Corporation Contractor Report SC-CR-70-6070, Feb. 1970.
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6. Stricklin, J. A., Haisler, W. E., MacDougall, H. R., and Stebbins, F. J., "Nonlinear Analysis of Shells of Revolution by the Matrix Displacement Method," AIAA Journal, Vol. 6, No. 12, Dec. 1968, pp. 2306-2312.
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Appendix 5 - Use of the Restart Option

In order for efficient use to be made of the DYNASOR II code, the user should become familiar with the option provided for restarting the program. Through effective use of this option the dynamic response studies can be completed using a minimum amount of computer time.

Use of the restart option may prove invaluable in a number of situations. Abnormal termination of the program may occur if a numerical instability is noted in the response. If this occurs, the restart option can be used with a different value of the time increment. Another important use of the restart option arises when the user is satisfied with the results previously obtained but desires to extend the response data to a further point in time. In such a case the program is restarted at the last time step for which the restart information was placed on tape. A most effective use of this option can be made when conducting dynamic stability analyses where it is desirable to evaluate the response to see if buckling has occurred. If it has not, the decision can then be made to extend the run to further points in time.

Utilizing large time steps can result in a damping effect upon the solution so it is advisable to run the problem for a couple of oscillations, check to see if the solution is significantly damped, and then run the problem for the desired number of oscillations. If an evaluation of the initial results indicates that a smaller or larger time step should be used, the restart facility might be used to keep from having to repeat the initial calculations.

The displacements, velocities, and forces should be written on tape for almost all of the cases to insure that the restart information will be available if an evaluation of the calculated response indicates that the program should be restarted. The time required to write the restart information on tape is negligible when compared with the amount of time required to obtain the total response.

If it is desirable to decrease the time increment when restarting the program, the user should exercise care in selection the increment (INRST) at which the program will be restarted. The decision to decrease the size of the time step will usually be based upon the observation that the solution has become unstable or that significant damping is present in the response. To restart the program the user must be sure that the increment (INCRST) has been selected small enough to insure that the inaccuracies created by the larger time step can be neglected.

On the other hand, if the results from a previous run indicate that it is possible to increase the size of the time step for the remaining calculations, then care must also be taken in the selection of INCRST. For the numerical extrapolation procedure to produce accurate sets of displacements, it is recommended that the solution be restarted on a

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relatively straight portion of the displacement response curve. Considering the curve presented in Figure 6, it would be recommended that the program be restarted at 500 microseconds rather than at 600 microseconds because of the extrapolation procedure being utilized (i.e. the curve is smoother at 500 microseconds).

When using the restart option, it is possible to specify different values for a number of the control constants and input parameters. The data on cards I-IV may be changed, but the same Fourier harmonics and boundary conditions must be used. It is also required that the coefficients of thermal expansion remain the same when restarting the program. These requirements allow the user to omit card types V, VI, and VII when preparing data for restart operations. The considerations effecting the input of the loads for restart operations are presented in Appendix 6.

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Appendix 6 - Load and Temperature Input Discussion

Since the DYNASOR II program accepts time varying loading and temperature conditions, the logic required to input these conditions is of necessity more complex than the logic required to input the other parameters. A discussion of the procedures for inputting these loading conditions is contained in this section. In this appendix the term loads refers to all distributed and concentrated forces while the term temperatures refers to both the temperature and temperature gradient distributions.

If there are no loads or no temperatures, it should be noted that a proper selection of the input constants allows omission of the input cards pertaining to the missing terms. In other words, the user selects the proper values for input keys and the proper read statements are automatically skipped.

To illustrate the procedure for inputting time varying loads and temperatures the information presented in Figure A6-1 is utilized. The load-time and temperature-time curves are approximated as a series of linear segments by specifying values of both the loads and temperatures at discrete points in time and then assuming linear variations between the times. In order to specify the loads and temperatures in Figure A6-1, it is necessary to specify both the loads and the corresponding temperatures at times T_{11} , T_{12} , and T_{13} . Both the applied loads and temperatures are constant from time T_{13} to the selected TOTIME so the value of CONSTL should be set equal to CONSTANT at time T_{13} . Obviously, if the loads or temperatures vary rapidly with time, it may be necessary to specify these conditions at a large number of times in order for the linear variation to be an accurate representation of the load-time and temperature-time curves.

The logic for the load and temperature input is now discussed for each of the two program start conditions, namely:

IRSTART = 0 Calculation begins at time increment = 0

IRSTART = 1 Calculation begins at time increment = INCRST

1. The loads and the temperatures must both be input at each time T_1 at which the loads or temperatures vary. In other words, the loads cannot be input at one time and the temperatures at another.
2. The difference between successive times at which the loads and temperatures are input ($T_{1j+1} - T_{1j}$) must always be

J-1.64

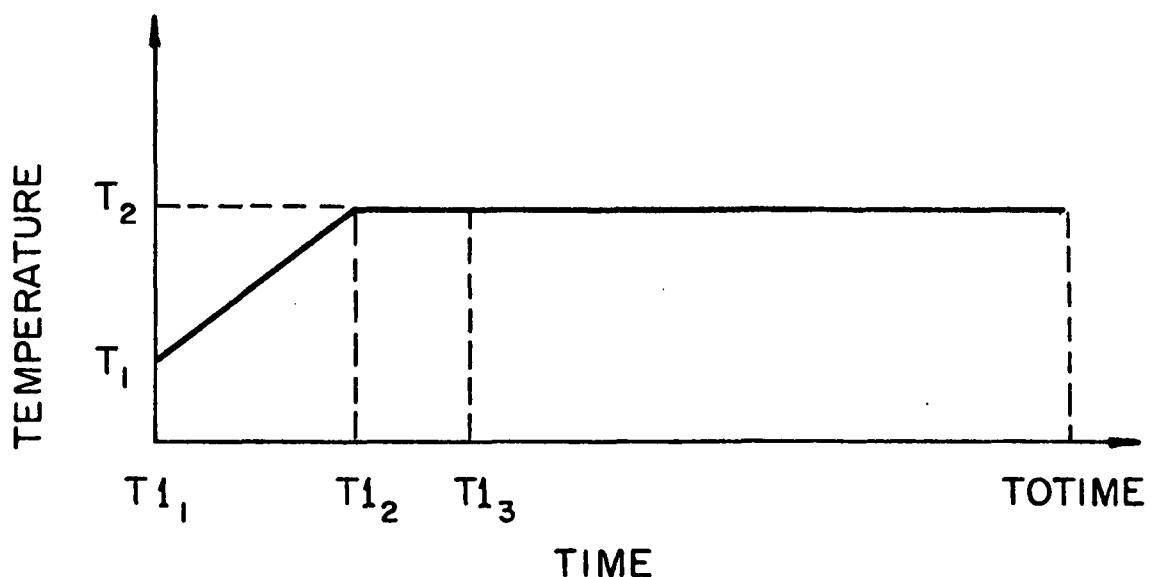
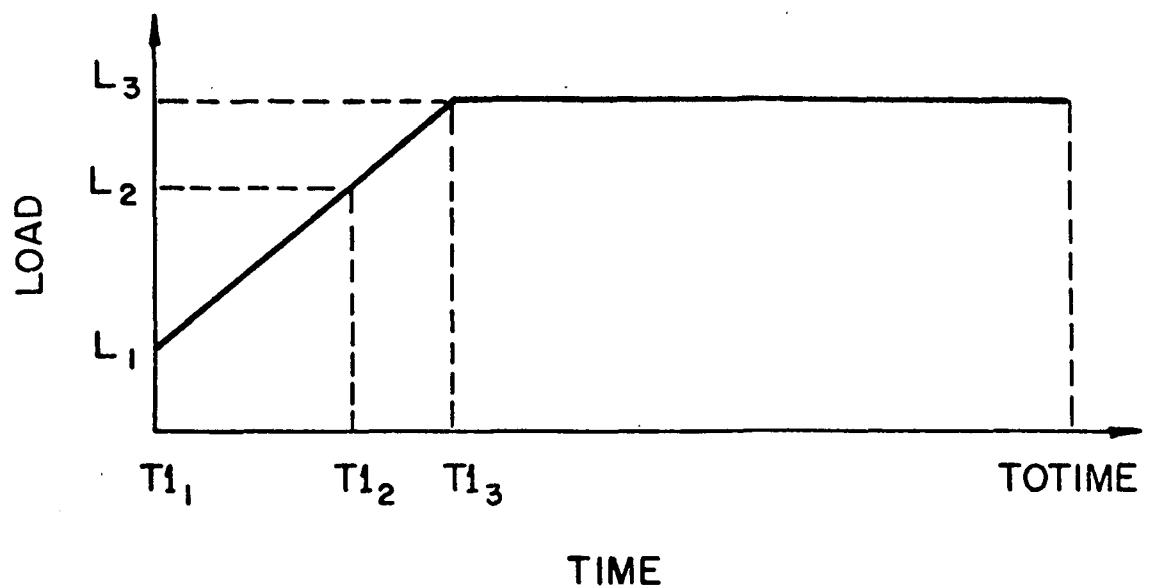


FIG A6-1 MECHANICAL AND THERMAL LOAD HISTORY FOR AN ELEMENT

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greater than the time increment (DELTE) specified for solving the equations of motion.

INRART = 0

The cases which may arise when considering the loads and temperatures and the input logic required to describe these situations are as follows when the program is making an initial run on a problem:

CASE	INPUT LOGIC
1. Loads and temperatures and constant (in time) on each element. Note, however, that variations from element to element are allowed.	Input only one set of loads and temperatures. These must be specified at time $T_1 = 0.0$ and the value of CONSTP should be read as CONSTANT.
2. Loads or temperatures (or both) vary with time.	Input, in order, the loads and temperatures at times T_{11} (must be equal to 0.0), T_{12} , T_{13} , ... until the value of T_1 reaches or exceed the value of TOTIME (total time for the case.) The columns for CONSTP should be left blank.

IRSTRRT = 1

The program may be restarted utilizing a new value for TOTIME which may be less than, equal to, or greater than the value which was utilized in the previous run which created and stored the restart information for use in this run. The previous value of TOTIME will be referred to as TOTIMEP. The input logic varies according to the relative values of TOTIME and TOTIMEP so each possible combination will be discussed separately.

Procedures which may not be utilized in the restart mode are:

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1. If the program was originally run as case A with IRSTART = 0, it is not possible to input loads and temperatures at any time until the value of TOTIMEP has been exceeded.
2. Consider that the program is being restarted at a time which is within the interval $T_{1,j} \text{ -- } T_{1,j+1}$. The loads and temperatures were input in the previous run for times $T_{1,j}$ and $T_{1,j+1}$. The first value of T_1 for which the loads and temperatures may be specified in the restart mode must be greater than the time $T_{1,j+1}$ which was utilized in the previous run.

Consideration will first be given to the cases where the new value of the maximum time is less than or equal to the one previously used.

TOTIME \leq TOTIMEP

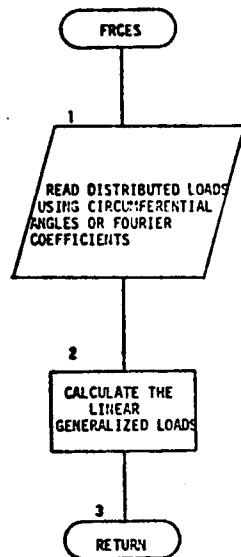
CASE	INPUT LOGIC
1. Both the loads and the temperatures are constant (in time) and are equal to the values specified for IRSTART = 0, Case 1.	No loads or temperatures are input
2. Both the loads and temperatures are constant (in time) but are different from the values specified for IRSTART = 0, Case 1.	This problem is not allowed by the program. If the user desires to run this case, it is suggested that the problem be rerun beginning at time = 0.0.
3. Loads or temperatures vary with time. (This cannot be a restart of Case 1, IRSTART = 0.)	Input loads and temperatures at times $T_{1,1}, T_{1,2}, \dots$ until the value $T_{1,n}$ reaches or exceeds the value of TOTIME. The value of T_1 must be greater than the value of $T_{1,j+1}$ of the previous run

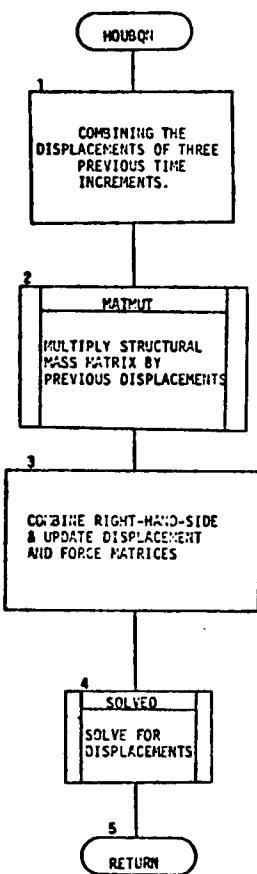
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The possible cases which may arise if the value of TOTIME is greater than TOTIMEP are now presented. It should be noted that cases differ only slightly from those previously discussed.

TOTIME > TOTIMEP

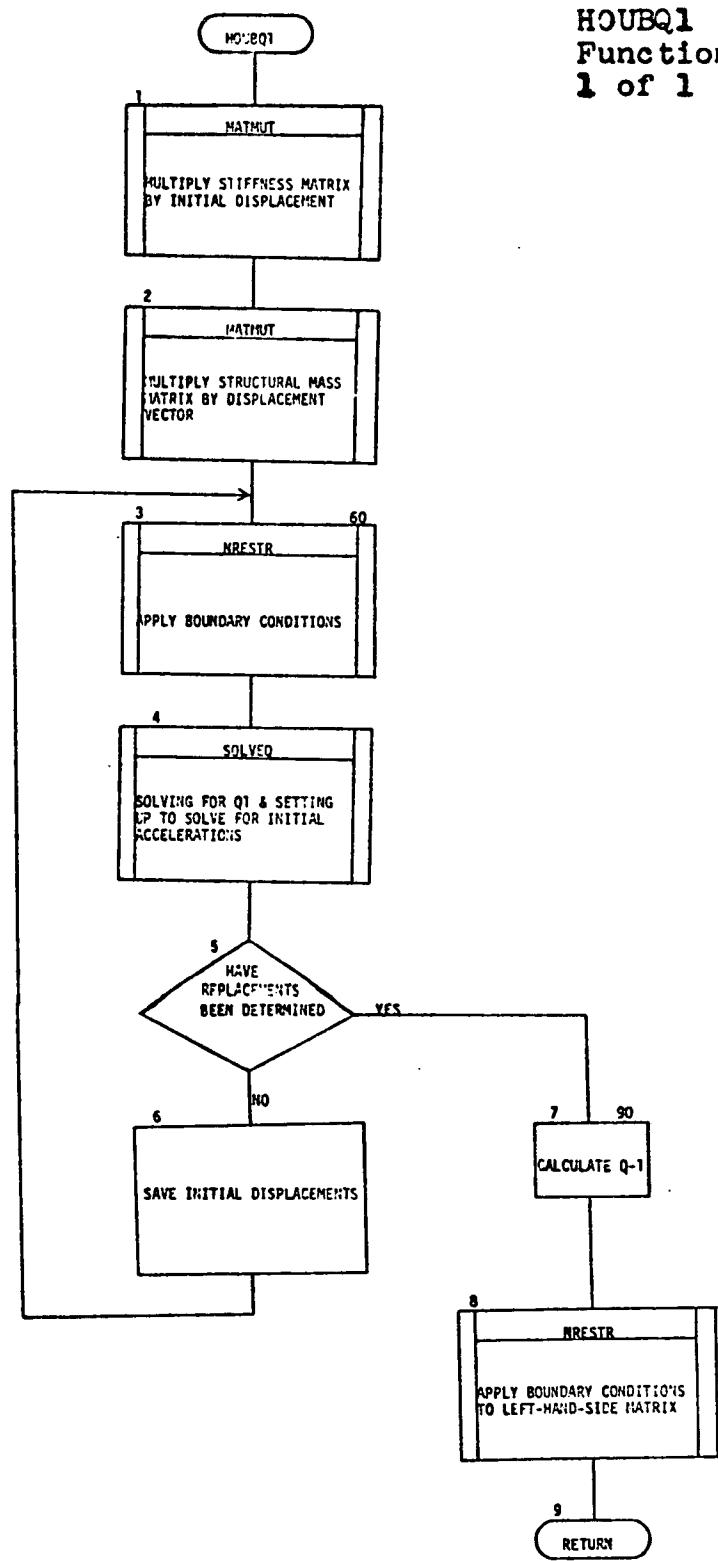
CASE	INPUT LOGIC
1. Both the loads and temperatures are constant (in time) and are equal to the values specified for IRSTART = 0, Case 1.	The loads and temperatures must be input for $T_1 = TOTIMEP$ and the value of CONSTF is set as CONSTANT. The specified loads and temperatures must be identical with those read for the previous run (IRSTART = 0).
2. Both the loads and temperatures are constant (in time) but are different from the values specified for IRSTART = 0, Case 1.	The new loads will not be applied until TOTIMEP is reached. The logic for Case 1, above, is then applied.
3. Loads at temperatures (or both) vary with time.	The loads and temperatures must be input at times $T_{1,1}, T_{1,2}, \dots$ until the value $T_{1,n}$ reaches or exceeds the value of TOTIME.



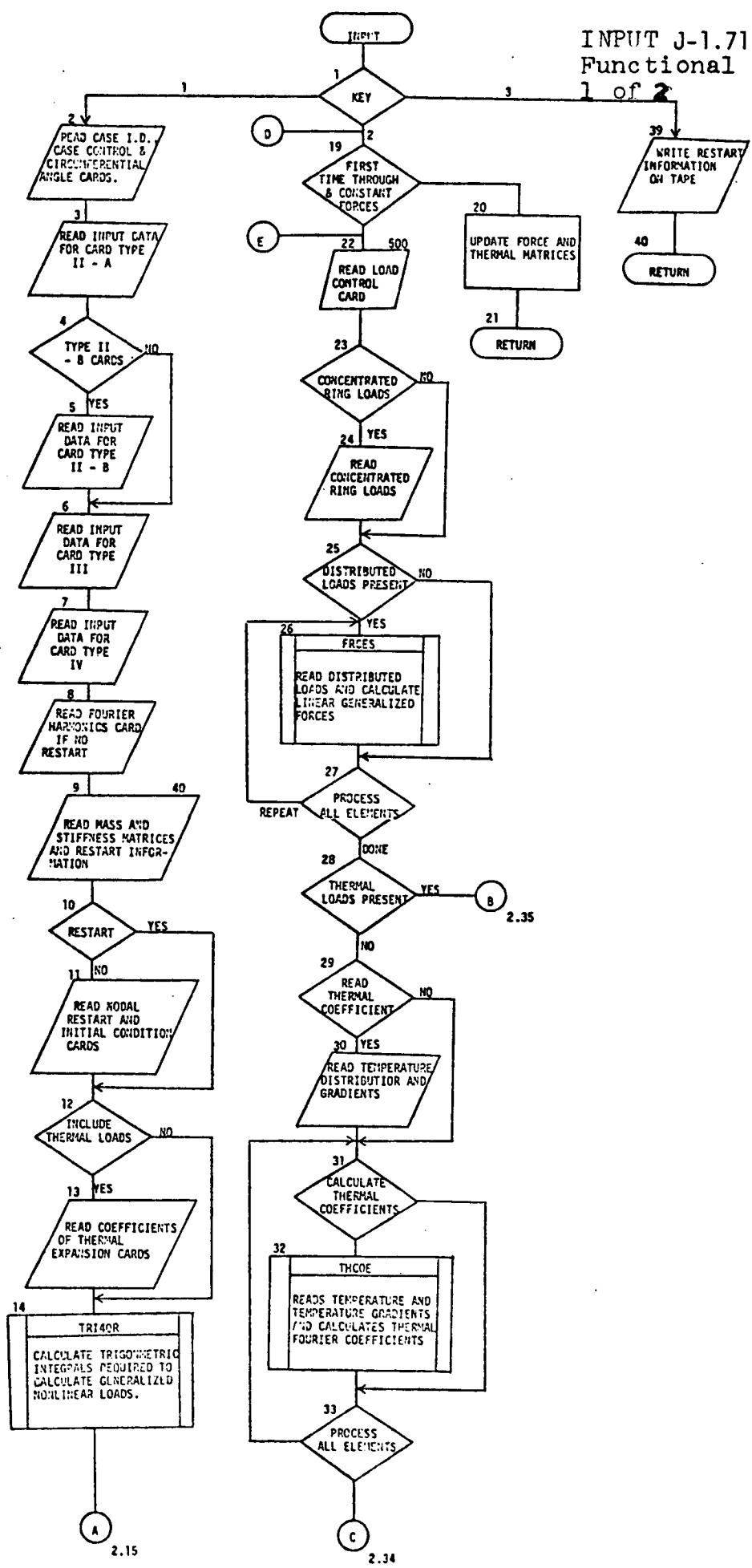


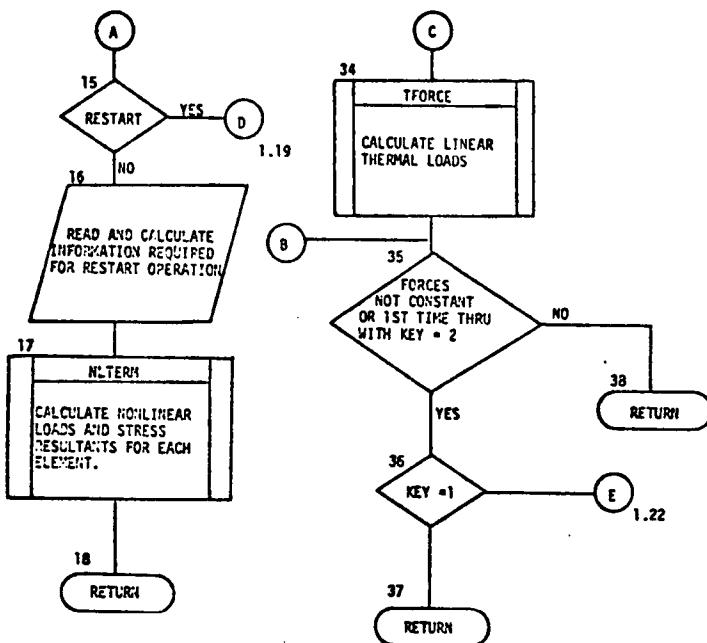
J-1.70

HQBQ1
Functional
1 of 1

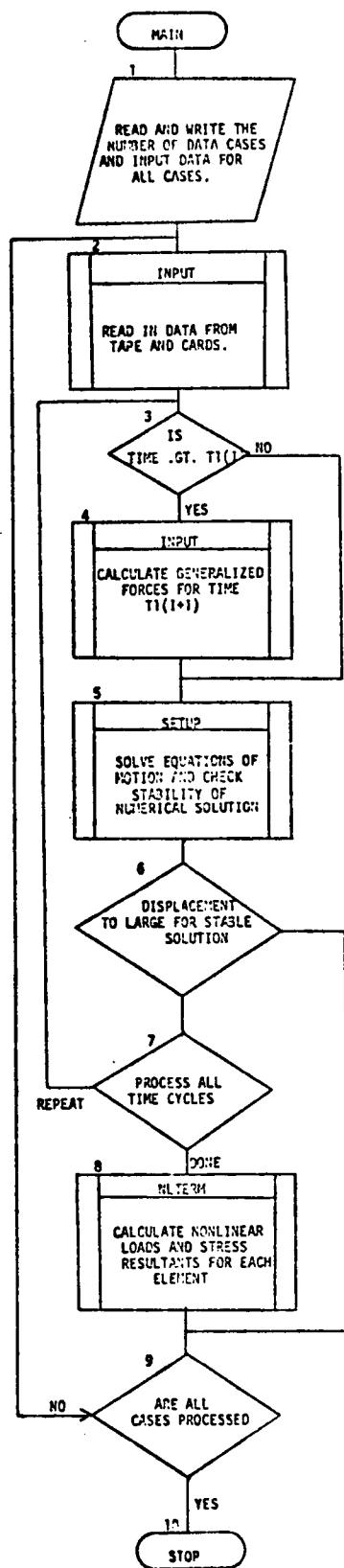


INPUT J-1.71
Functional
1 of 2



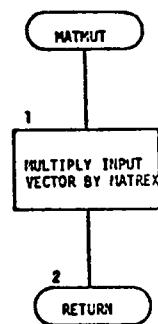


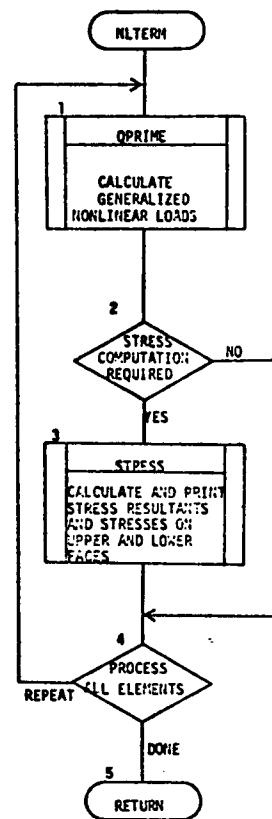
MAIN J-1.73
Functional
1 of 1

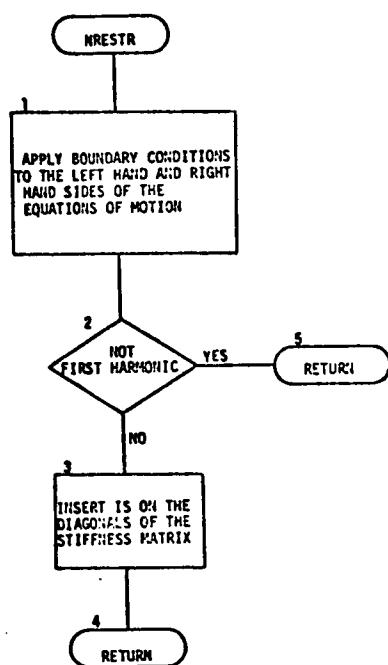


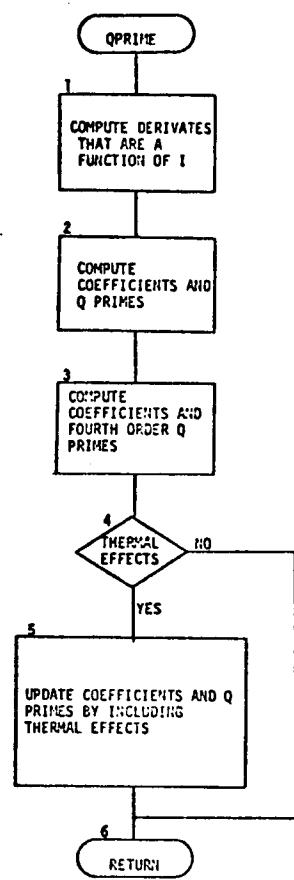
J-1.74

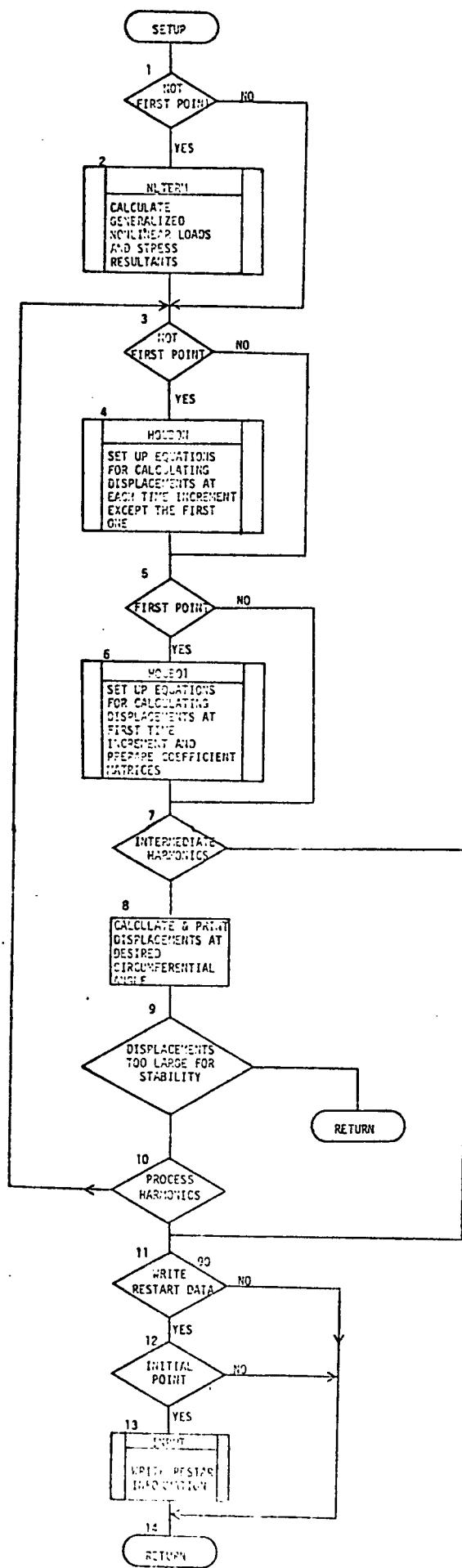
MATMUT
Functional
1 of 1



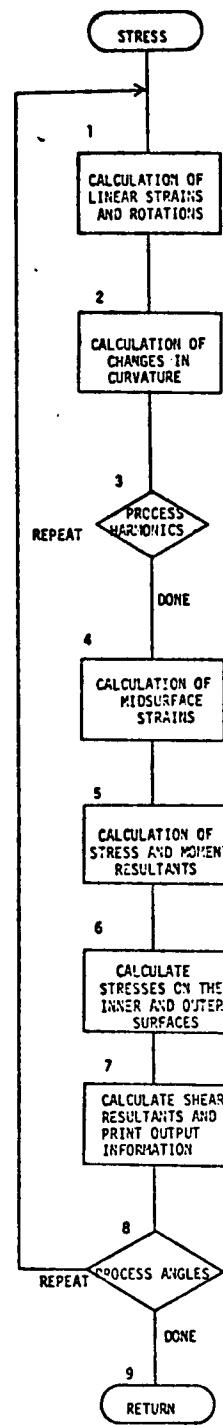


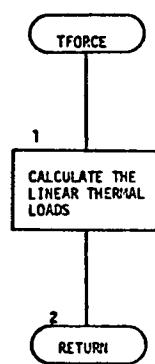


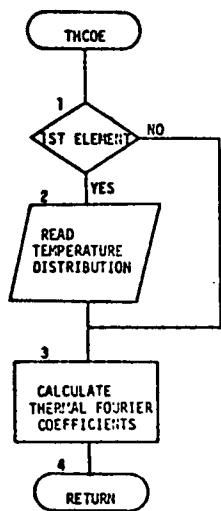


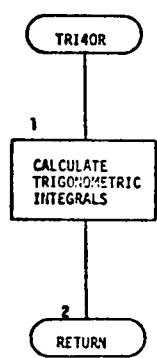












DYNASOR II - A FINITE ELEMENT PROGRAM FOR THE
DYNAMIC NONLINEAR ANALYSIS OF SHELLS OF REVOLUTION

Joe R. Tillerson and Walter E. Haisler

OPERATION MANUAL

October 15, 1970

TEES-RPT-70-19

Texas A&M University
College Station, Texas

J-2-1

ABSTRACT

The DYNASOR II program is used for the DYnamic Nonlinear Analysis of Shells Of Revolution. The equations of motion of the shell are solved using Houbolt's numerical procedure. The displacements and stress resultants can be determined for both symmetrical and asymmetrical loading conditions. Asymmetrical dynamic buckling can be investigated. Solutions can be obtained for highly nonlinear problems utilizing as many as five of the harmonics generated by SAMMSOR program. A restart capability allows the user to restart the program at a specified time.

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SOR - Shell Of Revolution**Computer Programs**

A family of compatible computer codes for the analysis of the shell of revolution (SOR) structures has been developed by researchers at Texas A&M University. These analyses employ the matrix displacement method of structural analysis utilizing a curved shell element. Geometrically nonlinear static and dynamic analyses can be conducted using these codes. The important natural frequencies and mode shapes can also be determined by employing another of the codes. Efficient programming provides codes capable of performing these desired analyses in relatively small amounts of computer time.

Each of these programs has been extensively tested using problems the solutions to which have been reported by other researchers in order to establish the validity of the codes. In addition, the capabilities of the codes have been demonstrated in a number of publications by presenting solutions to problems which were unsolved by other researchers.

SAMMSOR II - Stiffness And Mass Matrices for Shells Of Revolution are generated utilizing the first member of this family. This program accepts a description of the structure in terms of the coordinates and slopes of the nodes and the properties of the elements joining the nodes. For shells with simple geometries (such as cylinders, shallow caps, hemispheres, etc.) the shell geometry can be internally generated. Utilizing the element properties, the structural stiffness and mass matrices are generated for as many as twenty harmonics and stored on magnetic tape. Each of the other SOR programs utilizes the output tape generated by SAMMSOR as input data for the respective analyses. One advantage of creating the stiffness and mass matrices in a separate program is that a variety of analyses can be performed on the same shell configuration without having to create the matrices more than once. Obviously, a variety of boundary and loading conditions can be employed without having to create new mass and stiffness matrices for each case.

SNASOR II - The Static Nonlinear analysis of Shells Of Revolution subjected to arbitrary mechanical and thermal loading is performed using the second computer code. Utilizing the stiffness matrices generated by SAMMSOR and the loading conditions and boundary conditions input to SNASOR II, the equilibrium equations for the structure are generated. The nonlinear strain energy terms result in pseudo generalized forces (as functions of the displacements) which are combined with the applied generalized forces. The resulting set of nonlinear algebraic equilibrium equations is solved by one of several methods: Newton-Raphson

J-2.4

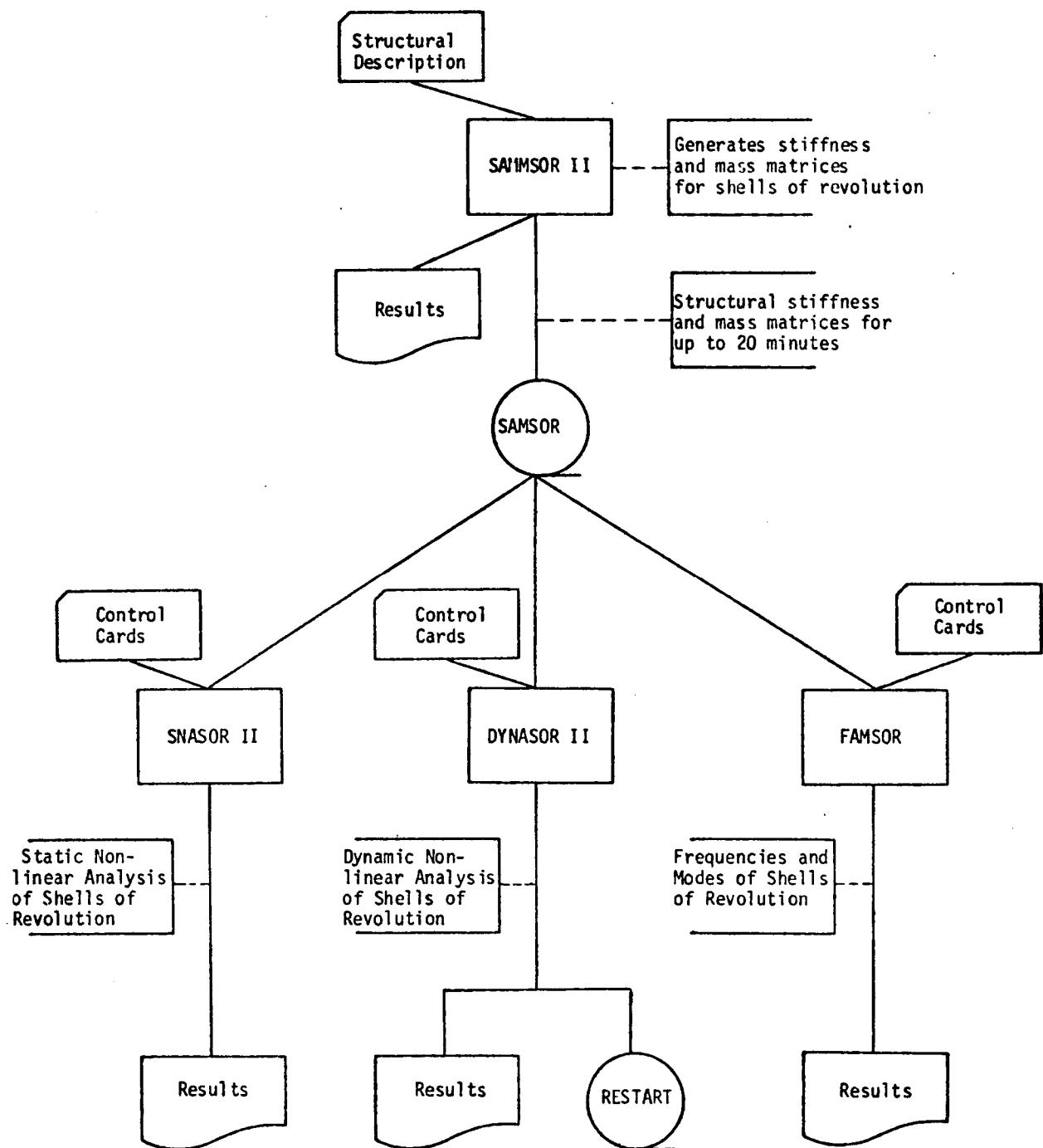
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type iteration, incremental stiffness method, or a modified incremental stiffness method. In general, the Newton-Raphson procedure is the best and yields accurate results for highly nonlinear problems.

DYNASOR II - The third code is used for the Dynamic Nonlinear Analysis of Shells Of Revolution. The equations of motion of the shell are solved using Houbolt's numerical procedure with the nonlinear terms being moved to the right-hand side of the equilibrium equations and again treated as generalized loads. The displacements and stress resultants can be determined for both symmetrical and asymmetrical loading conditions. Asymmetrical dynamic buckling can be investigated using this program. Solutions can be obtained for highly nonlinear problems in reasonable periods of time on the computer utilizing as many as five of the harmonics generated in SAMMSOR. A restart capability is incorporated in this code which allows the user to restart the program at a specified time without having to expend the computer time necessary to regenerate the prior response.

FAMSOR - Frequencies And Modes for Shells Of Revolution can be determined using the fourth code. Using the stiffness matrix generated by SAMMSOR and a lumped mass representation developed from the consistent mass matrix generated by SAMMSOR, a specified number of natural frequencies (beginning with the lowest or fundamental frequency) are obtained using the inverse iteration method. The mode shapes for each of the frequencies are also obtained.

SYSTEM FLOWCHART



ENVIRONMENT

The DYNASOR II program runs under OS/360 MFT or MVT and requires 220K of memory on an IBM S/360 computer. The system must also have a card reader, printer, 3 9-track tape drives and 2314 disk storage.

SYSTEM OPERATION

A. Run Characteristics

- 1). Functional description of run
(see abstract)
- 2). Relationship to other runs
(see system flowchart)
- 3). Set-up and run instructions
 - a. get SAMMSOR output tape
 - b. 2 scratch tapes
 - c. punch control cards
 - d. fill out job ticket
 - e. load job
- 4). Run frequency
when desired
- 5). Run prerequisites
SAMMSOR
- 6). Run control
none
- 7). Run schedule
no set schedule; run when desired or on demand
- 8). External procedures
none

B.

MACHINE SET UP FORM

PROG NAME DYNASOR PROG # _____ USER I.D. CODE _____
AREA Aerospace Engr. PROJECT _____ PROGRAMMER Haisler
JOB PREQ SAMMOSR REGION SIZE 110K K

DIRECT ACCESS REQUIREMENTS: none

PERMANENT

TEMPORARY none

TAPE REQUIREMENTS:

#7 TRK. UNITS 0 #9 TRK. UNITS 3

(FOR ADDITIONAL INFORMATION ATTACH ANOTHER SHEET)

ADDITION **REPLACEMENT**

DATE _____ SECTION _____ PAGE _____

CARD READER REQUIREMENTS: SYSIN

DATA SET NAME	DDNAME	SOURCE	DISPOSITION

CARD PUNCH REQUIREMENTS: none

DATA SET NAME	DDNAME	POCKET #	DISPOSITION

PRINTER REQUIREMENTS: SYSPRINT

DATA SET NAME	DDNAME	PRINT TRAIN	FORM #	SETUP #	LINES PER INCH	BURST	DECOL-LATE	DISPOSITION

ADDITION REPLACEMENT

DATE _____ SECTION _____ PAGE _____

C. File Information Sheet

date of last update

name: SAMSOR

system or application: DYNASOR

description of contents and use: stiffness and mass matrices for
up to 20 harmonies; input to DYNASOR II program

storage medium: tape

record characteristics: Fortran output, variable length records

block characteristics: 7200 byte blocks, spanned

file activity: (approximate when necessary)

- not a permanently maintained file
- created when computing shells of revolution
- restart information written on tape by DYNASOR run.

CL

D. Job Control Language

```
//DYNASR      JØB(_____,_____,_____)  
/*CLASS  
//JØBLIB      DD          DSNAME=USER.DYNASØR.JØBLIB,DISP=SHR  
//DYNASØR      EXEC        PGM=DYNASØR  
//FT01F005     DD          DDNAME=SYSIN  
//FT01F006     DD          SYSØUT=A  
//FT01F007     DD          SYSØUT=B  
//FT01F008     DD          UNIT=2400,DISP=(ØLD,KEEP),DSNAME=SAMSØRIN,  
//                           DCB=(RECFM=VBS,BLØCKSIZE=7200),VØL=SER=SAMSØI  
//FT01F009     DD          UNIT=2400,DISP=(NEW,DELETE),DCB=(RECFM=VBS,  
//                           BLØCKSIZE=7200),VØL=SER=DYNSR1  
//FT01F010     DD          UNIT=2400,DISP=(NEW,DELETE),DCB=(RECFM=VBS,  
//                           BLØCKSIZE=7200),VØL=SER=DYNSR2  
//SYSIN        DD          *  
.*.  
.*. CONTROL CARDS  
.*.  
/*
```

E. RUN CONTROL CARDS

Card Type I

Columns	Variable	Type
1-5	NCASES	Numeric
6-10	ND	Numeric
11-15	NS	Numeric

Card Type II-A

Columns	Variable	Type
1-5	NCARDS	Numeric
6-10	NT	Numeric

Card Type II-B

Columns	Variable	Type
1-80	COMENT	Alphanumeric

Card Type III-A

Columns	Variable	Type
1-10	TOTIME	Numeric
11-20	DELTE	Numeric
21-25	IRSTRT	Numeric
26-30	INCRST	Numeric
31-35	NCLOSE	Numeric
36-40	ITELF	Numeric

RUN CONTROL CARDS

Card Type III-B

Columns	Variable	Type
1-5	NPRNTQ	Numeric
6-10	IPRINT	Numeric
11-15	NCLCST	Numeric
16-20	NSTRSS	Numeric
21-25	NPRNT	Numeric
26-30	NPRNIT	Numeric
31-35	NPRNLT	Numeric
36-40	NPRNTF	Numeric
41-45	NPRNTH	Numeric
46-50	NPRNMS	Numeric

Card Type IV-A

Columns	Variable	Type
1-5	NTHETA	Numeric

Card Type IV-B

Columns	Variable	Type
1-10	THETA(1)	Numeric
11-20	THETA(2)	Numeric
"	"	
"	THETA (NTHETA)	

Card Type V

Columns	Variable	Type
1-5	NH	Numeric

RUN CONTROL CARDS

Card Type V (Continued)

Columns	Variable	Type
6-10	IHARM(1)	Numeric
11-15	IHARM(2)	
16-20	IHARM(3)	
21-25	IHARM(4)	
26-30	IHARM(5)	

Card Type VI-A

Columns	Variable	Type
1-5	NODRES	Numeric

Card Type VI-B

Columns	Variable	Type
1-5	NP	Numeric
6-10	NDIRCT	Numeric

Card Type VII-A

Columns	Variable	Type
1-5	IQN	Numeric
6-10	IQN1	Numeric

Card Type VII-B

Columns	Variable	Type
1-5	IN1	Numeric
6-10	IN2	Numeric

RUN CONTROL CARDS

Card Type VII-B (Continued)

Columns	Variable	Type
11-20	\dot{q}_1	Numeric
21-30	\dot{q}_2	Numeric
31-40	\dot{q}_3	Numeric
41-50	\dot{q}_4	Numeric

Card Type VII-C

Columns	Variable	Type
1-5	IN1	Numeric
6-10	IN2	Numeric
11-20	\dot{q}_1	Numeric
21-30	\dot{q}_2	Numeric
31-40	\dot{q}_3	Numeric
41-50	\dot{q}_4	Numeric

Card Type VIII

Columns	Variable	Type
1-5	IELM1	Numeric
6-10	IELM2	Numeric
11-20	ALSI1	Numeric
21-30	ALTI1	Numeric

Card Type IX-A

Columns	Variable	Type
1-10	T1	Numeric

RUN CONTROL CARDS

Card Type IX-A (Continued)

Columns	Variable	Type
11-15	NCF	Numeric
16-20	IDELF	Numeric
21-25	IDCOE	Numeric
26-30	ITCOE	Numeric
31-38	CONSTF	Alphanumeric

Card Type IX-B-1

Columns	Variable	Type
1-5	NCF1	Numeric

Card Type IX-B-2

Columns	Variable	Type
1-5	IN1	Numeric
6-10	IN2	Numeric
11-20	F1	Numeric
21-30	F2	Numeric
31-40	F3	Numeric
41-50	F4	Numeric

Card Type IX-C-1-a

Columns	Variable	Type
1-5	IELM1	Numeric
6-10	IELM2	Numeric
11-15	NDP	Numeric

RUN CONTROL CARDS

Card Type IX-C-1-b

Columns	Variable	Type
1-10	THETB	Numeric
11-20	P	Numeric
21-30	R	Numeric
31-40	S	Numeric

Card Type IX-C-2-a

Columns	Variable	Type
1-5	IELM1	Numeric
6-10	IELM2	Numeric

Card Type IX-C-2-b

Columns	Variable	Type
1-10	P	Numeric
11-20	R	Numeric
21-30	S	Numeric

Card Type IX-D-1-a

Columns	Variable	Type
1-5	IELM1	Numeric
6-10	IELM2	Numeric
11-15	NDP	Numeric

Card Type IX-D-1-b

Columns	Variable	Type
1-10	THETB	Numeric
11-20	P	Numeric
21-30	R	Numeric

RUN CONTROL CARDS

Card Type IX-D-2-a

Columns	Variable	Type
1-5	IELM1	Numeric
6-10	IELM2	Numeric

Card Type IX-D-2-b

Columns	Variable	Type
1-10	TH1	Numeric
11-20	DTH1	Numeric

Card Type X

Columns	Punch
1-11	END OF CASE

Card Type XI

Columns	Punch
1-10	END OF RUN

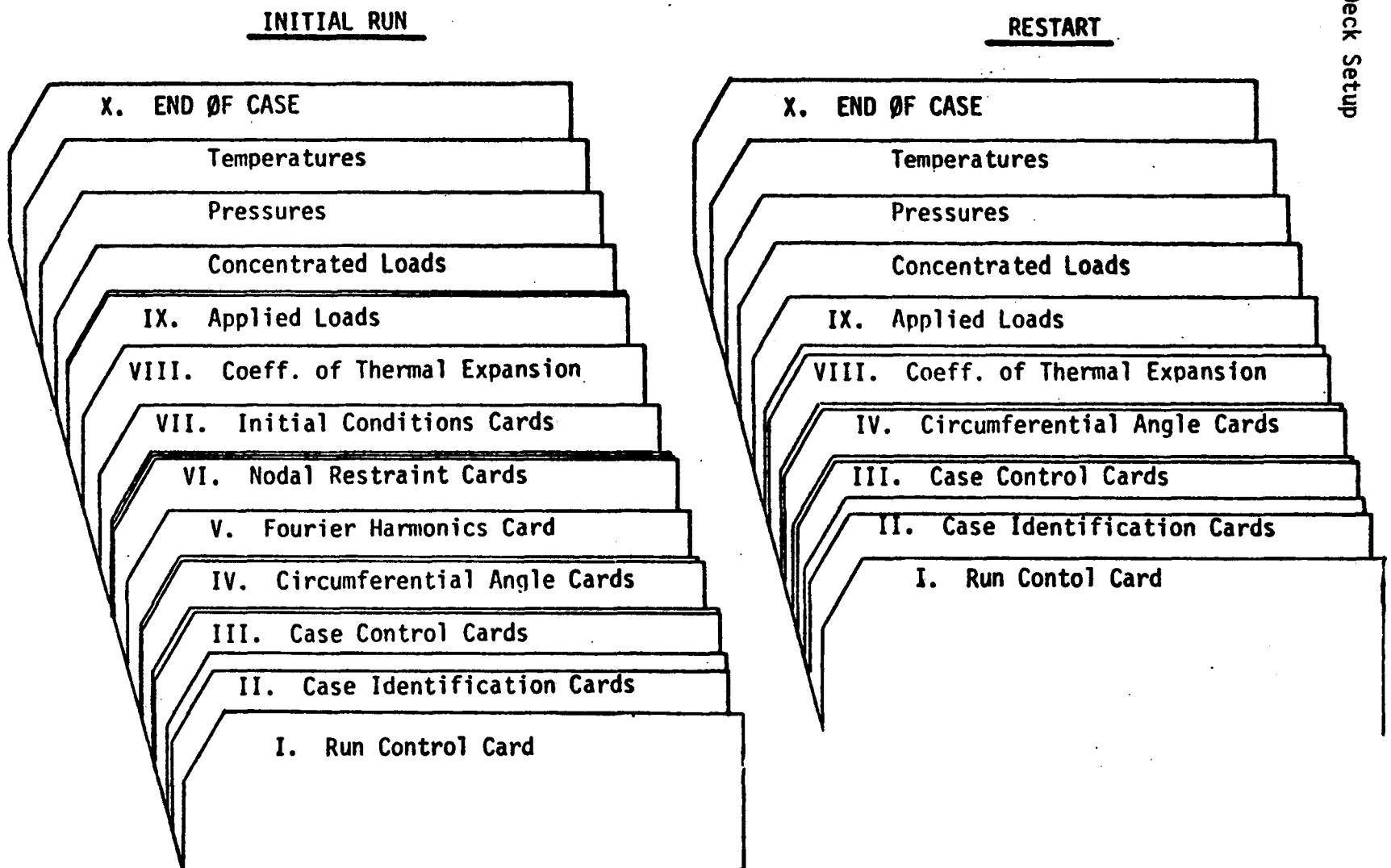
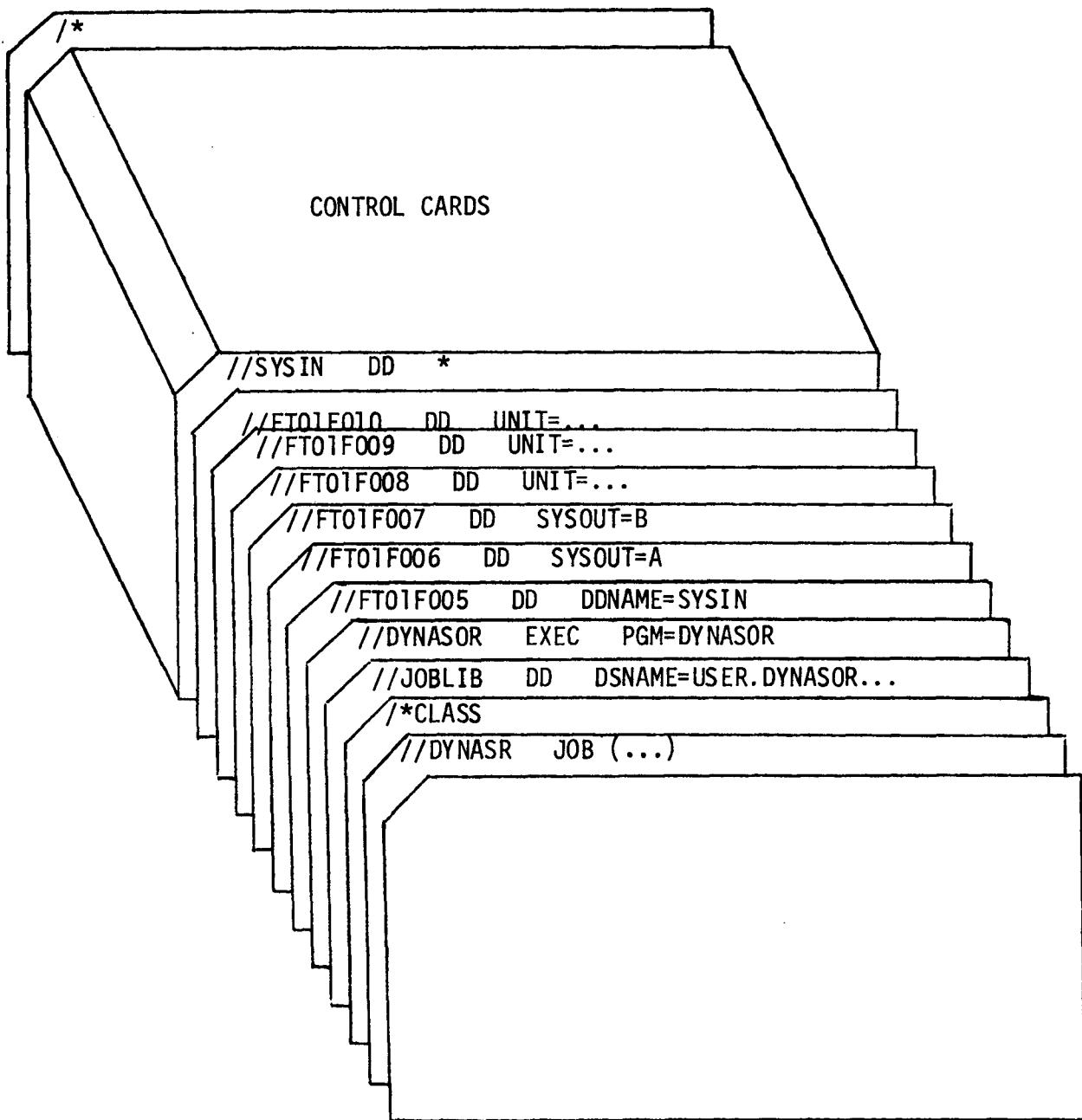


FIG. 1 CONSTITUTION OF DATA DECKS - INITIAL RUN AND RESTART MODES.

DECK SETUP FOR DYNASOR II



G. 360 MESSAGE FORM

DATE _____

ADDITION [] REPLACEMENT []

[] OPERATIONAL

[] ADMINISTRATIVE

Jobname _____ PROGRAMMER _____ MSG ID _____

MESSAGE: The number of input cases does not agree with the value of
ncases input

MEANING:

ACTION:

360 MESSAGE FORM

DATE _____

ADDITION [] REPLACEMENT []

[] OPERATIONAL

[] ADMINISTRATIVE

Jobname _____ PROGRAMMER _____ MSG ID _____

MESSAGE: Restart information for time increment no., I5,/,10X, corresponding
to time, F12.4, microseconds,/,2X, has been placed on tape for use
in subsequent runs//

MEANING:

ACTION:

360 MESSAGE FORM

DATE _____

ADDITION [] REPLACEMENT []

[] OPERATIONAL

[] ADMINISTRATIVE

Jobname _____ PROGRAMMER _____ MSG ID _____

MESSAGE: ITAM, I5, 5X time, E 12.5 Execution terminated - displacements
greater than 1.E + 4

MEANING:

ACTION:

H. CHECKPOINT, RESTART, ERROR PROCEDURES, BACKUP, AND RECOVERY PROCEDURES

Recovery Procedures:

If many computations are to be done, a backup copy of the SAMMSOR input and restart tape can be made. Otherwise, no backup is required.

Restart Procedures:

To restart DYNASOR program, set IRSTRT = 1 on control card type III-A. Use SAMMSOR input tape. Restart information was written onto this tape in the previous run.

DYNASOR II - A FINITE ELEMENT PROGRAM FOR THE
DYNAMIC NONLINEAR ANALYSIS OF SHELLS OF REVOLUTION

Joe R. Tillerson and Walter E. Haisler

MAINTENANCE MANUAL

October 15, 1970

TEES-RPT-70-19
Texas A&M University
College Station, Texas

J-3-1

ABSTRACT

The DYNASOR II program is used for the DYnamic Nonlinear Analysis of Shells Of Revolution. The equations of motion of the shell are solved using Houbolt's numerical procedure. The displacements and stress resultants can be determined for both symmetrical and asymmetrical loading conditions. Asymmetrical dynamic buckling can be investigated. Solutions can be obtained for highly nonlinear problems utilizing as many as five of the harmonics generated by SAMMSOR program. A restart capability allows the user to restart the program at a specified time.

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SYSTEM OVERVIEW

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SOR - Shell Of Revolution

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Computer Programs

A family of compatible computer codes for the analysis of the shell of revolution (SOR) structures has been developed by researchers at Texas A&M University. These analyses employ the matrix displacement method of structural analysis utilizing a curved shell element. Geometrically nonlinear static and dynamic analyses can be conducted using these codes. The important natural frequencies and mode shapes can also be determined by employing another of the codes. Efficient programming provides codes capable of performing these desired analyses in relatively small amounts of computer time.

Each of these programs has been extensively tested using problems the solutions to which have been reported by other researchers in order to establish the validity of the codes. In addition, the capabilities of the codes have been demonstrated in a number of publications by presenting solutions to problems which were unsolved by other researchers.

SAMMSOR II - Stiffness And Mass Matrices for Shells Of Revolution are generated utilizing the first member of this family. This program accepts a description of the structure in terms of the coordinates and slopes of the nodes and the properties of the elements joining the nodes. For shells with simple geometries (such as cylinders, shallow caps, hemispheres, etc.) the shell geometry can be internally generated. Utilizing the element properties, the structural stiffness and mass matrices are generated for as many as twenty harmonics and stored on magnetic tape. Each of the other SOR programs utilizes the output tape generated by SAMMSOR as input data for the respective analyses. One advantage of creating the stiffness and mass matrices in a separate program is that a variety of analyses can be performed on the same shell configuration without having to create the matrices more than once. Obviously, a variety of boundary and loading conditions can be employed without having to create new mass and stiffness matrices for each case.

SNASOR II - The Static Nonlinear analysis of Shells Of Revolution subjected to arbitrary mechanical and thermal loading is performed using the second computer code. Utilizing the stiffness matrices generated by SAMMSOR and the loading conditions and boundary conditions input to SNASOR II, the equilibrium equations for the structure are generated. The nonlinear strain energy terms result in pseudo generalized forces (as functions of the displacements) which are combined with the applied generalized forces. The resulting set of nonlinear algebraic equilibrium equations is solved by one of several methods: Newton-Raphson

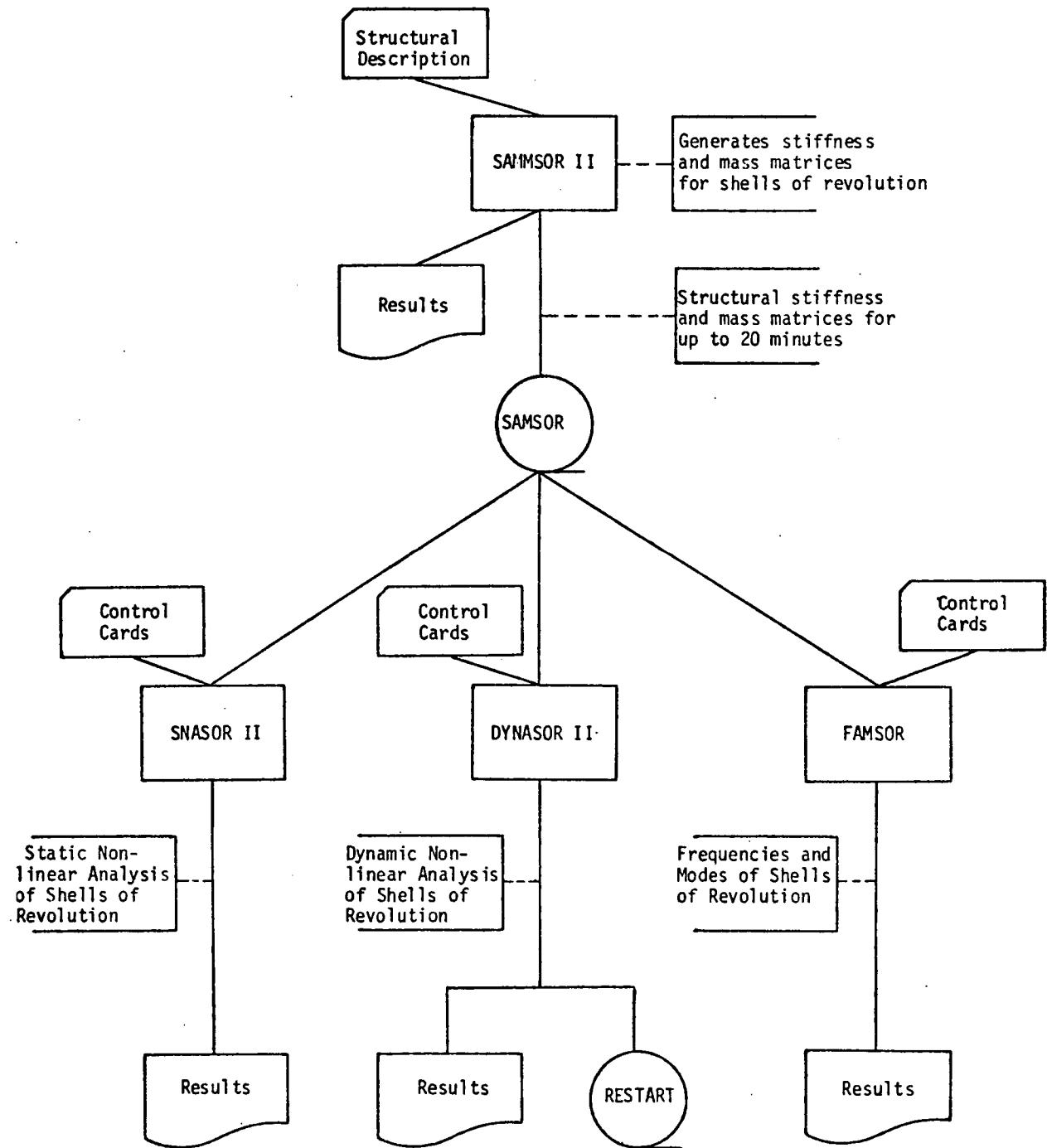
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type iteration, incremental stiffness method, or a modified incremental stiffness method. In general, the Newton-Raphson procedure is the best and yields accurate results for highly nonlinear problems.

DYNASOR II - The third code is used for the Dynamic Nonlinear Analysis of Shells Of Revolution. The equations of motion of the shell are solved using Houbolt's numerical procedure with the nonlinear terms being moved to the right-hand side of the equilibrium equations and again treated as generalized loads. The displacements and stress resultants can be determined for both symmetrical and asymmetrical loading conditions. Asymmetrical dynamic buckling can be investigated using this program. Solutions can be obtained for highly nonlinear problems in reasonable periods of time on the computer utilizing as many as five of the harmonics generated in SAMMSOR. A restart capability is incorporated in this code which allows the user to restart the program at a specified time without having to expend the computer time necessary to regenerate the prior response.

FAMSOR - Frequencies And Modes for Shells Of Revolution can be determined using the fourth code. Using the stiffness matrix generated by SAMMSOR and a lumped mass representation developed from the consistent mass matrix generated by SAMMSOR, a specified number of natural frequencies (beginning with the lowest or fundamental frequency) are obtained using the inverse iteration method. The mode shapes for each of the frequencies are also obtained.

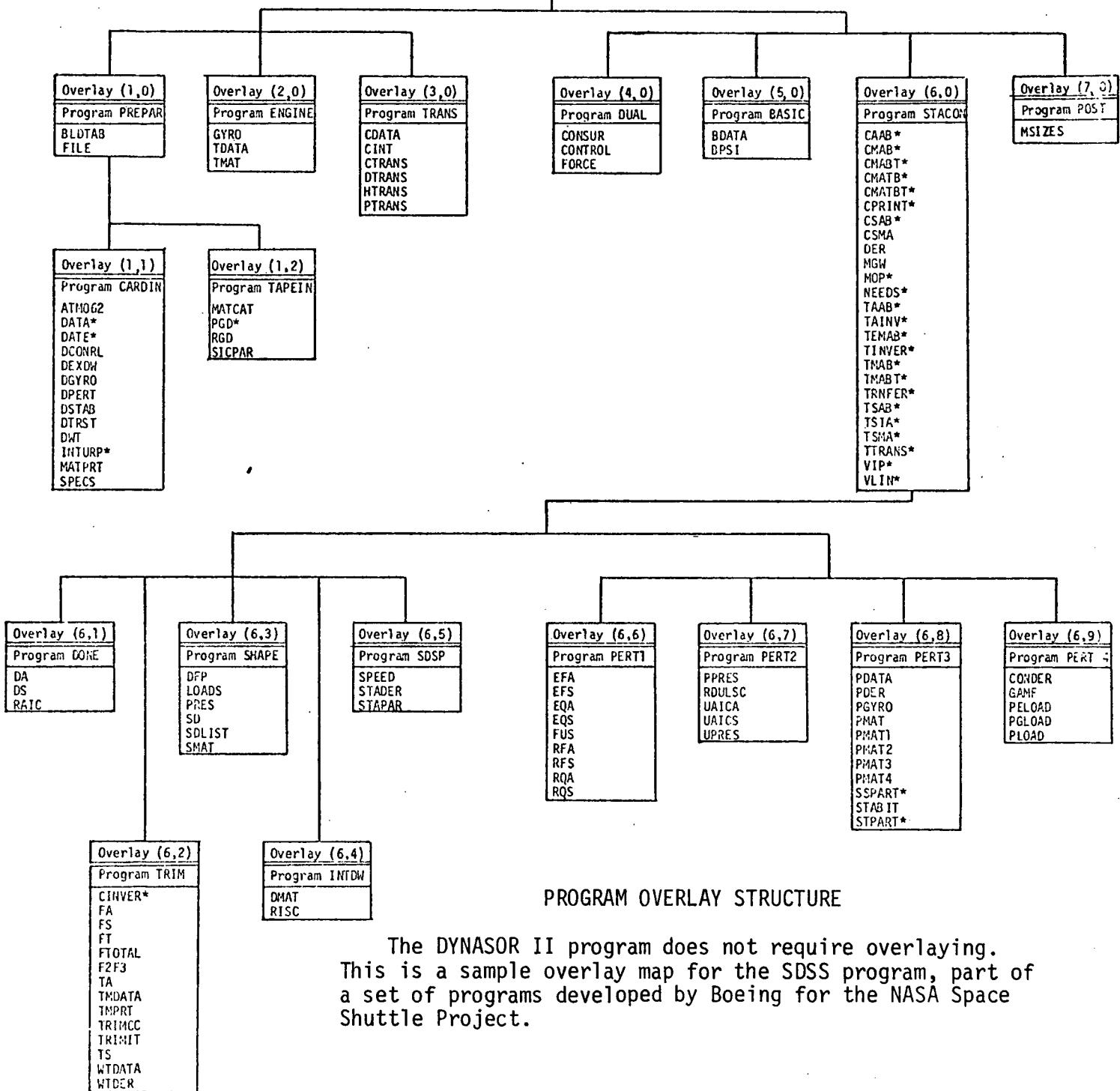
SYSTEM FLOWCHART

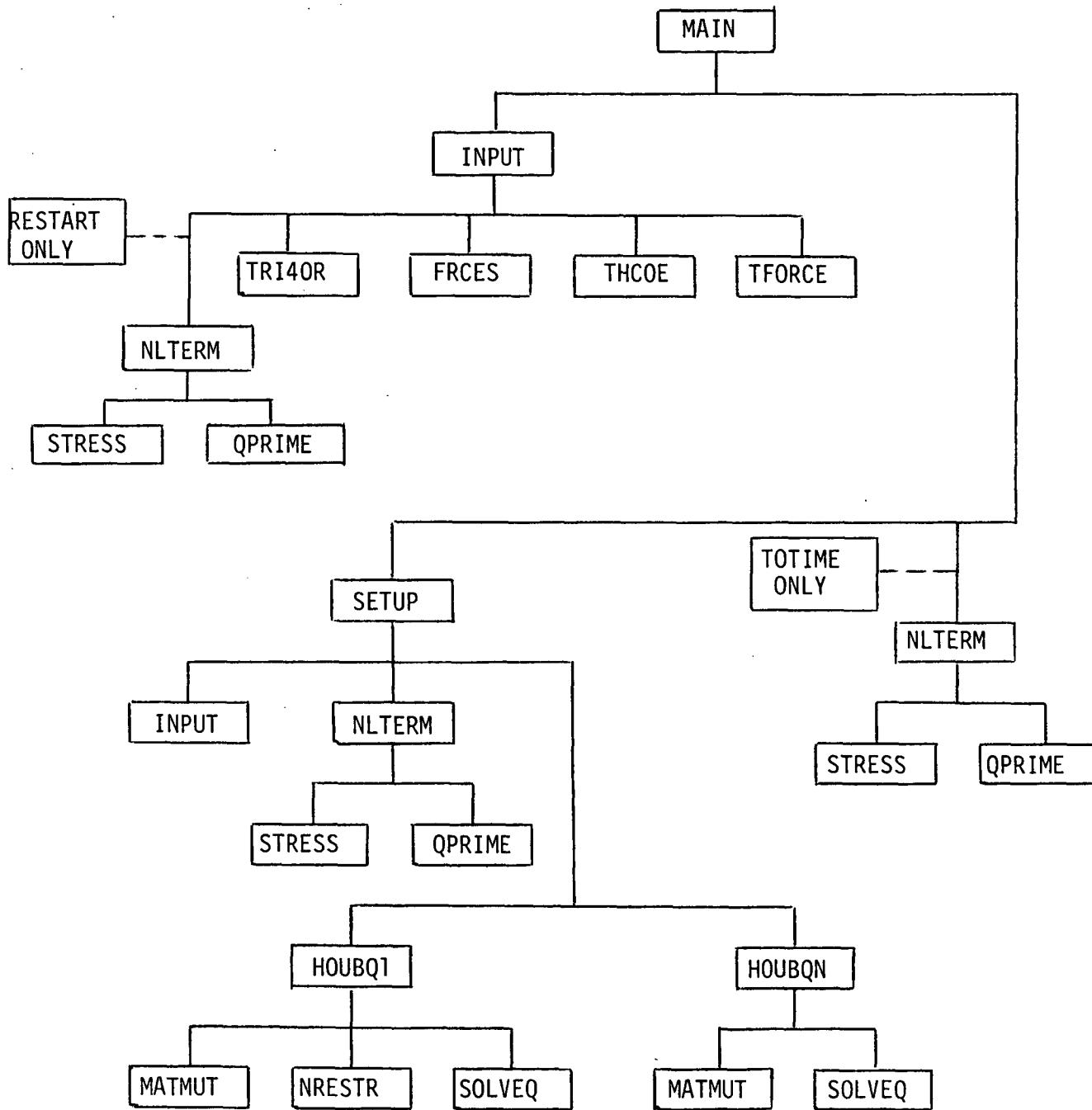


ENVIRONMENT

The DYNASOR II program runs under OS/360 MFT or MVT and requires 220K of memory on an IBM S/360 computer. The system must also have a card reader, printer, 3 9-track tape drives and 2314 disk storage.

Overlay (0,0)	
Program SDSS	
CLSRAT*	RELES*
CLRTAB*	RHEAD*
COPYM*	RVEC*
CREATE*	STATUS*
DMPTAB*	STOREM*
FETCHM*	SURFIN*
FIND*	TPRINT*
INITL	UREWIND*
IOUNTS	UTABUP*
LINEIN*	WHEAD*
LOCATE*	WSVEC*
MONITR	WVEC*
OPTFIL*	WVSVEC*
PNAME*	ZERO*





SUBROUTINE CALL DIAGRAM

FORTRAN IV G LEVEL 20

MAIN

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```

CE(FRCES)                               DYN14872
C                                         DYN14874
C     DESCRIPTION - TO READ IN THE DISTRIBUTED LOADS ON THE SHELL   DYN14876
C             STRUCTURE. THEN, USING EITHER CIRCUMFERENTIAL OR          DYN14878
C             FOURIER COEFFICIENTS DATA, CALCULATE THE LINEAR           DYN14880
C             GENERALIZED LOADS.                                       DYN14882
C                                         DYN14884
C     INPUT ARGUMENTS.                                              DYN14886
C         IB      = FORCE ARRAY STEPPING PARAMETER, USED TO MODIFY CURRENT DYN14888
C                     BLOCK OF STORAGE FOR FORCE.                      DYN14890
C         IELM    = NUMBER OF SHELL ELEMENTS.                         DYN14892
C                                         DYN14894
C     OUTPUT ARGUMENTS.                                             DYN14896
C         FORCE   = MATRIX OF GENERALIZED FORCES DUE TO EXTERNAL LOADS AND DYN14898
C                     TEMPERATURES.                                DYN14900
C         Q       = THERMAL COEFFICIENTS USED IN CALCULATING GENERALIZED DYN14902
C                     LINEAR LOADS DUE TO THERMAL EFFECTS.            DYN14904
C         QQ      = GENERALIZED LINEAR LOADS DUE TO THERMAL EFFECTS. DYN14906
C                                         DYN14908
C     EXTERNALS.                                                 DYN14910
C     CALLED BY
C         INPUT
C                                         DYN14912
C                                         DYN14914
C                                         DYN14916
0001   SUBROUTINE FRCES (IELM,ALPHK,IB)                           DYN14918
0002   IMPLICIT REAL*8 (A-H,O-Z)                                 DYN14920
0003   COMMON /FRCE/ P(74),R(74),S(74),THETB(74)                DYN14922
0004   COMMON /CHALS/ AL(167),CHECK(8,8)                          DYN14924
0005   COMMON /QS/ QN(1020),QN1(1020),FORCE(2040),QP(1020),QPI(1020), DYN14926
0006   1      QN2(1020)
0006   COMMON /CONST/ NH,NELEMS,NNODES,NSIZE,NPRNTQ,NEQ,NEQT,N,NN,NHNS, DYN14930
0006   1      DT2,NPRNTL,NPRNTF,IDEL,FIDCOE                      DYN14940
0007   COMMON /HARM/ NHP,IHARM(5)                                DYN14950
0008   COMMON /QUES/ Q(8),QQ(8)                                  DYN14960
0009   COMMON /TAPES/ NT,ND,NS                                  DYN14970
C1     READ DISTRIBUTED LOADS USING CIRCUMFERENTIAL ANGLES OR FOURIER DYN14972
C1C    COEFFICIENTS                                         DYN14974
0010   PI=3.14159265                                         DYN15020
0011   IF (IELM.EQ.1) IELM2=0                                 DYN15030
0012   IF (IELM.LE.IELM2.AND.IELM.NE.1) GO TO 40              DYN15040
0013   IF (ICCOE.NE.1) GO TO 10                            DYN15050
0014   IF (NPRNTL.EQ.1.AND.IELM.EQ.1) WRITE (6,160)           DYN15060
0015   C     READ INPUT DATA FOR CARD TYPE IX - C - 2          DYN15070
0015   READ (ND,170) IELM1,IELM2,(P(I),R(I),S(I),I=1,NH)        DYN15080
0016   IF (NPRNTL.EQ.1) WRITE (6,180) IELM1,IELM2,(P(I),R(I),S(I),I,I=1, DYN15090
0016   1      NH)                                           DYN15100
0017   GO TO 40                                            DYN15110
0018   10 CONTINUE                                         DYN15120
0019   IF (NPRNTL.EQ.1.AND.IELM.EQ.1) WRITE (6,190)           DYN15130

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C     READ DISTRIBUTED LOADS          DYN15140
C
C     READ INPUT DATA FOR CARD TYPE IX - C - 1          DYN15150
C     READ (ND,200) IELM1,IELM2,NDP,(THETB(I),P(I),R(I),S(I),I=1,NDP)  DYN15160
C     NDP2=2*NDP+1          DYN15170
C
C     DO 20 IF=1,NDP          DYN15180
C     ANG=360.0-THETB(IF)          DYN15188
C     KEY=NDP2-IF          DYN15190
C     THETB(KEY)=ANG          DYN15200
C     P(KEY)=P(IF)          DYN15210
C     R(KEY)=R(IF)          DYN15220
C     S(KEY)=S(IF)          DYN15230
C
C     20 CONTINUE          DYN15240
C
C     IF (NPRNTL.EQ.1) WRITE (6,21C) IELM1,IELM2,(P(I),R(I),S(I),
C     1           THETB(I),THETB(I+1),I=1,NDP)          DYN15250
C     ND2=2*NDP          DYN15260
C     NDPP2=NDP+2          DYN15263
C     IF (NPRNTL.EQ.1.AND.NDP.GT.1) WRITE (6,220) (P(I),R(I),S(I),
C     1           THETB(I-1),THETB(I),I=NDPP2,ND2)          DYN15270
C
C     DO 30 IDP=1,ND2          DYN15280
C     THETB(IDP)=THETB(IDP)/57.2957795          DYN15290
C
C     30 CONTINUE          DYN15300
C
C     C1     CALCULATE THE LINEAR GENERALIZED LOADS          DYN15310
C
C     40 CONTINUE          DYN15320
C
C     DO 150 IH=1,NH          DYN15328
C     KYP=IHARM(IH)          DYN15330
C     YKP=KYP          DYN15340
C     IF (IDCOE.EQ.1) GO TO 110          DYN15342
C
C     DO 50 I=1,8          DYN15348
C     Q(I)=0.0          DYN15350
C
C     50 CONTINUE          DYN15358
C
C     NDP1=2.0*NDP-1          DYN15360
C
C     DO 100 I=1,NDP1          DYN15370
C     IF (NDP.EQ.1) GO TO 70          DYN15380
C     X1=THETB(I)*YKP          DYN15390
C     X2=THETB(I+1)*YKP          DYN15398
C     IF (KYP.GT.0) GO TO 60          DYN15400
C     PINT=P(I)*(THETB(I+1)-THETB(I))          DYN15410
C     RINT=R(I)*(THETB(I+1)-THETB(I))          DYN15412
C     SINT=0.0          DYN15415
C
C     100 CONTINUE          DYN15420
C
C     DO 150 IH=1,NH          DYN15428
C     KYP=IHARM(IH)          DYN15430
C     YKP=KYP          DYN15440
C     IF (IDCOE.EQ.1) GO TO 110          DYN15450
C     X1=THETB(I)*YKP          DYN15460
C     X2=THETB(I+1)*YKP          DYN15470
C     IF (KYP.GT.0) GO TO 60          DYN15480
C     PINT=P(I)*(THETB(I+1)-THETB(I))          DYN15490
C     RINT=R(I)*(THETB(I+1)-THETB(I))          DYN15500
C
C     150 CONTINUE          DYN15500
  
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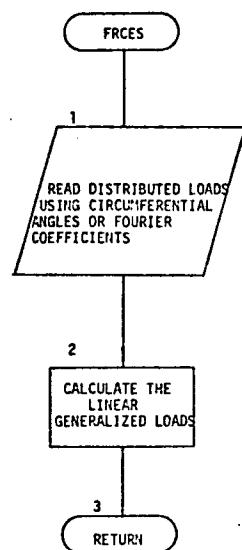
0054      GO TO 90                               DYN15510
0055      60       PINT=P(I)*(DSIN(X2)-DSIN(X1))/YKP   DYN15520
0056      RINT=R(I)*(DSIN(X2)-DSIN(X1))/YKP         DYN15530
0057      SINT=-S(I)*(DCOS(X2)-DCOS(X1))/YKP        DYN15540
0058      GO TO 90                               DYN15550
0059      70       IF (KYP.GT.0) GO TO 80             DYN15560
0060      PINT=2.0*PI*P(1)                      DYN15570
0061      RINT=2.0*PI*R(1)                      DYN15580
0062      SINT=0.0                                DYN15590
0063      GO TO 90                               DYN15600
0064      80       PINT=0.0                          DYN15610
0065      RINT=0.0                          DYN15620
0066      SINT=0.0                          DYN15630
0067      90       Q(1)=Q(1)+RINT*AL(1)          DYN15640
0068      Q(2)=Q(2)+RINT*AL(2)          DYN15650
0069      Q(3)=Q(3)+RINT*AL(3)          DYN15660
0070      Q(4)=Q(4)+RINT*AL(157)        DYN15670
0071      Q(5)=Q(5)+PINT*AL(1)          DYN15680
0072      Q(6)=Q(6)+PINT*AL(2)          DYN15690
0073      Q(7)=Q(7)+SINT*AL(1)          DYN15700
0074      Q(8)=Q(8)+SINT*AL(2)          DYN15710
0075      100      CONTINUE                         DYN15712
C
0076      GO TO 120                         DYN15715
0077      110      CONTINUE                         DYN15720
0078      C12=1.0                            DYN15730
0079      IF (KYP.EQ.0) C12=2.0              DYN15740
0080      PINT=C12*PI*P(IH)                  DYN15750
0081      RINT=C12*PI*R(IH)                  DYN15760
0082      SINT=(2.0-C12)*PI*S(IH)          DYN15770
0083      Q(1)=RINT*AL(1)                  DYN15780
0084      Q(2)=RINT*AL(2)                  DYN15790
0085      Q(3)=RINT*AL(3)                  DYN15800
0086      Q(4)=RINT*AL(157)                DYN15810
0087      Q(5)=PINT*AL(1)                  DYN15820
0088      Q(6)=PINT*AL(2)                  DYN15830
0089      Q(7)=SINT*AL(1)                  DYN15840
0090      Q(8)=SINT*AL(2)                  DYN15850
0091      120      CONTINUE                         DYN15860
C
0092      DO 130 I=1,8                      DYN15870
0093      QQ(I)=0.0                          DYN15878
C
0094      DO 130 J=1,8                      DYN15880
0095      QQ(I)=QQ(I)+CHECK(J,I)*Q(J)      DYN15890
0096      130      CONTINUE                         DYN15898
C
0097      DO 130 J=1,8                      DYN15900
0098      QQ(I)=QQ(I)+CHECK(J,I)*Q(J)      DYN15910
0099      130      CONTINUE                         DYN15912
C
0100      DO 130 J=1,8                      DYN15915
0101      QQ(I)=QQ(I)+CHECK(J,I)*Q(J)      DYN15918

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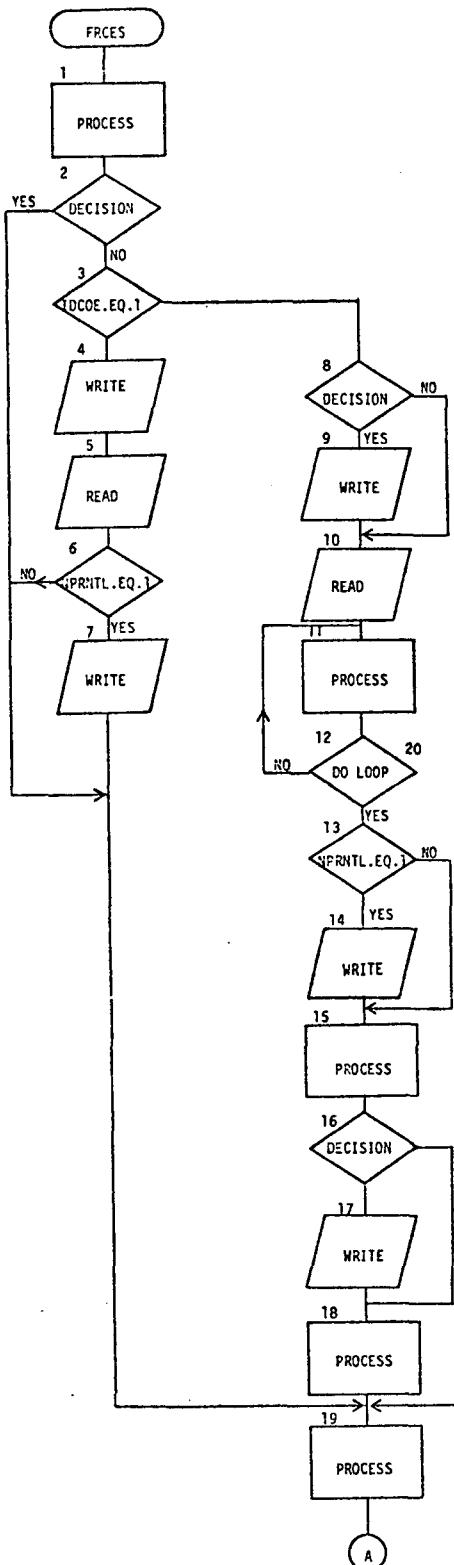
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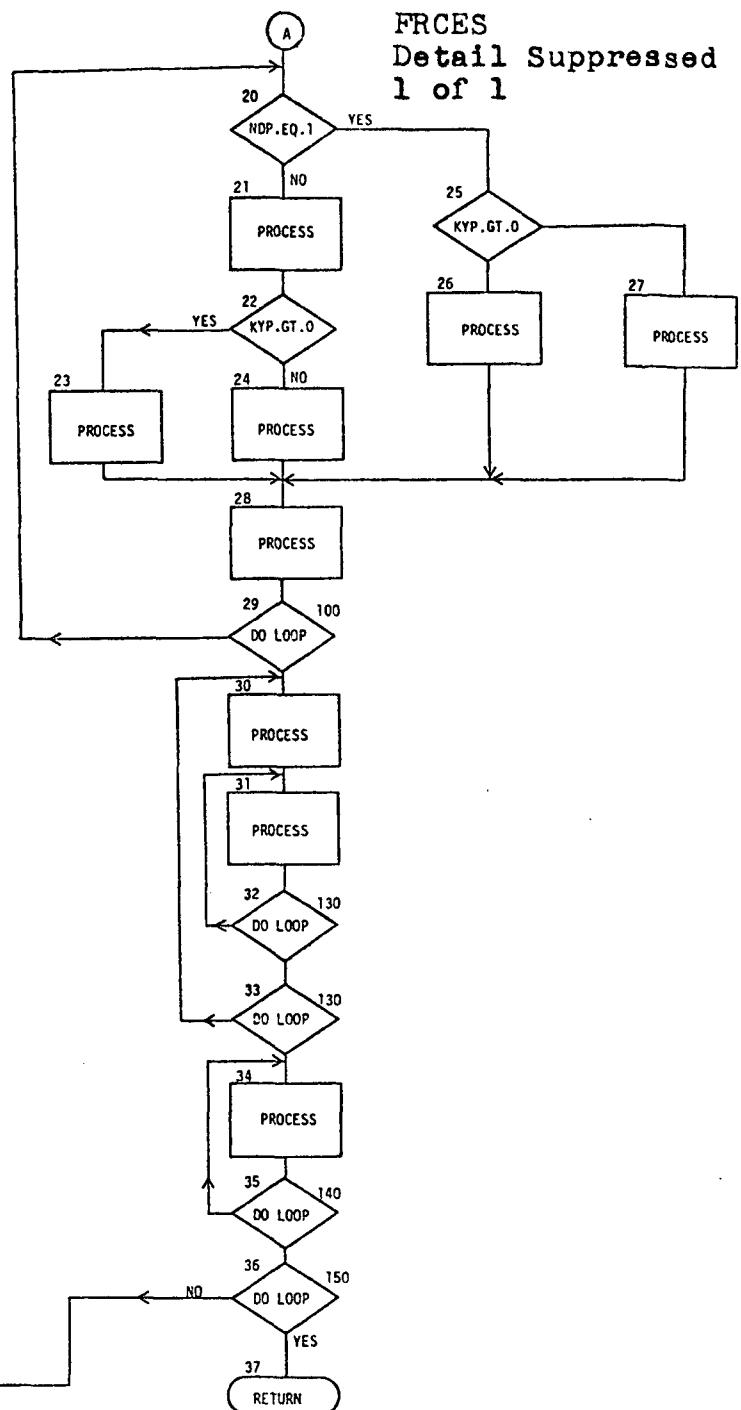
0097      DO 140 I=1,8                               DYN15920
0098      J=4*(IELM-1)+I+(IH-1)*NEQ+IB*NEQT        DYN15930
0099      FORCE(J)=FORCE(J)+QQ(I)                  DYN15940
0100      140  CONTINUE                            DYN15942
C
0101      150  CONTINUE                            DYN15945
C
0102      RETURN                                  DYN15950
C
0103      160 FORMAT (1H1,35X,40HFOURIER COEFFICIENTS OF APPLIED PRESSURE,
1          9H LOADINGS//                           DYN15953
1          20X,10HMERIDIANAL,20X,6HNORMAL,20X,10HTANGENTIAL,10X,
2          12HHARMONIC NO.//}                         DYN15960
DYN15970
0104      170 FORMAT (2I5/(3F10.0))                 DYN15980
0105      180 FORMAT (/60X,11HELEMENT NO.,I3,1H-,I3,//(2X,3D28.7,15X,I2)) DYN15982
0106      190 FORMAT (1H1,51X,30HAPPLIED LOADS ON THE STRUCTURE//)
1          56X,19HPRESSURE COMPONENTS//             DYN15990
2          20X,10HMERIDIANAL,20X,6HNORMAL,20X,10HTANGENTIAL,11X,
2          19HFROM THETA TO THETA,9H(DEGREES))       DYN16000
DYN16010
0107      200 FORMAT (3I5/(4F10.0))                 DYN16020
0108      210 FORMAT (/60X,11HELEMENT NO.,I3,1H-,I2//(2X,3F28.3,12X,2F10.3)) DYN16030
0109      220 FORMAT (2X,3F28.3,12X,2F10.3)           DYN16032
0110      END                                     DYN16040
DYN16050
DYN16060
DYN16070
DYN16080
DYN16090
  
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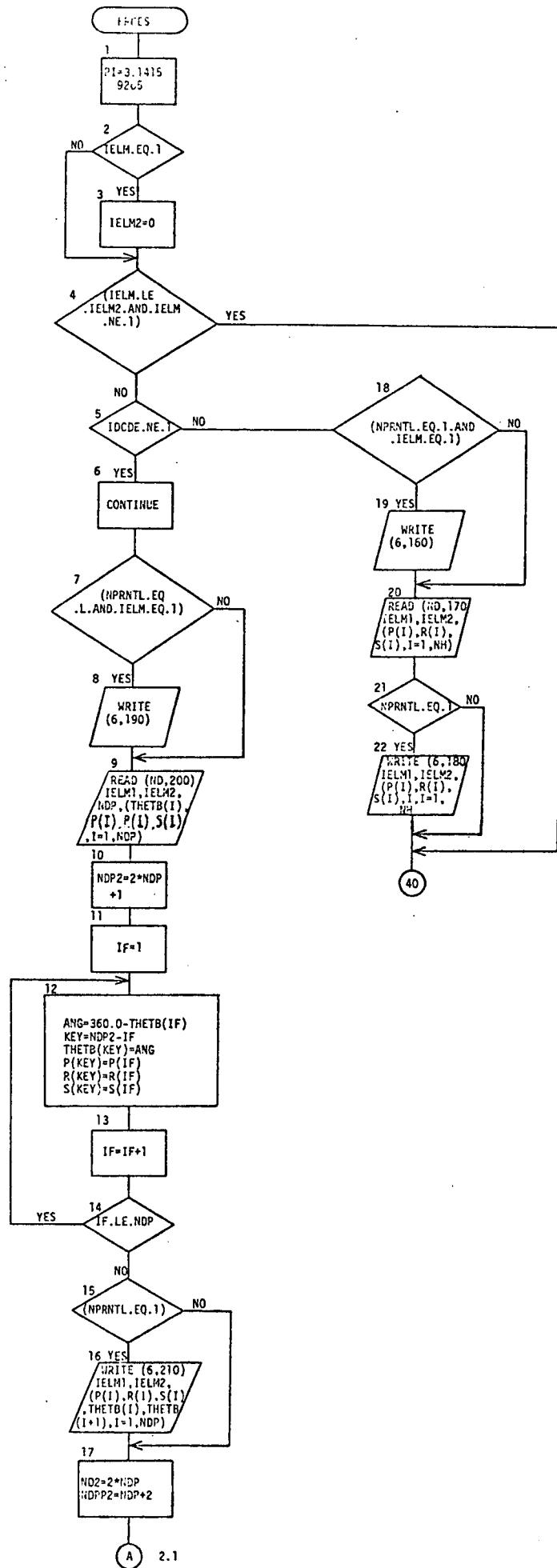


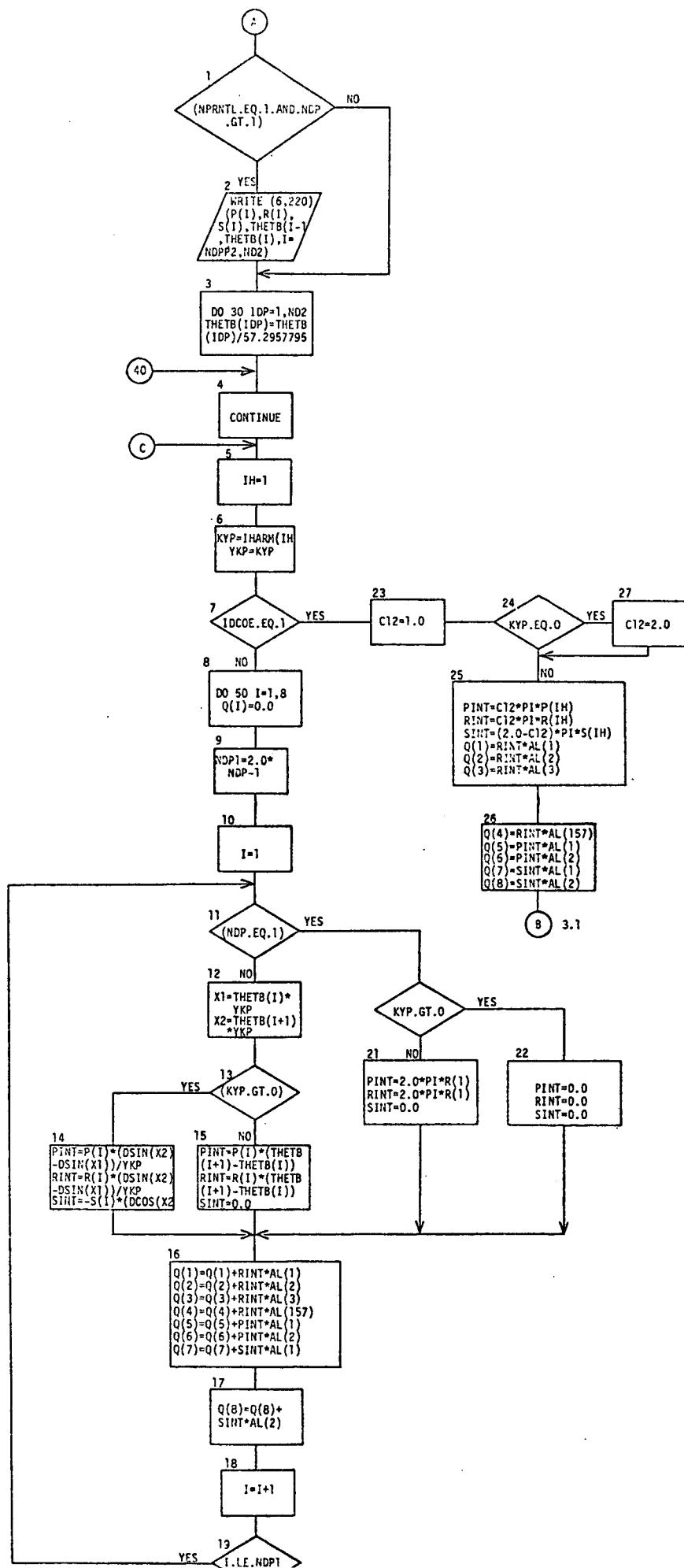
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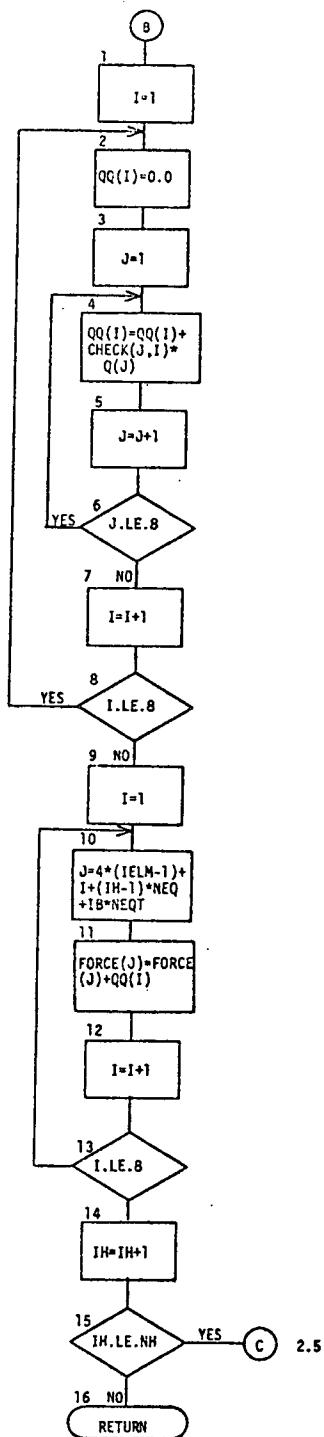


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CE(HOUBQN)                               DYNC9772
C                                         DYNC9774
C   DESCRIPTION - TO SET UP AND CONTROL THE SOLUTION OF THE      DYN09776
C   EQUATIONS OF MOTION FOR EACH TIME STEP EXCEPT THE FIRST ONE.  DYN09778
C                                         DYN09780
C   INPUT ARGUMENTS.                                              DYN09782
C     FORCE = MATRIX OF GENERALIZED FORCES DUE TO EXTERNAL LOADS AND DYN09784
C           TEMPERATURES.                                         DYN09786
C     IH    = HARMONIC KEY.                                       DYN09788
C     KY    = RESTART KEY.                                       DYN09790
C     QN    = DISPLACEMENTS AT TIME INCREMENT (N-1) UP TO STATEMENT 20 DYN09792
C           AFTER STATEMENT 30 THIS MATRIX HAS BEEN CHANGED TO      DYN09794
C           THE DISPLACEMENTS AT TIME STEP (N).                      DYN09796
C     QN1   = DISPLACEMENTS AT TIME INCREMENT (N-2) BEFORE STATEMENT 10 DYN09798
C           AND AT TIME INCREMENT (N-1) AFTER STATEMENT 20.          DYN09800
C     QP    = Q - PARTIAL DERIVATIVE OF U-NL WITH RESPECT TO LOWER DYN09802
C           CASE Q AT TIME STEP (N-1).                           DYN09804
C     QP1   = Q - PARTIAL DERIVATIVE OF U-NL WITH RESPECT TO LOWER CASE DYN09806
C           Q AT TIME STEP (N-2).                                DYN09808
C                                         DYN09810
C   OUTPUT ARGUMENTS.                                             DYN09812
C     QLOAD  = RIGHT-HAND SIDE OF THE DYNAMIC EQUATIONS OF MOTION DYN09814
C           BEFORE CALLING SOLVEQ.                            DYN09816
C     QN    = DISPLACEMENTS AT TIME INCREMENT (N-1) UP TO STATEMENT 20 DYN09818
C           AFTER STATEMENT 30 THIS MATRIX HAS BEEN CHANGED TO      DYN09820
C           THE DISPLACEMENTS AT TIME STEP (N).                      DYN09822
C     QN1   = DISPLACEMENTS AT TIME INCREMENT (N-2) BEFORE STATEMENT 10 DYN09824
C           AND AT TIME INCREMENT (N-1) AFTER STATEMENT 20.          DYN09826
C     QN2   = DISPLACEMENTS AT TIME INCREMENT (N-3) BEFORE STATEMENT 10 DYN09828
C           AND AT TIME STEP (N-2) AFTER STATEMENT 20.              DYN09830
C     QP1   = Q - PARTIAL DERIVATIVE OF U-NL WITH RESPECT TO LOWER CASE DYN09832
C           Q AT TIME STEP (N-2).                                DYN09834
C                                         DYN09836
C   EXTERNALS.                                                 DYN09838
C     CALLED BY
C       SETUP                                         DYNC9840
C       CALLS
C         MATMUT                                         DYNC9842
C         SOLVEQ                                         DYNC9844
C                                         DYNC9846
C                                         DYNC9848
C                                         DYNC9850
C
0001   SUBROUTINE HOUBQN (KY,IH)                               DYNC9852
0002   IMPLICIT REAL*8 (A-H,O-Z)                             DYNC9854
0003   COMMON /SLVEEQ/ XN(6550),QLOAD(204)                  DYNC9856
0004   COMMON /QS/ QN(1020),QN1(1020),FORCE(2040),QP(1020),QP1(1020),  DYN09858
1      QN2(1020)
0005   COMMON /RSTRNT/ NODRES,NCLOSE,LK(204)                DYNC9860
0006   COMMON /CONST/ NH,NELEMS,NNODES,NSIZE,NPRNTQ,NEQ,NEQT,N,NN,NHNS,  DYNC9862
1      DT2,NPRNTL,NPRNTF,IDEFL,IDCOE                         DYNC9864
                                         DYNC9866

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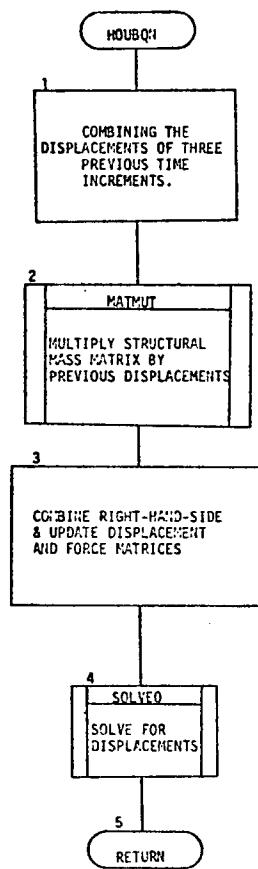
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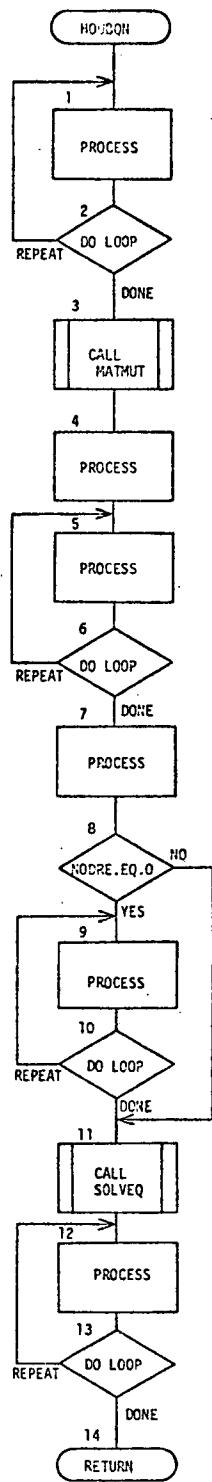
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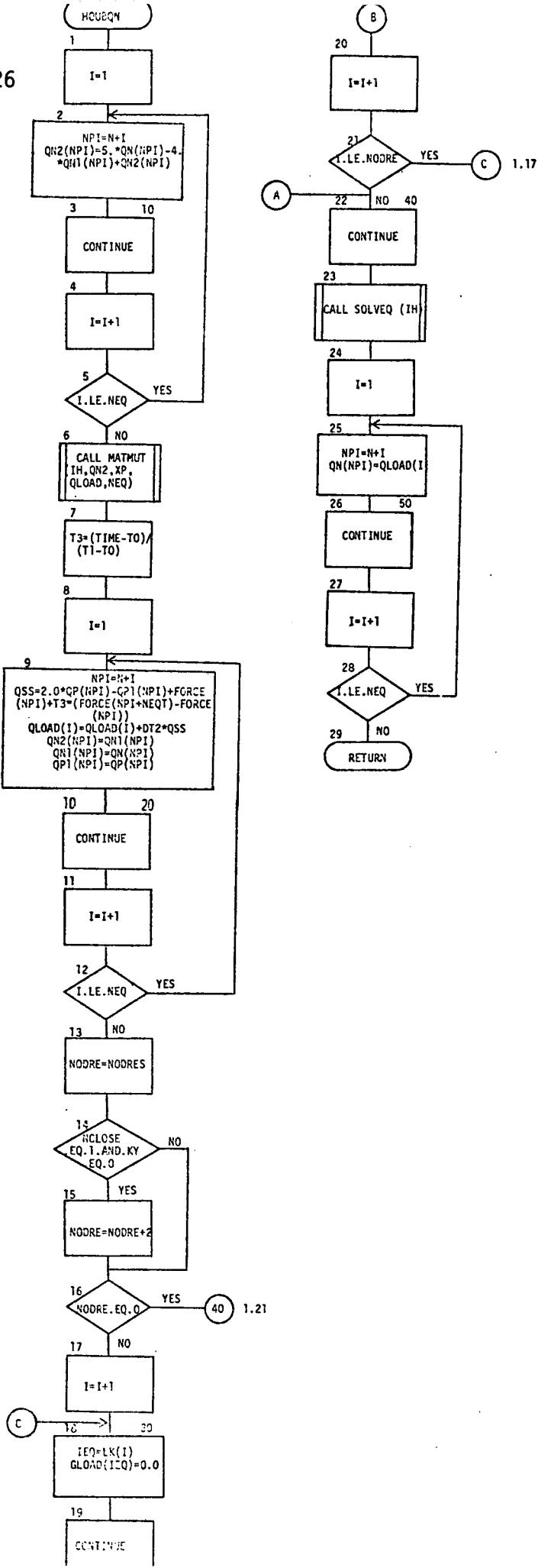
0007      COMMON /PS/ XP(6550)                               DYN09868
0008      COMMON /TMFT/ TOTIME,DELTE,TIME,T0,T1           DYN09870
          C1   COMBINING THE DISPLACEMENTS OF THREE PREVIOUS TIME INCREMENTS DYNC9872
          C
0009      DO 10 I=1,NEQ                                     DYN09918
0010      NPI=N+I                                         DYN09920
0011      QN2(NPI)=5.*QN(NPI)-4.*QN1(NPI)+QN2(NPI)       DYN09930
0012      10 CONTINUE                                      DYN09940
          C
          C1   MULTIPLY STRUCTURAL MASS MATRIX BY PREVIOUS DISPLACEMENTS DYN09953
0013      CALL MATMUT (IH,QN2,XP,QLOAD,NEQ)                 DYN09960
          C1   COMBINE RIGHT-HAND-SIDE & UPDATE DISPLACEMENT AND FORCE MATRICES DYNC9962
0014      T3=(TIME-T0)/(T1-T0)                             DYNC9980
          C
0015      DO 20 I=1,NEQ                                     DYN09988
0016      NPI=N+I                                         DYN10000
0017      QSS=2.0*QP(NPI)-QP1(NPI)+FORCE(NPI)+T3*(FORCE(NPI)+NEQT)- DYN10010
          1     FORCE(NPI))                                DYN10012
0018      QLOAD(I)=QLOAD(I)+DT2*QSS                      DYN10030
0019      QN2(NPI)=QN1(NPI)                             DYN10040
0020      QN1(NPI)=QN(NPI)                             DYN10050
0021      QP1(NPI)=QP(NPI)                            DYN10060
0022      20 CONTINUE                                      DYN10C70
          C
          C1   APPLY BOUNDARY CONDITIONS TO RIGHT-HAND-SIDE DYN10073
0023      NODRE=NODRES                                 DYN10075
0024      IF (INCLOSE.EQ.1.AND.KY.EQ.0) NODRE=NODRE+2 DYN10090
0025      IF (NODRE.EQ.0) GO TO 40                      DYN10100
          C
0026      DO 30 I=1,NODRE                                DYN10110
0027      IEQ=LK(I)                                     DYN10118
0028      QLOAD(IEQ)=0.0                                  DYN10120
0029      30 CONTINUE                                     DYN10130
          C
0030      40 CONTINUE                                     DYN10140
          C1   SOLVE FOR DISPLACEMENTS                   DYN10153
0031      CALL SOLVEQ (IH)                           DYN10160
          C
0032      DO 50 I=1,NEQ                                     DYN10188
0033      NPI=N+I                                         DYN10190
0034      QN(NPI)=QLOAD(I)                           DYN10200
0035      50 CONTINUE                                     DYN10210
          C
0036      RETURN                                         DYN10220
0037      END                                            DYN10230
                                                DYN10240

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CE(HOUBQ1)                               DYNC8962
C
C      DESCRIPTION - TO CALCULATE THE DISPLACEMENTS AT THE END      DYNC8964
C          OF THE FIRST TIME STEP ONLY AND SET UP THE COEFFICIENT      DYNC8966
C          MATRICES FOR USE IN SUBSEQUENT STEPS.                      DYNC8968
C
C      INPUT ARGUMENTS.                                              DYNC8970
C          DELTE   = TIME INCREMENT USED IN SOLVING THE EQUATIONS OF MOTION DYNC8972
C                         OF THE SHELL.                                DYNC8974
C          DT2     = THE SQUARE OF THE TIME INCREMENT.                  DYNC8976
C          FORCE   = MATRIX OF GENERALIZED FORCES DUE TO EXTERNAL LOADS AND DYNC8978
C                         TEMPERATURES.                            DYNC8980
C          IH      = HARMONIC KEY.                                 DYNC8982
C          IRSTRT  = INPUT CONSTANT WHICH INDICATES IF THE PROGRAM IS BEING DYNC8984
C                         RESTARTED.                           DYNC8986
C          KY      = RESTART KEY.                                DYNC8988
C          QN      = DISPLACEMENTS AT TIME INCREMENT (N-1) UP TO STATEMENT 20 DYNC8990
C                         AFTER STATEMENT 30 THIS MATRIX HAS BEEN CHANGED TO DYNC8992
C                         THE DISPLACEMENTS AT TIME STEP (N).           DYNC8994
C          TIME    = CURRENT TIME.                                DYNC8996
C          TO      = INITIAL TIME.                                DYNC8998
C          T1      = STOP TIME.                                 DYNC9000
C          XN      = STRUCTURAL STIFFNESS MATRIX AS READ FROM INPUT TAPE. DYNC9002
C                         AFTER THE FIRST TIME STEP, THIS MATRIX IS REPLACED BY A DYNC9004
C                         COMBINATION OF THE MASS AND STIFFNESS MATRICES. DYNC9006
C
C      EXTERNALS.                                                 DYNC9008
C          CALLED BY:                                             DYNC9010
C              SETUP.                                         DYNC9012
C
C          CALLS:                                                 DYNC9014
C              MATMUT.                                         DYNC9016
C              NRESTR.                                         DYNC9018
C              SOLVEQ.                                         DYNC9020
C
C          SUBROUTINE HOUBQ1 (KY,IH)                             DYNC9022
C          IMPLICIT REAL*8 (A-H,O-Z)                          DYNC9024
C          COMMON /SLVEEQ/ XN(6550),QLOAD(204)                DYNC9026
C          COMMON /QS/ QN(1020),QN1(1020),F0RCE(2040),QP(1020),QP1(1020), DYNC9028
C              1        QN2(1020)                                DYNC9030
C          COMMON /RSTRNT/ NCDRES,NCLOSE,LK(204)                DYNC9032
C          COMMON /CONST/ NH,NELEMS,NNODES,NSIZE,NPRNTQ,NEQ,NEQT,N,NN,NHNS, DYNC9034
C              1        DT2,NPRNTL,NPRNTF,IDEFL,IDCOE             DYNC9036
C          COMMON /PS/ XP(6550)                                DYNC9038
C          COMMON /TMFT/ TOTIME,DELTE,TIME,TO,T1                DYNC9040
C          COMMON /RESTRT/ IRSTRT,NPRNT,NPRNIT,ITP,TIMEP,DELTEP DYNC9042
C          DIMENSION QLOAD1(1020)                            DYNC9044
C
C          IFLAG=0                                         DYNC9046
C
0001
0002
0003
0004
0005
0006
0007
0008
0009
0010
0011

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0012      T3=(TIME-T0)/(T1-T0)                               DYN09140
0013      T3M1=(TIME-DELTE-T0)/(T1-T0)                   DYNC9150
0014      C1      MULTIPLY STIFFNESS MATRIX BY INITIAL DISPLACEMENT DYN09152
0015      CALL MATMUT (IH,QN1,XN,QLOAD1,NEQ)             DYN09170
0016      C
0017      DO 20 I=1,NEQ                                  DYN09178
0018          NPI=N+I                                     DYN09180
0019          QN(NPI)=QN1(NPI)+DELTE*QN(NPI)           DYN09200
0020          IF (IRSTRT.EQ.1) GO TO 10                 DYNC9210
0021          QLOAD1(I)=FORCE(NPI)-QLOAD1(I)           DYN09220
0022          GO TO 20                                     DYN09230
0023          10      QLOAD1(I)=QP1(NPI)-QLOAD1(I)+FORCE(NPI)+T3M1*(FORCE(NPI+NEQT)- DYNC9240
0024              FORCE(NPI))                           DYNC9250
0025          20      CONTINUE                            DYNC9260
0026          C
0027          C1      MULTIPLY STRUCTURAL MASS MATRIX BY DISPLACEMENT VECTOR DYN09263
0028          CALL MATMUT (IH,QN,XP,QLOAD,NEQ)           DYNC9265
0029          TDT2=2*DT2                                DYNC9280
0030          C
0031          DO 40 I=1,NEQ                                  DYN09290
0032          NPI=N+I                                     DYN09298
0033          IF (IRSTRT.EQ.1) GO TO 30                 DYN09300
0034          QLOAD(I)=6.*QLOAD(I)+DT2*FORCE(NPI)+TDT2*QLOAD1(I) DYNC9310
0035          GO TO 40                                     DYNC9320
0036          30      QLOAD(I)=6.*QLOAD(I)+DT2*QP(NPI)+TDT2*QLOAD1(I)+DT2* DYNC9330
0037              (FORCE(NPI)+T3*(FORCE(NPI+NEQT)-FORCE(NPI))) DYNC9340
0038          40      CONTINUE                            DYNC9350
0039          C
0040          C
0041          DO 50 I=1,NSIZE                            DYN09360
0042          NNPI=NN+I                                 DYN09370
0043          XN(NNPI)=DT2*XN(NNPI)+6.*XP(NNPI)       DYN09373
0044          50      CONTINUE                            DYNC9378
0045          C
0046          C1      APPLY BOUNDARY CONDITIONS           DYN09380
0047          60      CALL NRESTR (KY)                  DYN09390
0048          C1      SOLVING FOR Q1 & SETTING UP TO SOLVE FOR INITIAL ACCELERATIONS DYNC9400
0049          CALL SOLVEQ (IH)                         DYNC9413
0050          C1      HAVE DISPLACEMENTS BEEN DETERMINED//YES(90) DYNC9415
0051          IF (IFLAG.EQ.1) GO TO 90                 DYNC9430
0052          C1      SAVE INITIAL DISPLACEMENTS        DYNC9432
0053          C
0054          DO 70 I=1,NEQ                                  DYN09450
0055          NPI=N+I                                     DYN09452
0056          QN(NPI)=QLOAD(I)                         DYN09460
0057          QLOAD(I)=QLOAD1(I)                        DYN09462
0058          70      CONTINUE                            DYNC9468
0059          C

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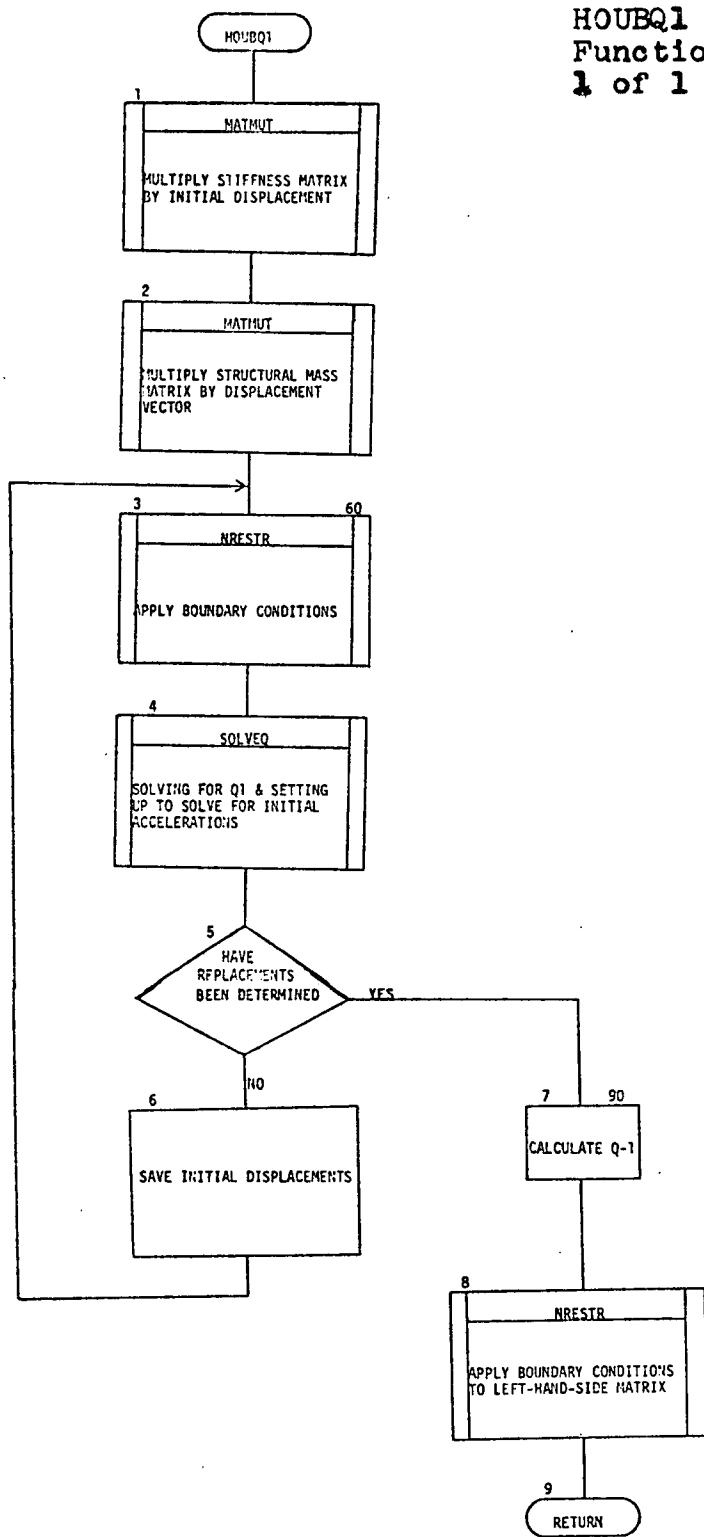
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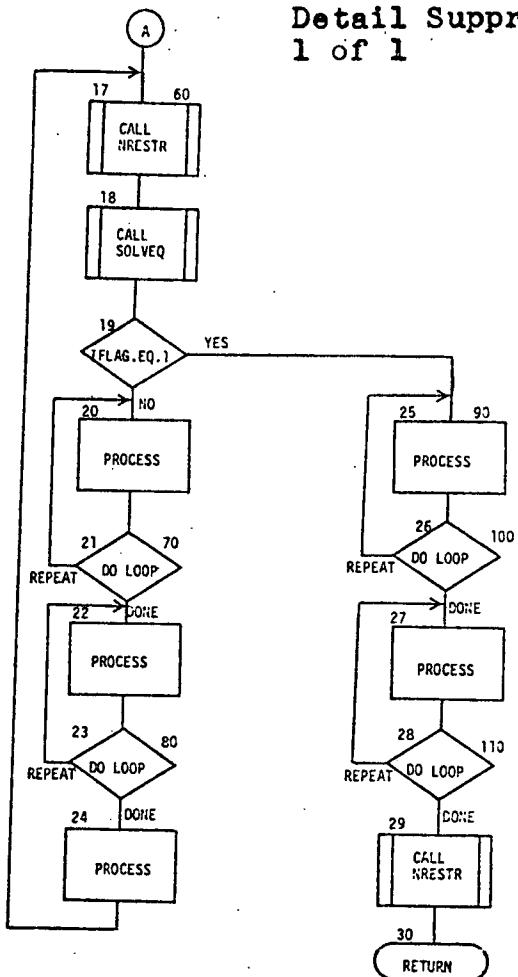
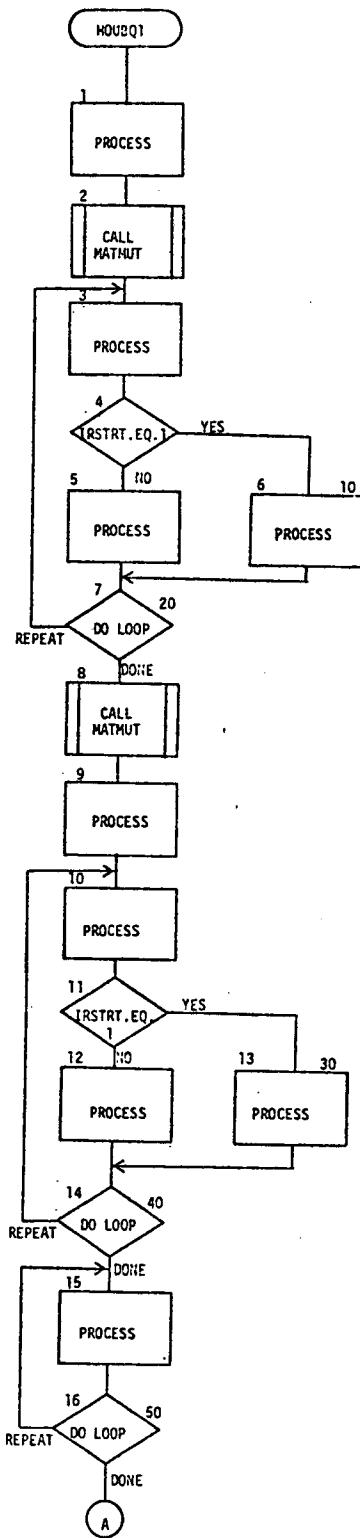
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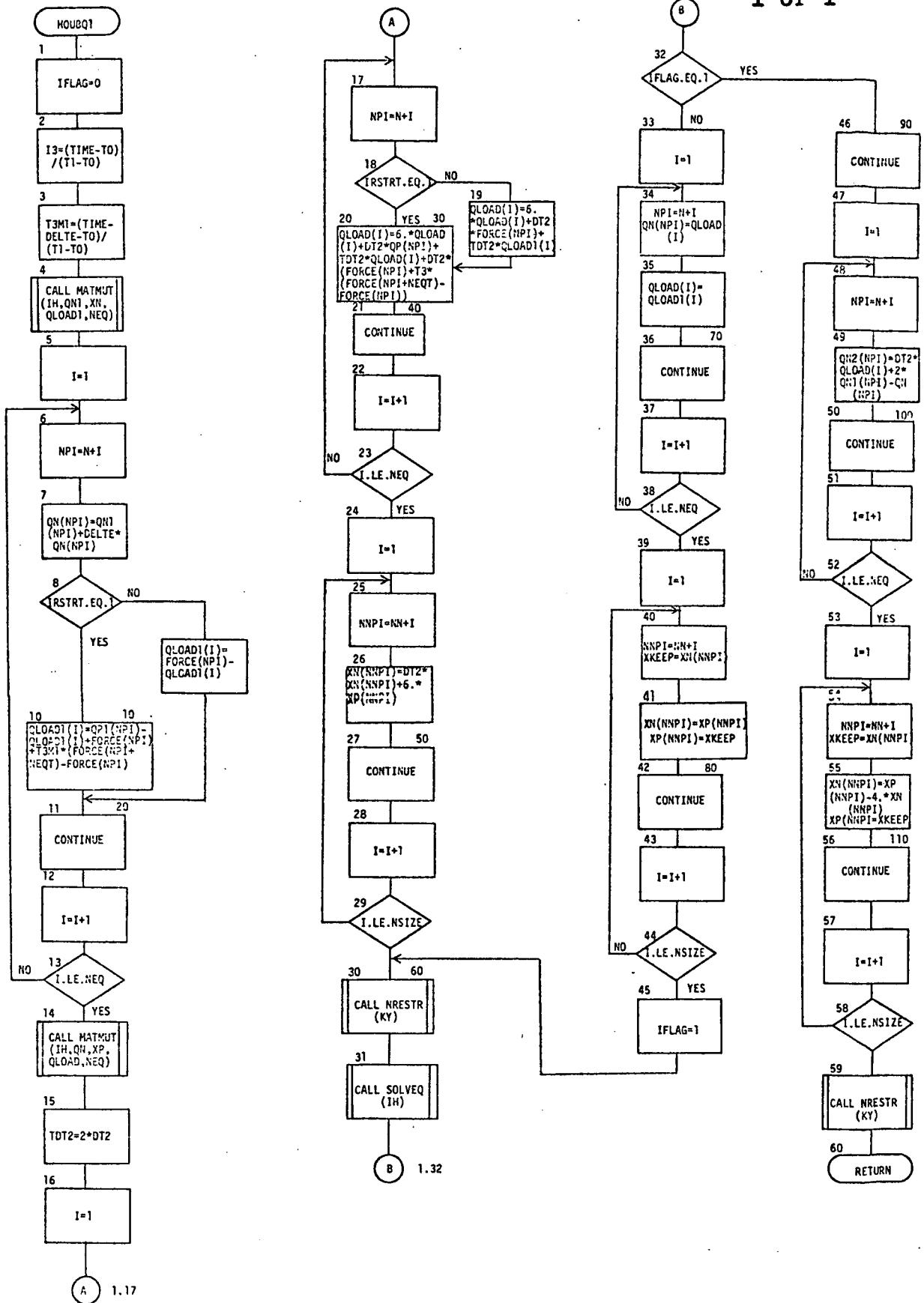
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C          DO 80 I=1,NSIZE          DYN09518
0044      NNPI=NN+I          DYNC9520
0045      XKEEP=XN(NNPI)          DYNC9530
0046      XN(NNPI)=XP(NNPI)          DYN09540
0047      XP(NNPI)=XKEEP          DYN09550
0048
0049      80 CONTINUE          DYNC9560
C          IFLAG=1          DYNC9570
0050      GO TO 60          DYN09573
0051
0052      90 CONTINUE          DYNC9600
C1      CALCULATE Q-1          DYNC9610
C
0053      DO 100 I=1,NEQ          DYN09612
0054      NPI=N+I          DYN09628
0055      QN2(NPI)=DT2*QLOAD(I)+2*QN1(NPI)-QN(NPI)          DYN09630
0056
100 CONTINUE          DYN09640
C          C          DYN09650
0057      DO 110 I=1,NSIZE          DYN09660
0058      NNPI=NN+I          DYN09663
0059      XKEEP=XN(NNPI)          DYN09668
0060      XN(NNPI)=XP(NNPI)-4.*XN(NNPI)          DYNC9670
0061      XP(NNPI)=XKEEP          DYN09680
0062
110 CONTINUE          DYN09690
C          C1      APPLY BOUNDARY CONDITIONS TO LEFT-HAND-SIDE MATRIX          DYN09700
0063      CALL NRESTR (KY)          DYN09710
0064      RETURN          DYNC9720
0065      END          DYNC9723
DYN09725
DYN09740
DYN09750
DYN09760
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CE(INPUT) DYN00912
 C DYN00914
 C DESCRIPTION - TO PERFORM THE MAJOR INPUT FUNCTIONS FOR THE DYN00916
 C DYNASOR PROGRAM. IT READS ALL CASE CONTROL PARAMETERS DYN00918
 C AND ALL DATA CARD TYPES. SOME DATA REFINEMENT DYN00920
 C FUNCTIONS, SUCH AS CALCULATION OF THE TRIGONOMETRIC DYN00922
 C INTEGRALS REQUIRED TO CALCULATE THE GENERALIZED DYN00924
 C NONLINEAR LOADS, ARE PERFORMED. THE FOLLOWING DYN00926
 C QUANTITIES CAN BE READ IN - FOURIER HARMONICS, DYN00928
 C MASS AND STIFFNESS MATRICES, NODAL RESTRAINTS, DYN00930
 C INITIAL CONDITIONS, SHELL STRUCTURAL DATA, THERMAL DYN00932
 C LOADS, THERMAL EXPANSION COEFFICIENTS, CONCENTRATED DYN00934
 C RING LOADS, TEMPERATURE DISTRIBUTIONS AND GRADIENTS. DYN00936
 C DYN00938
 C INPUT ARGUMENTS. DYN00940
 C KEY = FLAG GOVERNING =1) DATA INPUT FROM TAPE AND CARDS DYN00942
 C =2) BYPASSING DATA INPUT DURING RESTART DYN00944
 C =3) PERIODIC OUTPUT OF RESTART DATA TO DYN00946
 C TAPE. DYN00948
 C DYN00950
 C OUTPUT ARGUMENTS. DYN00952
 C ALS = MATRIX OF COEFFICIENTS OF THERMAL EXPANSION IN THE DYN00954
 C MERIDIANAL DIRECTION FOR THE ELEMENTS. DYN00956
 C ALT = MATRIX OF COEFFICIENTS OF THERMAL EXPANSION IN THE DYN00958
 C CIRCUMFERENTIAL DIRECTION FOR THE ELEMENTS. DYN00960
 C COSM = MATRIX WHOSE ELEMENTS ARE THE COSINE OF PHI AT THE DYN00962
 C MIDDLE OF EACH ELEMENT. DYN00964
 C DTH = MATRIX OF FOURIER COEFFICIENTS FOR THE CIRCUMFERENTIAL DYN00966
 C TEMPERATURE GRADIENT DISTRIBUTION. DYN00968
 C FORCE = MATRIX OF GENERALIZED FORCES DUE TO EXTERNAL LOADS AND DYN00970
 C TEMPERATURES. DYN00972
 C LK = MATRIX INDICATING THE NODAL RESTRAINTS WHICH ARE APPLIED DYN00974
 C ON THE SHELL. DYN00976
 C NEQ = NUMBER OF EQUILIBRIUM EQUATIONS PER HARMONIC. DYN00978
 C NEQT = TOTAL NUMBER OF EQUILIBRIUM EQUATIONS FOR ALL HARMONICS. DYN00980
 C NHNS LENGTH OF STRUCTURAL STIFFNESS OR MASS MATRIX FOR ALL DYN00982
 C HARMONICS STORED IN VECTOR FORM. DYN00984
 C NNODES = TOTAL NUMBER OF NODES, EQUAL TO (NFELEMS + 1). DYN00986
 C NSIZE = THE NUMBER OF TERMS IN THE STRUCTURAL STIFFNESS OR MASS DYN00988
 C MATRIX (IN VECTOR FORM) FOR A PARTICULAR HARMONIC. DYN00990
 C QN = INITIAL NODAL VELOCITIES. DYN00992
 C QN1 = DISPLACEMENTS AT TIME INCREMENT (N-2) BEFORE STATEMENT 10 DYN00994
 C AND AT TIME INCREMENT (N-1) AFTER STATEMENT 20. DYN00996
 C QP = Q - PARTIAL DERIVATIVE OF U-NL WITH RESPECT TO LOWER DYN00998
 C CASE Q AT TIME STEP (N-1). DYN01000
 C QP1 = Q - PARTIAL DERIVATIVE OF U-NL WITH RESPECT TO LOWER CASE DYN01002
 C Q AT TIME STEP (N-2). DYN01004
 C SINM = SINE OF PHI AT THE MIDDLE OF THE ELEMENTS. DYN01006

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C	TH	= MATRIX WHOSE ELEMENTS ARE THE FOURIER COEFFICIENTS OF THE CIRCUMFERENTIAL TEMPERATURE DISTRIBUTION.	DYN01008
C	TO	= INITIAL TIME.	DYN01010
C	T1	= STOP TIME.	DYN01012
C			DYN01014
C			DYN01016
C	EXTERNALS.		DYN01018
C	CALLED BY		DYN01020
C		MAIN	DYN01022
C		SETUP	DYN01024
C	CALLS		DYN01026
C		TRI4OR	DYN01028
C		NLTERM	DYN01030
C		FRCES	DYN01032
C		THCOE	DYN01034
C		TFORCE	DYN01036
C			DYN01038
0001		SUBROUTINE INPUT (KEY)	DYN01040
0002		IMPLICIT REAL*8 (A-H,O-Z)	DYN01042
0003		COMMON /CHALS/ AL(167),CHECK(8,8)	DYN01044
0004		COMMON /SLVEEQ/ XN(6550),QLOAD(204)	DYN01046
0005		COMMON /QS/ QN(1020),QN1(1020),FORCE(2040),QP(1020),QP1(1020), 1 QN2(1020)	DYN01048
0006		COMMON /RSTRNT/ NODRES,NCLOSE,LK(204)	DYN01050
0007		COMMON /CONST/ NH,NELEMS,NNODES,NSIZE,NPRNTQ,NEQ,NEQT,N,NN,NHNS, 1 DT2,NPRNTL,NPRNTF,IDEFL,IDCQE	DYN01052
0008		COMMON /PS/ XP(6550)	DYN01054
0009		COMMON /TMFT/ TOTIME,DELTE,TIME,TO,T1	DYN01056
0010		COMMON /GEOM/ FNU1(50),FNU2(50),E1(50),E2(50),G(50),T(50), 1 SINE(51),COSINE(51),SINM(50),COSM(50),R(50),PH(50), 1 PHP(50),ARCL(50)	DYN01058
0011		COMMON /THETAS/ THETA(20),NTHETA,NCLCST,NSTRSS	DYN01060
0012		COMMON /PRINT/ IPRINT,NOIT,LL	DYN01062
0013		COMMON /HARM/ NHP,IHARM(5)	DYN01064
0014		COMMON /RESTRT/ IRSTRTR,NPRNT,NPRNTIT,ITP,TIMEP,DELTEP	DYN01066
0015		COMMON /THER/ TH(50,5,2),DTH(50,5,2),ALS(50),ALT(50)	DYN01068
0016		COMMON /THCON/ ITEL,F,ITCOE,NPRNTH	DYN01070
0017		COMMON /CYCLE/ ITAM	DYN01072
0018		COMMON /TAPES/ NT,ND,NS	DYN01074
0019		COMMON /RZ/ R0(51),Z(51)	DYN01076
0020		DIMENSION COMENT(20), JUNK(20), TH1(5), DTH1(5)	DYN01078
0021		DIMENSION DUM(1310)	DYN01080
0022		EQUIVALENCE (DUM(1),XN(1)), (XN(1),COMENT(1))	DYN01082
0023		DOUBLE PRECISION CONSTN,CONSTF,CONSTI	DYN01084
0024		DATA CONSTN/8HCONSTANT/,CONSTI/8H /	DYN01086
C1		KEY//1(10),2(430),3(710)	DYN01088
0025		GO TO (10,430,710), KEY	DYN01090
C1		READ CASE I.O., CASE CONTROL, AND CIRCUMFERENTIAL ANGLE CARDS	DYN01092
0026		10 CONTINUE	DYN01094

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0027      CONSTF=CONST1                               DYN01200
0028      WRITE (6,730)                             DYN01210
0029      C2      READ INPUT DATA FOR CARD TYPE II - A   DYN01212
          READ (ND,740) NCARDS,NT                  DYN01230
0030      C2      TYPE II-B CARDS LEFT//NO(30)        DYN01232
          IF (NCARDS.EQ.0) GO TO 30                 DYN01240
          C
0031      DO 20 I=1,NCARDS                         DYN01248
          C2      READ INPUT DATA FOR CARD TYPE II - B   DYN01250
          READ (ND,750) (COMENT(J),J=1,20)           DYN01270
0033      WRITE (6,800) (COMENT(J),J=1,20)           DYN01280
0034      20 CONTINUE                                DYN01282
          C
0035      30 CONTINUE                                DYN01285
          C2      READ INPUT DATA FOR CARD TYPE III     DYN01290
          READ (ND,760) TOTIME,DELTE,IRSTR,INCRST,NCLOSE,ITELF,NPRNTQ,
          1       IPRINT,NCLCST,NSTRSS,NPRNT,NPRNIT,NPRNTL,NPRNTF,NPRNTH, DYN01292
          1       NPRNMS                                DYN01320
          C2      READ INPUT DATA FOR CARD TYPE IV      DYN01322
          READ (ND,770) NTHETA,(THETA(I),I=1,NTHETA) DYN01330
0037      NOIT=1                                    DYN01332
0038      C1      READ FOURIER HARMONICS CARD IF NO RESTART DYN01340
          IF (IRSTRT.EQ.0) READ (ND,780) NH,(IHARM(I),I=1,NH) DYN01370
0040      KEYRS=0                                    DYN01380
0041      IF (IRSTRT.EQ.1) KEYRS=1                  DYN01390
0042      40 CONTINUE                                DYN01400
          C2      READ INFORMATION AND SHELL DESCRIPTION FROM INPUT TAPE DYN01402
          REWIND NT                                 DYN01440
0043      READ (NT) NCARDS,JUNK                   DYN01450
0044      IF (NCARDS.EQ.0) GO TO 60                 DYN01460
0045      WRITE (6,790)                           DYN01470
          C
0047      DO 50 K=1,NCARDS                         DYN01478
          READ (NT) (COMENT(J),J=1,20)               DYN01490
          IF (KEYRS.EQ.1) GO TO 50                 DYN01500
          WRITE (6,800) (COMENT(J),J=1,20)           DYN01510
0051      50 CONTINUE                                DYN01520
          C
0052      60 READ (NT) NHP,NELEMS,JUNK             DYN01523
          IF (KEYRS.EQ.0) GO TO 110                DYN01530
0053      C2      READ ADDITIONAL INFORMATION FROM INPUT TAPE FOR RESTART OPERATION DYN01540
          C
0054      DO 70 K=1,NELEMS                         DYN01542
          READ (NT) (DUM(I),I=1,230)               DYN01578
0055      70 CONTINUE                                DYN01580
          C
0056      J=6*NELEMS                            DYN01590
          READ (NT) (DUM(I),I=1,J)                 DYN01592
0057
0058

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      C
0059      DO 90 K=1,NELEMS                               DYN01618
0060      IF (K.EQ.NELEMS) GO TO 80                      DYN01620
0061      READ (NT) (DUM(I),I=1,6)                      DYN01630
0062      GO TO 90                                      DYN01640
0063      80      READ (NT) (DUM(I),I=1,8)              DYN01650
0064      90      CONTINUE                                DYN01660
      C
0065      J=2*(NELEMS+1)                                DYN01670
0066      READ (NT) (DUM(I),I=1,J)                      DYN01673
0067      J=2*NHP                                      DYN01680
0068      NSIZE=10+26*NELEMS                            DYN01690
      C
0069      DO 100 K=1,J                                  DYN01700
0070      READ (NT) (DUM(I),I=1,NSIZE)                  DYN01710
0071      100     CONTINUE                                DYN01718
      C
0072      READ (NT) NH,(IHARM(I),I=1,NH),JUNK          DYN01720
0073      KEYRS=0                                     DYN01730
0074      GO TO 40                                     DYN01732
0075      110     CONTINUE                                DYN01735
0076      WRITE (6,810) TOTIME,DELTE,IRSTR,INCRST,NPRNT,NPRNIT,NPRNTQ,
1           IPRINT,NCLCST,NSTRSS,NPRNLT,NPRNTF,NPRNTH,NT,NS,ND,   DYN01740
2           NCLOSE,IITLEF,NELFMS,NPRNMS,NH,(IHARM(I),I=1,NH)       DYN01750
0077      WRITE (6,820) NTHETA,(THETA(I),I=1,NTHETA)        DYN01760
      C
C2      READ IN QN1      INITIAL DISPLACEMENTS  Q0      DYN01770
C2C     QN      INITIAL VELOCITIES    Q0DOT             DYN01780
C2C     XN      STIFFNESS MATRIX      K                DYN01790
C2C     XP      MASS MATRIX          M                DYN01800
C2C     FORCE LOADS                         DYN01810
C2C     NODRES NUMBER OF NODAL RESTRAINTS DYN01820
C2C     LK      LOCATION OF RESTRAINTS      DYN01822
      C
0078      PI=3.14159                                 DYN01824
0079      RAD=PI/180.                                DYN01826
      C
0080      DO 120 I=1,NTHETA                          DYN01828
0081      THETA(I)=THETA(I)*RAD                     DYN01830
0082      120     CONTINUE                                DYN01832
      C
0083      NNODES=NELEMS+1                           DYN01834
0084      NEQ=4*NNODES                             DYN01840
0085      NEQT=NH*NEQ                                DYN01850
0086      NSIZE=10+26*NELEMS                        DYN01860
0087      NHNS=NH*NSIZE                            DYN01870
0088      DT2=DELTE**2                                DYN01880
      C

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0089      DO 130 I=1,NEQT                      DYN02020
0090          QN(I)=0.0                         DYN02030
0091          QN1(I)=0.0                        DYN02040
0092      130 CONTINUE                           DYN02050
0093      C                                     DYN02053
0094          C1        RESTART//YES(250)           DYN02055
0095          IF (IRSTRT.EQ.1) GO TO 250         DYN02060
0096          C1        READ NODAL RESTRAINT AND INITIAL CONDITIONS CARDS. DYN02062
0097          C         READ INPUT DATA FOR CARD TYPE VI - A             DYN02100
0098          READ (ND,780) NODRES                DYN02110
0099          WRITE (6,830) NODRES                 DYN02120
0100          IF (NODRES.EQ.0) GO TO 150          DYN02130
0101          C                                     DYN02138
0102          DO 140 I=1,NODRES                  DYN02140
0103          C         READ INPUT DATA FOR CARD TYPE VI - B             DYN02150
0104          READ (ND,780) NP,NDIRCT              DYN02160
0105          WRITE (6,840) NP,NDIRCT              DYN02170
0106          LK(I)=4*(NP-1)+NDIRCT               DYN02180
0107          140 CONTINUE                           DYN02182
0108          C                                     DYN02185
0109          150 LK(NODRES+1)=3                   DYN02190
0110          LK(NODRES+2)=4                     DYN02200
0111          C2        READ AND PRINT INITIAL VELOCITIES AND DISPLACEMENTS DYN02202
0112          C         READ INPUT DATA FOR CARD TYPE VII - A             DYN02240
0113          READ (ND,780) IQN,IQN1                DYN02250
0114          IF (IQN.EQ.0) GO TO 190              DYN02260
0115          C                                     DYN02268
0116          DO 180 IH=1,NH                      DYN02270
0117          N=NEQ*(IH-1)                         DYN02280
0118          C2        READ INPUT DATA FOR CARD TYPE VII - B             DYN02282
0119          160 READ (ND,850) IN1,IN2,Q1,Q2,Q3,Q4          DYN02300
0120          C                                     DYN02308
0121          DO 170 INODE=IN1,IN2                DYN02310
0122          IFLAG=4*(INODE-1)+N                 DYN02320
0123          QN(IFLAG+1)=Q1                     DYN02330
0124          QN(IFLAG+2)=Q2                     DYN02340
0125          QN(IFLAG+3)=Q3                     DYN02350
0126          QN(IFLAG+4)=Q4                     DYN02360
0127          170 CONTINUE                           DYN02362
0128          C                                     DYN02365
0129          IF (IN2.NE.NNODES) GO TO 160          DYN02370
0130          180 CONTINUE                           DYN02380
0131          C                                     DYN02383
0132          190 CONTINUE                           DYN02390
0133          IF (IQN1.EQ.0) GO TO 230              DYN02400
0134          C                                     DYN02408
0135          DO 220 IH=1,NH                      DYN02410
0136          N=NEQ*(IH-1)                         DYN02420

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0122      C2      READ INPUT DATA FOR CARD TYPE VII - C          DYN02422
0122      200     READ (ND,850) IN1,IN2,Q1,Q2,Q3,Q4          DYN02440
0122      C
0123      DO 210 INODE=IN1,IN2          DYN02448
0124      IFLAG=4*(INODE-1)+N          DYN02450
0125      QN1(IFLAG+1)=Q1          DYN02460
0126      QN1(IFLAG+2)=Q2          DYN02470
0127      QN1(IFLAG+3)=Q3          DYN02480
0128      QN1(IFLAG+4)=Q4          DYN02490
0129      210     CONTINUE          DYN02500
0130      C
0130      IF (IN2.NE.NNODES) GO TO 200          DYN02502
0131      220     CONTINUE          DYN02505
0131      C
0132      230     CONTINUE          DYN02510
0133      WRITE (6,860)          DYN02520
0133      C
0134      DO 240 I=1,NH          DYN02523
0135      IQ=NEQ*(I-1)
0135      C
0136      DO 240 II=1,NNODES          DYN02530
0137      IX=4*(II-1)
0138      WRITE (6,870) II,IHARM(I),QN(IQ+IX+1),QN(IQ+IX+2),
0138      1           QN(IQ+IX+3),QN(IQ+IX+4),QN1(IQ+IX+1),QN1(IQ+IX+2),
0138      1           QN1(IQ+IX+3),QN1(IQ+IX+4)          DYN02540
0139      240     CONTINUE          DYN02550
0139      C
0140      250     CONTINUE          DYN02560
0141      REWIND NS          DYN02568
0141      C2      READ STRUCTURAL DATA FOR SHELL          DYN02570
0141      C
0142      DO 260 II=1,NELEMS          DYN02580
0143      READ (NT) ((CHECK(I,J),I=1,8),J=1,8),(AL(I),I=1,166)          DYN02590
0144      WRITE (NS) ((CHECK(I,J),I=1,8),J=1,8),(AL(I),I=1,166)          DYN02600
0145      260     CONTINUE          DYN02610
0145      C
0146      READ (NT) (FNU1(I),I=1,NELEMS),(FNU2(I),I=1,NELEMS),(E1(I),I=1,
0146      1           NELEMS),(E2(I),I=1,NELEMS),(G(I),I=1,NELEMS),(T(I),I=1,
0146      1           NELEMS)          DYN02620
0147      C
0147      DO 280 I=1,NELEMS          DYN02630
0148      IF (I.EQ.NELEMS) GO TO 270          DYN02632
0149      READ (NT) R(I),PH(I),PHP(I),ARCL(I),SINE(I),COSINE(I)          DYN02640
0150      GO TO 280          DYN02650
0151      270     READ (NT) R(I),PH(I),PHP(I),ARCL(I),SINE(I),COSINE(I),
0151      1           SINE(I+1),COSINE(I+1)          DYN02660
0152      280     CONTINUE          DYN02670
0152      C
  
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0153      READ (NT) (RO(I),I=1,NNODES),(Z(I),I=1,NNODES)          DYN02770
          C
0154      DO 290 I=1,NELEMS                                     DYN02778
0155          COSM(I)=DCOS(PH(I))                                DYN02780
0156          SINM(I)=DSIN(PH(I))                                DYN02790
0157      290 CONTINUE                                         DYN02800
          C1 INCLUDE THERMAL LOADS//NO(320)                      DYN02810
          C
0158      IF (ITELF.NE.1) GO TO 320                            DYN02815
          C1 READ COEFFICIENTS OF THERMAL EXPANSION CARDS       DYN02820
          C2 READ INPUT DATA FOR CARD TYPE VIII                  DYN02822
0159      300 READ (ND,880) IELM1,IELM2,ALSI1,ALT11            DYN02824
          C
0160      DO 310 IELM=IELM1,IELM2                           DYN02870
0161          ALS(IELM)=ALSI1                                 DYN02878
0162          ALT(IELM)=ALT11                                DYN02880
0163      310 CONTINUE                                         DYN02890
          C
0164      IF (IELM2.NE.NELEMS) GO TO 300                      DYN02900
0165      GO TO 340                                           DYN02902
          C
0166      320 DO 330 IELM=1,NELEMS                         DYN02905
0167          ALS(IELM)=0.0                                  DYN02910
0168          ALT(IELM)=0.0                                  DYN02920
0169      330 CONTINUE                                         DYN02928
          C
0170      340 CONTINUE                                         DYN02930
          C2 PRINT ELEMENT PROPERTIES AND DESIRED STIFFNESS AND MASS MATRICES DYN02970
0171          WRITE (6,890)
0172          WRITE (6,900) (I,ALSI(I),ALT(I),E1(I),E2(I),FNU1(I),FNU2(I),G(I),
0173              1           R(I),T(I),ARCL(I),PH(I),PHP(I),I=1,NELEMS) DYN03010
          C
0174      DO 370 IH=1,NHP                                       DYN03020
          C
0175          DO 350 JH=1,NH                                     DYN03030
0176              IF (IH-1.EQ.IHARM(JH)) GO TO 360             DYN03038
0177          350 CONTINUE                                         DYN03040
          C
0178          READ (NT) (FORCE(I),I=1,NSIZE)                   DYN03048
0179          READ (NT) (FORCE(I),I=1,NSIZE)                   DYN03050
0180          GO TO 370                                         DYN03060
          C
0181          360 CONTINUE                                         DYN03070
0182          NN=NSIZE*(JH-1)                                 DYN03073
0183          READ (NT) (XN(I+NN),I=1,NSIZE)                   DYN03080
0184          READ (NT) (XP(I+NN),I=1,NSIZE)                   DYN03090
0185          IF (NPRNMS.EQ.0) GO TO 370                     DYN03100
0186          WRITE (6,910) IHARM(JH)                          DYN03110
0187          WRITE (6,920) (XN(I+NN),I=1,NSIZE)               DYN03120

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 0187 WRITE (6,930) IHARM(JH) DYN03180
 0188 WRITE (6,920) (XP(I+NN),I=1,NSIZE) DYN03190
 0189 370 CONTINUE DYN03200
 C DYN03203
 C1 CALCULATE TRIGONOMETRIC INTEGRALS REQUIRED TO CALCULATE DYN03205
 C1C GENERALIZED NONLINEAR LOADS DYN03207
 0190 CALL TRI40R DYN03210
 C1 RESTART//NO(400) DYN03212
 0191 IF (IRSTRT.EQ.0) GO TO 400 DYN03220
 C1 READ AND CALCULATE INFORMATION REQUIRED FOR RESTART OPERATION DYN03222
 0192 NTF=2*NEQT DYN03260
 0193 380 READ (NT) NH,(IHARM(I),I=1,NH),JUNK DYN03270
 0194 READ (NT) ITP,TIMEP,DELTEP,TO,T1,NODRES,(LK(I),I=1,NODRES), DYN03280
 1 (FORCE(I),I=1,NTF) DYN03290
 0195 READ (NT) (((TH(IELM,IH,IBP1),IELM=1,NELEMS),IH=1,NH),IBP1=1,2), DYN03300
 1 (((DTH(IELM,IH,IBP1),IELM=1,NELEMS),IH=1,NH),IBP1=1,2) DYN03310
 0196 READ (NT) (QP1(I),I=1,NEQT),(QN(I),I=1,NEQT),(QN1(I),I=1,NEQT) DYN03320
 0197 LK(NODRES+1)=3 DYN03330
 0198 LK(NCDRES+2)=4 DYN03340
 0199 IF (ITP.NE.INCRST) GO TO 380 DYN03350
 0200 C1 CALCULATE NONLINEAR LOADS AND STRESS RESULTANTS FOR EACH ELEMENT DYN03352
 CALL NLTERM (0) DYN03360
 C DYN03368
 0201 DO 390 I=1,NEQT DYN03370
 XKEEP=QN(I)
 0203 QN(I)=QN1(I) DYN03380
 0204 QN1(I)=XKEEP DYN03390
 0205 XKEEP=QP1(I) DYN03400
 0206 QP1(I)=QP(I) DYN03410
 0207 QP(I)=QP(I)+(DELTE/DELTEP)*(QP(I)-XKEEP) DYN03420
 0208 390 CONTINUE DYN03430
 C DYN03435
 C QP - GENERALIZED FORCES AT N+1 TH INCREMENT DYN03450
 C QP1 - GENERALIZED FORCES AT N TH INCREMENT DYN03460
 C QN - GENERALIZED NODAL VELOCITIES AT N TH INCREMENT DYN03470
 C QN1 - GENERALIZED NODAL DISP. AT N TH INCREMENT DYN03480
 C DYN03482
 0209 TPRNT=TIMEP*1000000. DYN03500
 0210 WRITE (6,940) ITP,TPRNT,DELTEP DYN03510
 0211 RETURN DYN03520
 0212 400 CONTINUE DYN03530
 C2 INITIALIZE FORCE AND THERMAL MATRICES DYN03532
 C DYN03568
 0213 DO 410 I=1,NEQT DYN03570
 FORCE(I)=0.0
 0214 FORCE(I+NEQT)=0.0 DYN03580
 0215 410 CONTINUE DYN03590
 C DYN03600
 0216 DYN03603

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0217	C	DYN03608
	DO 420 I=1,NELEMS	DYN03610
0218	C	DYN03618
	DO 420 J=1,NH	DYN03620
0219	TH(I,J,1)=0.0	DYN03630
0220	TH(I,J,2)=0.0	DYN03640
0221	DTH(I,J,1)=0.0	DYN03650
0222	DTH(I,J,2)=0.0	DYN03660
0223	420 CONTINUE	DYN03670
	C	DYN03673
0224	C1 FIRST TIME THROUGH AND CONSTANT FORCES//NO(440)	DYN03675
0225	430 IF (CONSTF.EQ.CONSTN.AND.KEY.NE.1) GO TO 440	DYN03710
	GO TO 470	DYN03720
	C1 UPDATE FORCE AND THERMAL MATRICES	DYN03722
0226	C	DYN03728
	440 DO 450 I=1,NEQT	DYN03730
0227	FORCE(I)=FORCE(I+NEQT)	DYN03740
0228	450 CONTINUE	DYN03742
	C	DYN03745
0229	C	DYN03748
	DO 460 I=1,NELEMS	DYN03750
0230	C	DYN03758
	DO 460 J=1,NH	DYN03760
0231	TH(I,J,1)=TH(I,J,2)	DYN03770
0232	DTH(I,J,1)=DTH(I,J,2)	DYN03780
0233	460 CONTINUE	DYN03782
	C	DYN03785
0234	T0=T1	DYN03790
0235	T1=TOTIME	DYN03800
0236	RETURN	DYN03810
0237	470 CONTINUE	DYN03820
	C	DYN03828
0238	DO 480 I=1,NEQT	DYN03830
0239	FORCE(I)=FORCE(I+NEQT)	DYN03840
0240	FORCE(I+NEQT)=0.0	DYN03850
0241	480 CONTINUE	DYN03860
	C	DYN03863
0242	C	DYN03868
	DO 490 I=1,NELEMS	DYN03870
0243	C	DYN03878
	DO 490 J=1,NH	DYN03880
0244	TH(I,J,1)=TH(I,J,2)	DYN03890
0245	DTH(I,J,1)=DTH(I,J,2)	DYN03900
0246	TH(I,J,2)=0.0	DYN03910
0247	DTH(I,J,2)=0.0	DYN03920
0248	490 CONTINUE	DYN03930
	C	DYN03933
0249	IB=0	DYN03940

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0250	IF (KEY.EQ.2) IB=1		DYN03950	
0251	IF (IB.EQ.1) T0=T1		DYN03960	
C1	READ LOAD CONTROL CARD		DYN03962	
0252	500 READ (ND,950) T1,NCF,IIDELF,ITCOE,CONSTF		DYN03980	
0253	TIM=T1		DYN03990	
0254	IF (CONSTF.EQ.CONSTN.AND.IB.EQ.0) T1=TOTIME		DYN04000	
0255	IF (NPRNTL.EQ.0.AND.NPRNTF.EQ.0) GO TO 510		DYN04010	
C2	PRINT LOADING DESCRIPTION		DYN04012	
0256	TPRNT=TIM*1000000.		DYN04050	
0257	WRITE (6,960) TPRNT,CONSTF		DYN04060	
C1	CONCENTRATED RING LOADS//NO(550)		DYN04062	
0258	510 IF (NCF.EQ.0) GO TO 550		DYN04070	
C1	READ CONCENTRATED RING LOADS		DYN04072	
C			DYN04078	
0259	DO 540 IH=1,NH		DYN04080	
0260	IHI=IH-1		DYN04090	
C	READ INPUT DATA FOR CARD TYPE IX - B - 1		DYN04100	
0261	READ (ND,970) NCF1		DYN04110	
0262	IF (NCF1.EQ.0) GO TO 540		DYN04120	
0263	IF (NPRNTL.EQ.0) GO TO 520		DYN04130	
0264	WRITE (6,980) IHARM(IH)		DYN04140	
C	READ INPUT DATA FOR CARD TYPE IX - B - 2		DYN04150	
0265	520 READ (ND,970) IN1,IN2,F1,F2,F3,F4		DYN04160	
C			DYN04168	
0266	DO 530 IN=IN1,IN2		DYN04170	
0267	K=4*IN+NEQ*IH1+IB*NEQT		DYN04180	
0268	FORCE(K-3)=F1		DYN04190	
0269	FORCE(K-2)=F2		DYN04200	
0270	FORCE(K-1)=F3		DYN04210	
0271	FORCE(K)=F4		DYN04220	
0272	IF (NPRNTL.EQ.1) WRITE (6,990) IN,F1,F2,F3,F4		DYN04230	
0273	530 CONTINUE		DYN04240	
C			DYN04243	
0274	IF (IN2.NE.NNODES) GO TO 520		DYN04250	
0275	540 CONTINUE		DYN04260	
C			DYN04263	
0276	550 CONTINUE		DYN04270	
C1	DISTRIBUTED LOADS PRESENT//NO(57C)		DYN04272	
0277	IF (IIDELF.NE.1) GO TO 570		DYN04280	
0278	REWIND NS		DYN04290	
C100	PROCESS ALL ELEMENTS		DYN04292	
C			DYN04298	
0279	DO 560 IELM=1,NELEMS		DYN04300	
0280	READ (NS) ((CHECK(I,J),I=1,8),J=1,8),(AL(I),I=1,166)		DYN04310	
C1	READ DISTRIBUTED LOADS AND CALCULATE LINEAR GENERALIZED FORCES		DYN04312	
0281	CALL FRCES (IELM,ALPHK,IB)		DYN04320	
0282	560 CONTINUE		DYN04330	
C			DYN04333	

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C1    THERMAL LOADS PRESENT//NO(650)          DYN04335
0283   570 IF (ITELF.EQ.0) GO TO 650          DYNC4340
0284   REWIND NS                                DYNC4380
0285   IBP1=IB+1                                DYNC4390
C1    READ THERMAL COEFICIENTS//NO(600)        DYN04392
0286   IF (ITCOE.EQ.0) GO TO 600                DYN04400
C1    READ TEMPERATURE DISTRIBUTIONS AND GRADIENTS DYN04402
0287   580 READ (ND,1000) IELM1,IELM2,(TH1(IH),DTH1(IH),IH=1,NH) DYN04420
C      DO 590 IELM=IELM1,IELM2                  DYN04428
C      DO 590 IH=1,NH                          DYN04430
0289   DTHIELM,IH,IBP1)=DTH1(IH)              DYN04438
0290   THIELM,IH,IBP1)=TH1(IH)                  DYN04440
0291   590 CONTINUE                                DYN04450
0292   C                                         DYN04460
0293   IF (IELM2.NE.NELEMS) GO TO 580          DYN04462
C100  PROCESS ALL ELEMENTS                    DYN04465
C      C                                         DYN04470
0294   600 DO 620 IELM=1,NELEMS                DYN04472
0295   READ (NS)((CHECK(I,J),I=1,8),J=1,8),(AL(I),I=1,166) DYN04478
C1    CALCULATE THERMAL COEFFICIENTS//NO(610) DYN04480
0296   IF (ITCOE.EQ.1) GO TO 610                DYN04490
C1    READS TEMPERATURE AND TEMPERATURE GRADIENTS AND CALCULATES DYN04492
C1C   THERMAL FOURIER COEFFICIENTS           DYN04500
0297   CALL THCOE (IELM,IB)                      DYN04502
C1    CALCULATES LINEAR THERMAL LOADS         DYN04504
0298   610 CALL TFORCE (IELM,IB)                 DYN04510
0299   620 CONTINUE                                DYN04512
C      C                                         DYN04520
0300   IF (NPRNTH.EQ.0) GO TO 640              DYN04530
C      C                                         DYN04533
0301   DO 630 IH=1,NH                          DYN04540
0302   WRITE (6,1010) IHARM(IH)                 DYN04548
C      C                                         DYN04550
0303   DO 630 IELM=1,NELEMS                   DYN04560
0304   WRITE (6,1020) IELM,THIELM,IH,IBP1),DTHIELM,IH,IBP1) DYN04568
0305   630 CONTINUE                                DYN04570
C      C                                         DYN04580
0306   640 CONTINUE                                DYN04582
0307   650 IF (NPRNTF.EQ.0) GO TO 670          DYN04585
C2    PRINT GENERALIZED FORCES FOR EACH HARMONIC DYN04590
C      C                                         DYN04600
0308   DO 660 IH=1,NH                          DYN04602
0309   KK=NEQ*(IH-1)+IB*NEQT                  DYN04638
0310   KYP=IHARM(IH)                            DYN04640
0311   WRITE (6,1030) KYP                      DYN04650
C      C                                         DYN04660
0308   DO 660 IH=1,NH                          DYN04670
0309   KK=NEQ*(IH-1)+IB*NEQT                  DYN04678
0310   KYP=IHARM(IH)
0311   WRITE (6,1030) KYP
C

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0312      DO 660 I=1,NNODES          DYN04680
0313      K=KK+4*(I-1)            DYN04690
0314      WRITE (6,1040) I,FORCE(K+1),FORCE(K+2),FORCE(K+3),FORCE(K+4) DYN04700
0315      660 CONTINUE           DYN04702
0316      C                      DYN04705
0317      670 CONTINUE           DYN04710
0318      C1                     FORCES NOT CONSTANT OR FIRST TIME THROUGH WITH KEY=2//YES(700) DYN04712
0319      IF (CONSTF.NE.CONSTN.OR.IB.EQ.1) GO TO 700 DYN04720
0320      C                      DYN04728
0321      DO 680 I=1,NEQT          DYN04730
0322      FORCE(I+NEQT)=FORCE(I) DYN04740
0323      680 CONTINUE           DYN04742
0324      C                      DYN04745
0325      C                      DYN04748
0326      DO 690 I=1,NELEMS        DYN04750
0327      C                      DYN04758
0328      DO 690 J=1,NH            DYN04760
0329      TH(I,J,2)=TH(I,J,1)     DYN04770
0330      DTH(I,J,2)=DTH(I,J,1)   DYN04780
0331      690 CONTINUE           DYN04790
0332      C                      DYN04793
0333      RETURN                 DYN04800
0334      700 CONTINUE           DYN04810
0335      IB=IB+1                DYN04820
0336      C1                     KEY = 1 //YES(500) DYN04822
0337      IF (IB.EQ.1) GO TO 500 DYN04830
0338      RETURN                 DYN04840
0339      C1                     WRITE RESTART INFORMATION ON TAPE DYN04842
0340      710 CONTINUE           DYN04880
0341      NTF=2*NEQT             DYN04890
0342      WRITE (NT) NH,(IHARM(I),I=1,NH),JUNK DYN04900
0343      WRITE (NT) ITAM,TIME,DELTE,TC,T1,NODRES,(LK(I),I=1,NODRES), DYN04910
0344      1           (FORCE(I),I=1,NTF) DYN04920
0345      WRITE (NT) (((THIELM,IH,IBP1),IELM=1,NELEMS),IH=1,NH),IBP1=1,2, DYN04930
0346      1           (((DTHIELM,IH,IBP1),IELM=1,NELFMS),IH=1,NH),IBP1=1,2) DYN04940
0347      QDC3=1.0/(2.0*DELTE)   DYN04950
0348      QDC2=4.0*QDC3         DYN04960
0349      QDC1=3.0*QDC3         DYN04970
0350      C                      DO 720 I=1,NEQT DYN04978
0351      QP(I)=QDC1*QN(I)-QDC2*QN1(I)+QDC3*QN2(I) DYN04980
0352      720 CONTINUE           DYN04990
0353      C                      WRITE (NT) (QP(I),I=1,NEQT),(QN(I),I=1,NEQT),(QP(I),I=1,NEQT) DYN04992
0354      TPRNT=TIME*1000000.     DYN05000
0355      WRITE (6,1050) ITAM,TPRNT DYN05010
0356      RETURN                 DYN05020
0357      C                      QP(I)=QDC1*QN(I)-QDC2*QN1(I)+QDC3*QN2(I) DYN05030
0358      720 CONTINUE           DYN05040
  
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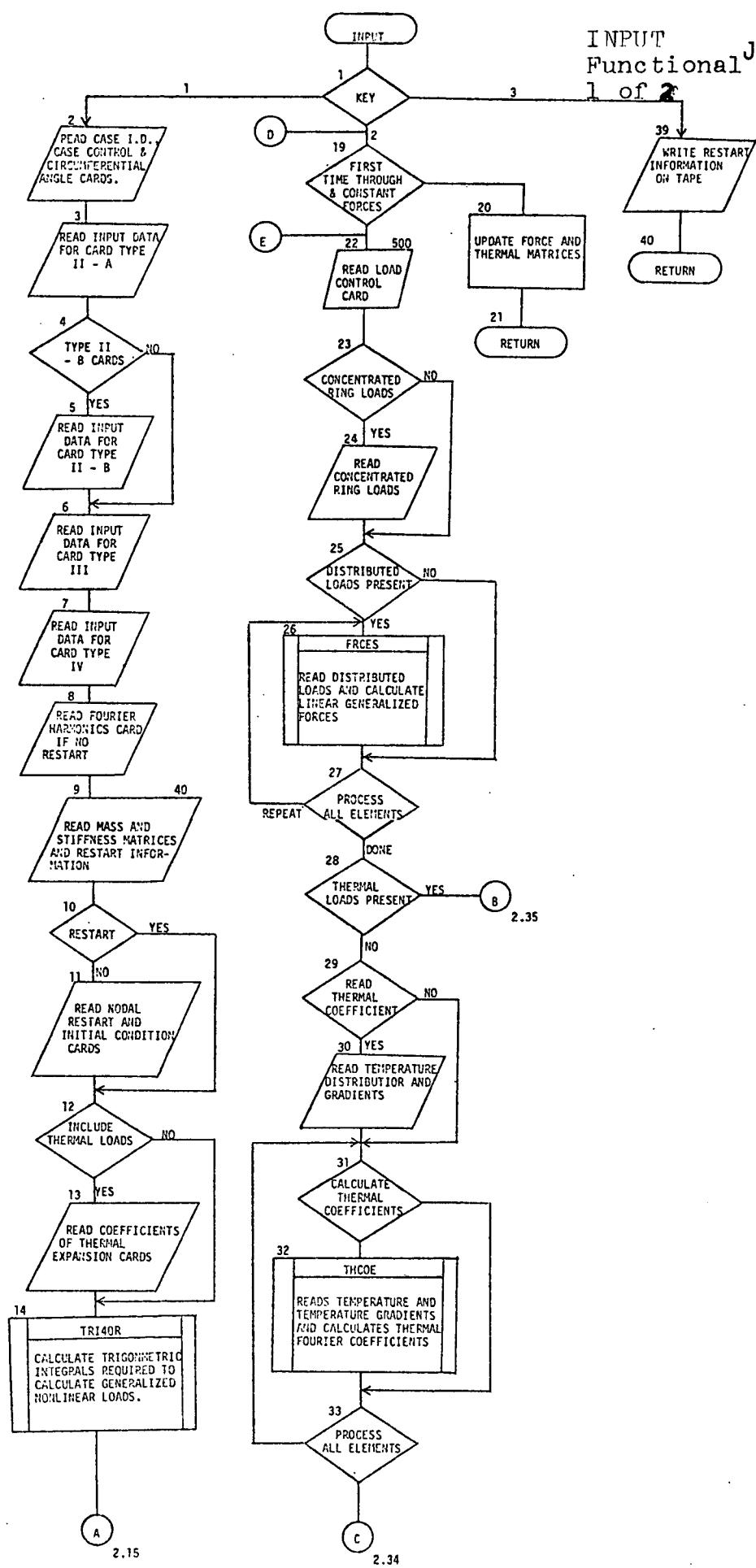
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0346      730 FORMAT (1H1,38X,44HDYNASOR-II - DYNAMIC NONLINEAR ANALYSIS OF, DYN05050
           1          21H SHELLS OF REVOLUTION//) DYN05060
0347      740 FORMAT (2I5) DYN05070
0348      750 FORMAT (20A4) DYN05080
0349      760 FORMAT (2F10.0,4I5,/,10I5) DYN05090
0350      770 FORMAT (I5,/, (8F10.0)) DYN05100
0351      780 FORMAT (16I5) DYN05110
0352      790 FORMAT (///,2X,46H**SHELL IDENTIFICATION COMMENTS FROM SAMMSOR**) DYN05120
0353      800 FORMAT (/5X,20A4) DYN05130
0354      810 FORMAT (1H1,50X,33HCONTROL CONSTANTS AND COMMENTS//)
           1          35X,8HTOTIME =,F12.9,22X,7HDELTE =,F13.9/ DYN05142
           1          35X,8HIRSTR =,I12,22X,8HINCRST =,I12/ DYN05144
           2          35X,7HNPRTN =,I13,22X,8HNPRNIT =,I12/ DYN05146
           2          35X,8HNPRTNTQ =,I12,22X,8HIPRINT =,I12/ DYN05148
           3          35X,8HNCLCST =,I12,22X,8HNSTRSS =,I12/ DYN05150
           3          35X,8HNPRNTL =,I12,22X,8HNPRNTF =,I12/ DYN05152
           4          35X,8HNPRNTH =,I12,22X,4HNT =,I16/ DYN05154
           4          35X,4HNS =,I16,22X,4HND =,I16,/ DYN05156
           5          35X,8HNCLOSE =,I12,22X,7HITLEF =,I13/ DYN05158
           5          35X,8HNELEMS =,I12,22X,8HNPRNMS =,I12/ DYN05160
           6          35X,4HNN =,I16/ DYN05162
           6          35X,7IHARM =,5I11//) DYN05164
0355      820 FORMAT (35X,8HNTHETA =,I12,/35X,7HTHETA =,5F10.2,(/,42X,5F10.2)) DYNC5210
0356      830 FORMAT (/////50X,29HNUMBER OF NODAL RESTRAINTS IS I15//)
           1          52X,9HDIRECTION,12X,7HAPPLIES// DYN05222
           1          57X,1H1,10X,15HAXIAL RESTRAINT/ DYN05230
           2          57X,1H2,10X,20HTANGENTIAL RESTRAINT//, DYN05232
           2          57X,1H3,10X,16HRADIAL RESTRAINT/ DYN05240
           3          57X,1H4,10X,17HANGULAR RESTRAINT//, DYN05242
           4          58X,15HNUODE DIPECTION//) DYN05250
0357      840 FORMAT (58X,I3,7X,I1) DYN05260
0358      850 FORMAT (2I5,4F10.0) DYN05270
0359      860 FORMAT (1H1,7X,7HINITIAL,29X,10HVELOCITIES,22X,3HAND,19X,
           1          13HDISPLACEMENTS// DYN05290
           1          4X,14HNODE HARMONIC,213CH AXIAL TANGENTIAL , DYNC5300
           2          26H RADIAL ANGULAR //) DYN05310
0360      870 FORMAT (5X,I2,6X,I2,3X,8D14.4) DYN05320
0361      880 FORMAT (2I5,2F10.0) DYN05330
0362      890 FORMAT (1H1,45X,41HELEMENT EL ASTIC AND GEOMETRIC PROPERTIES,///
           1          48H ELEMENT ALPHA--S ALPHA--T E1 E2 , DYN05342
           1          11H FNU1 FNU2,7X,1HG,11X,1HR,11X,1HT,9X,4HARCL,9X,2HPH, DYN05350
           2          10X,3HPHP//) DYN05360
0363      900 FORMAT (3X,I2,2X,4D10.2,2F6.3,6D12.4) DYN05370
0364      910 FORMAT (1H1,38X,15HHARMONIC NUMBER,I5, DYNC5380
           1          37H HAS THE FOLLOWING STIFFNESS MATRIX//) DYN05390
0365      920 FORMAT (2X,D16.8,/,2X,2D16.8,/,2X,3D16.8,/,2X,4D16.8,/,2X,5D16.8,/,DYN05400
           1          2X,6D16.8,/,2X,7D16.8,/,2X,8D16.8,/
           1          (2X,5D16.8,/,2X,6D16.8/2X,7D16.8/2X,8D16.8//) DYN05410
                                         DYN05420

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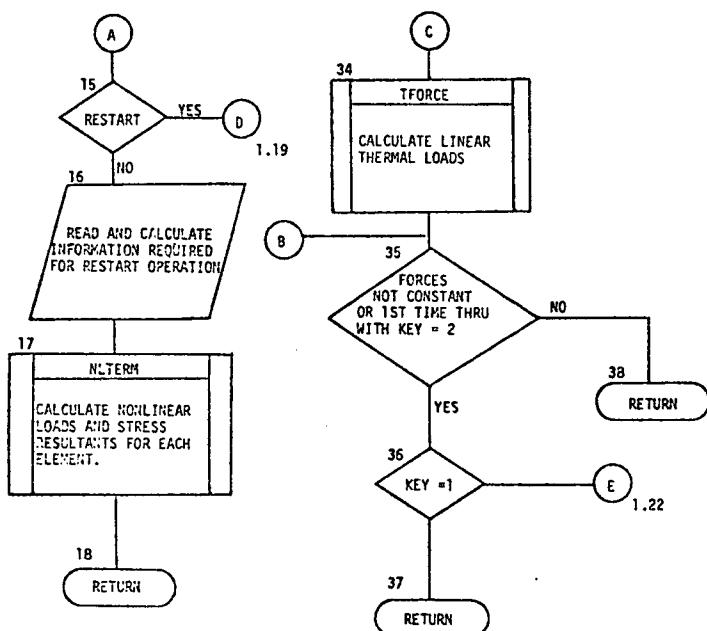
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0366	930 FORMAT (1H1,38X,15HHARMONIC NUMBER,I5, 1 32H HAS THE FOLLOWING MASS MATRIX//)		DYN05430 DYN05440	
0367	940 FORMAT (1H1////5X,41HTHIS SOLUTION STARTS AFTER TIME INCREMENT, 1 4H NO.,I5,19H WHERE THE TIME WAS,F12.4,13H MICROSECONDS./ 1 5X,27H AND THE TIME INCREMENT WAS,D12.5//://)		DYN05450 DYN05460 DYN05470	
0368	950 FORMAT (F10.0,4I5,A8)		DYN05480	
0369	960 FORMAT (40H1FOLLOWING IS LOAD DESCRIPTION AT TIME =,F12.4, 1 13H MICRCSECONDS,5X,A8)		DYN05490 DYN05500	
0370	970 FORMAT (2I5,4F10.0)		DYN05510	
0371	980 FORMAT (///20X,30HCONCENTRATED FORCES HARMONIC ,I5// 1 6X,8HNODE NO.,6X,5HAXIAL,10X,10HTANGENTIAL,10X,6HRADIAL, 1 7HANGULAR//)		DYN05520 DYN05530 DYN05532	
0372	990 FORMAT (I10,4D20.8)		DYN05540	
0373	1000 FORMAT (2I5,/(2F10.0))		DYN05550	
0374	1010 FORMAT (1H1,25X,39HTEMPERATURE COEFFICIENTS, HARMONIC NO. I3// 1 10X,11HELEMENT NO.,17X,12HTEMP. COEFF.,12X, 1 18HTEMP. GRAD. COEFF.///)		DYN05560 DYN05570 DYN05572	
0375	1020 FORMAT (I20,2D30.5)		DYN05580	
0376	1030 FORMAT (1H1,25X,32HGENERALIZED FORCES, HARMONIC NO.,I3,// 1 6X,8HNODE NO.,6X,5HAXIAL,13X,10HTANGENTIAL,11X,6HRADIAL, 1 13X,7HANGULAR///)		DYN05590 DYN05600 DYN05602	
0377	1040 FORMAT (I9,4D19.8)		DYN05610	
0378	1050 FORMAT (1H1////5X,42HRESTART INFORMATION FOR TIME INCREMENT NO., 1 I5/ 1 10X,22H CORRESPONDING TO TIME,F12.4,13H MICROSECONDS,/		DYN05620 DYN05622 DYN05630	
	2 2X,46H HAS BEEN PLACED ON TAPE FOR USE IN SUBSEQUENT, 2 5H RUNS//)		DYN05640 DYN05642	
0379	END		DYN05650	

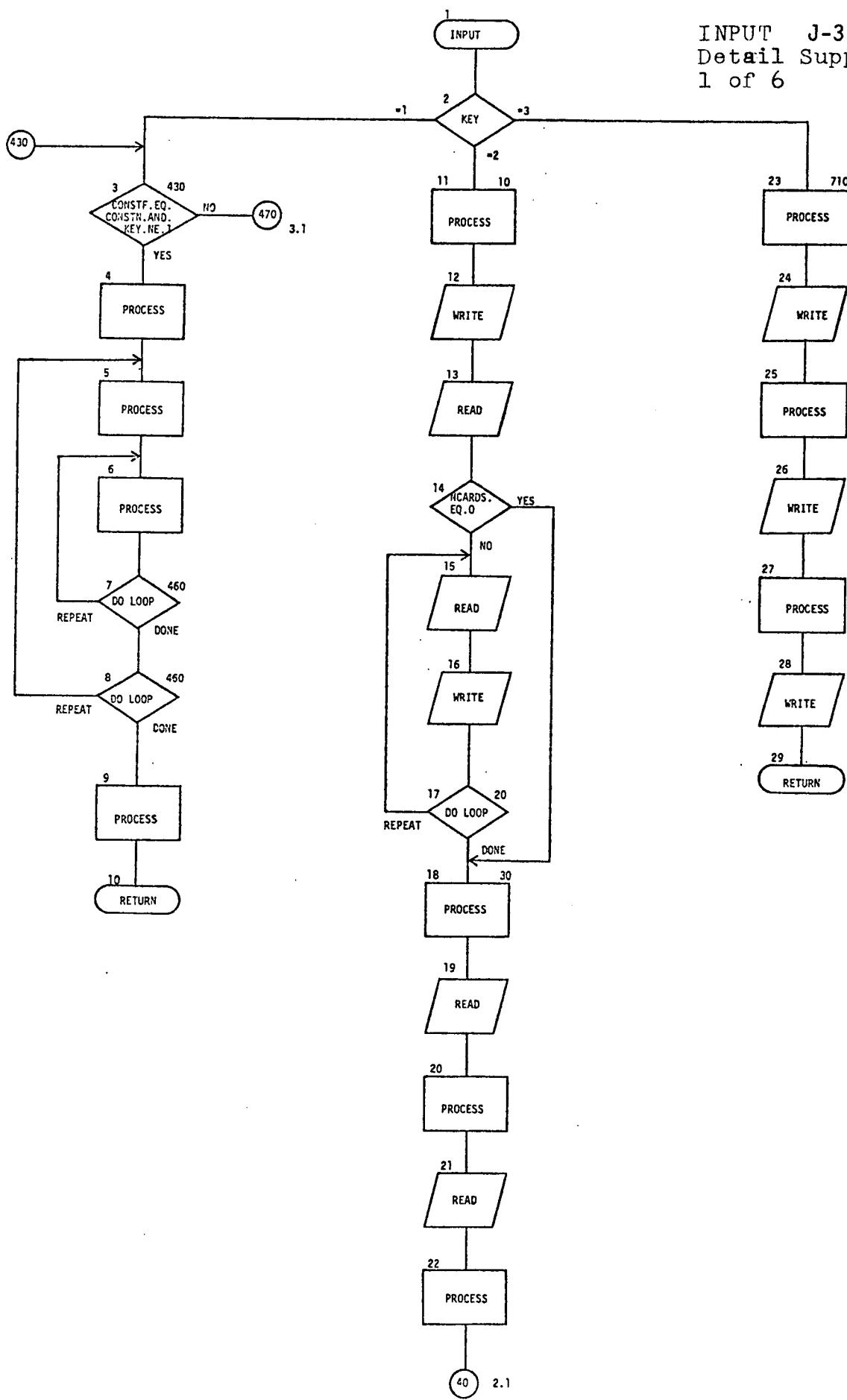
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1 of 2



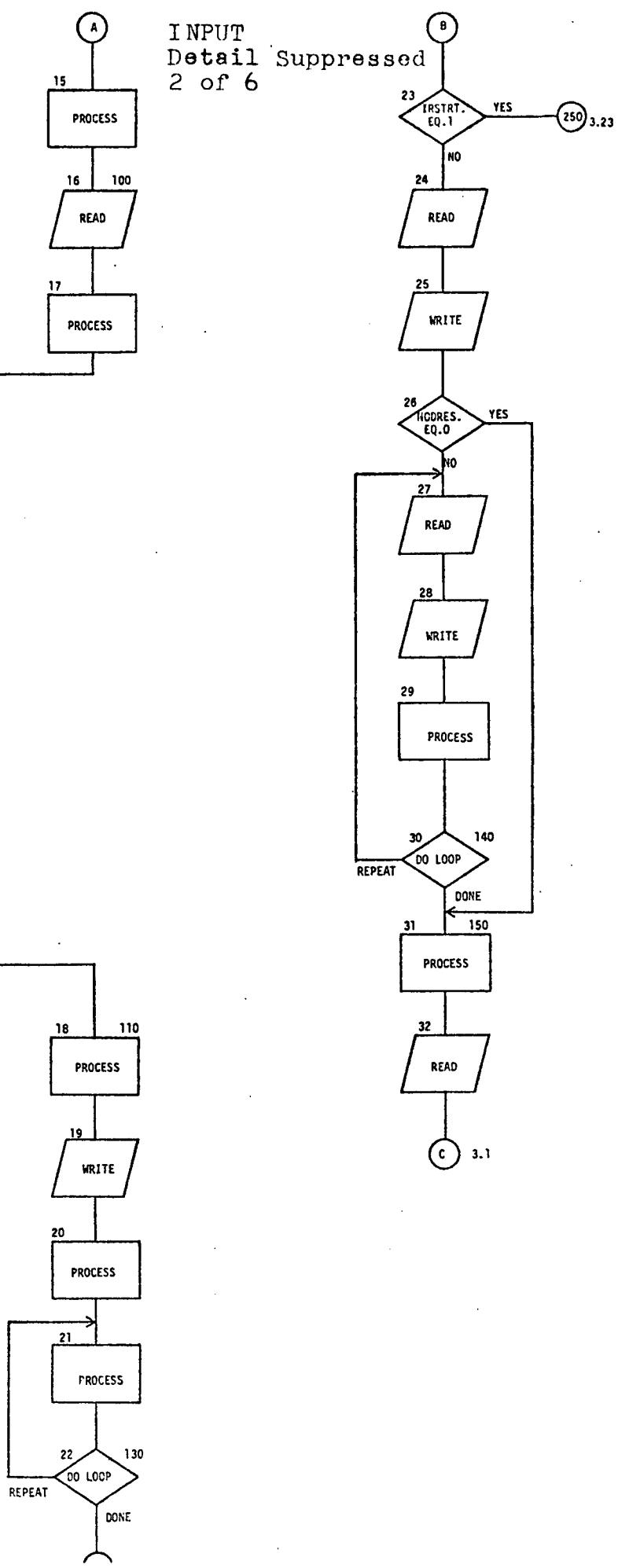
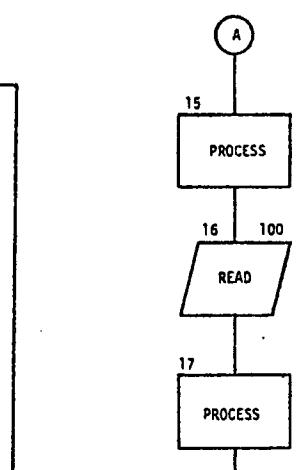
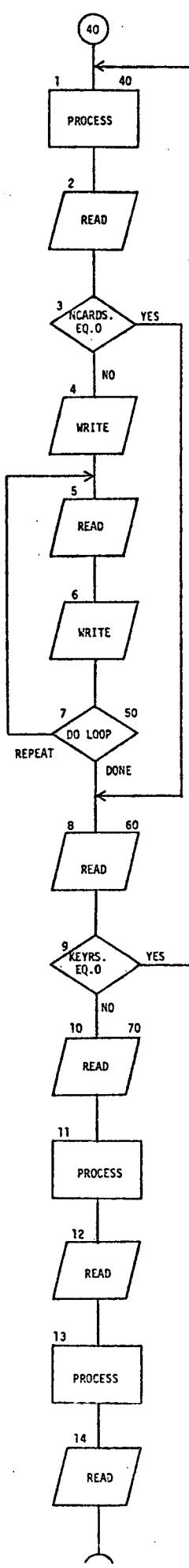
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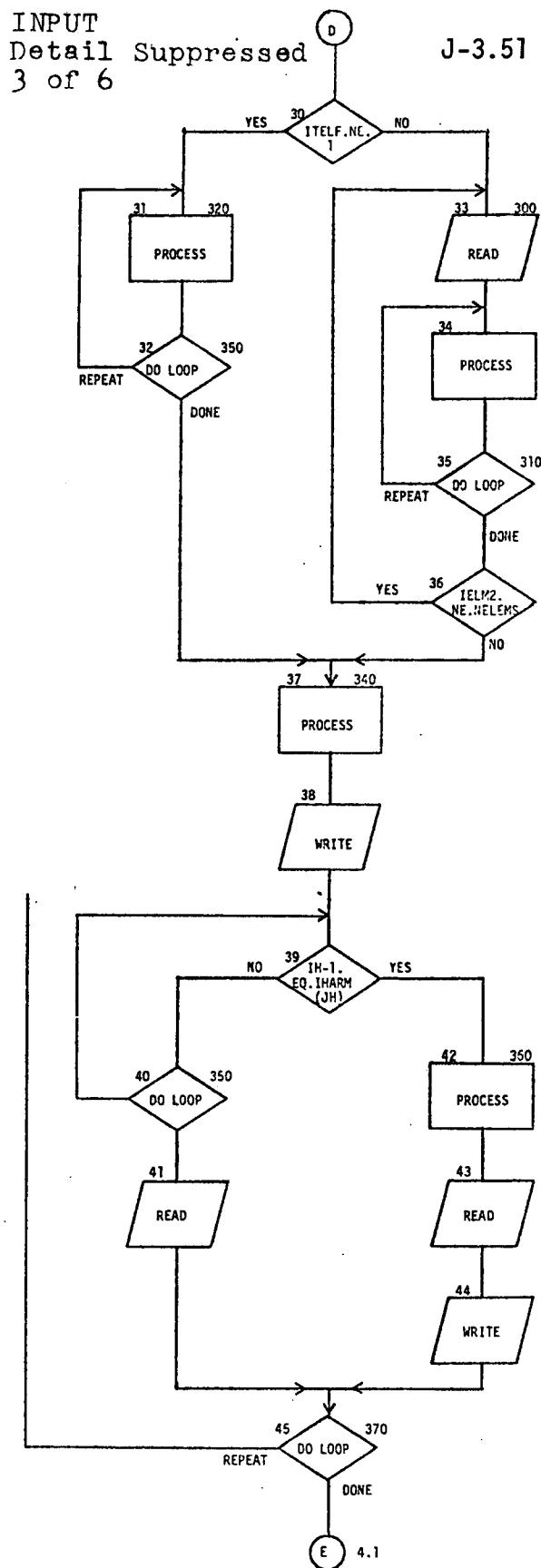
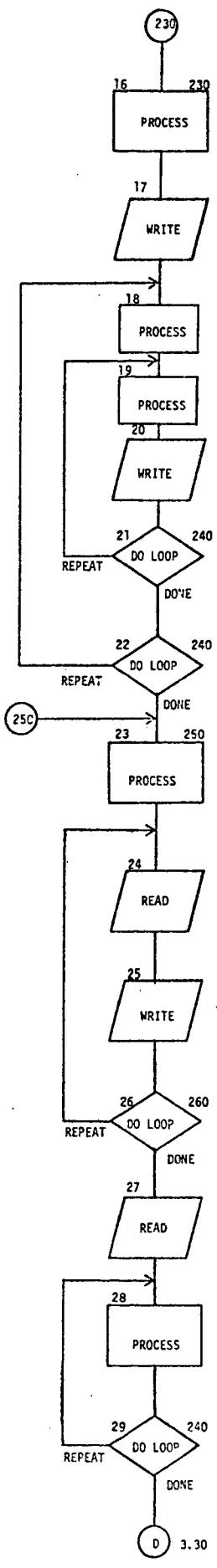
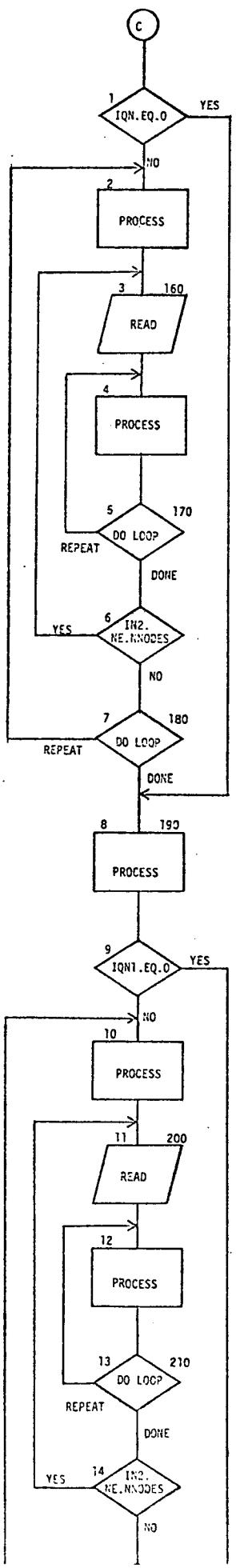
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2 of 2





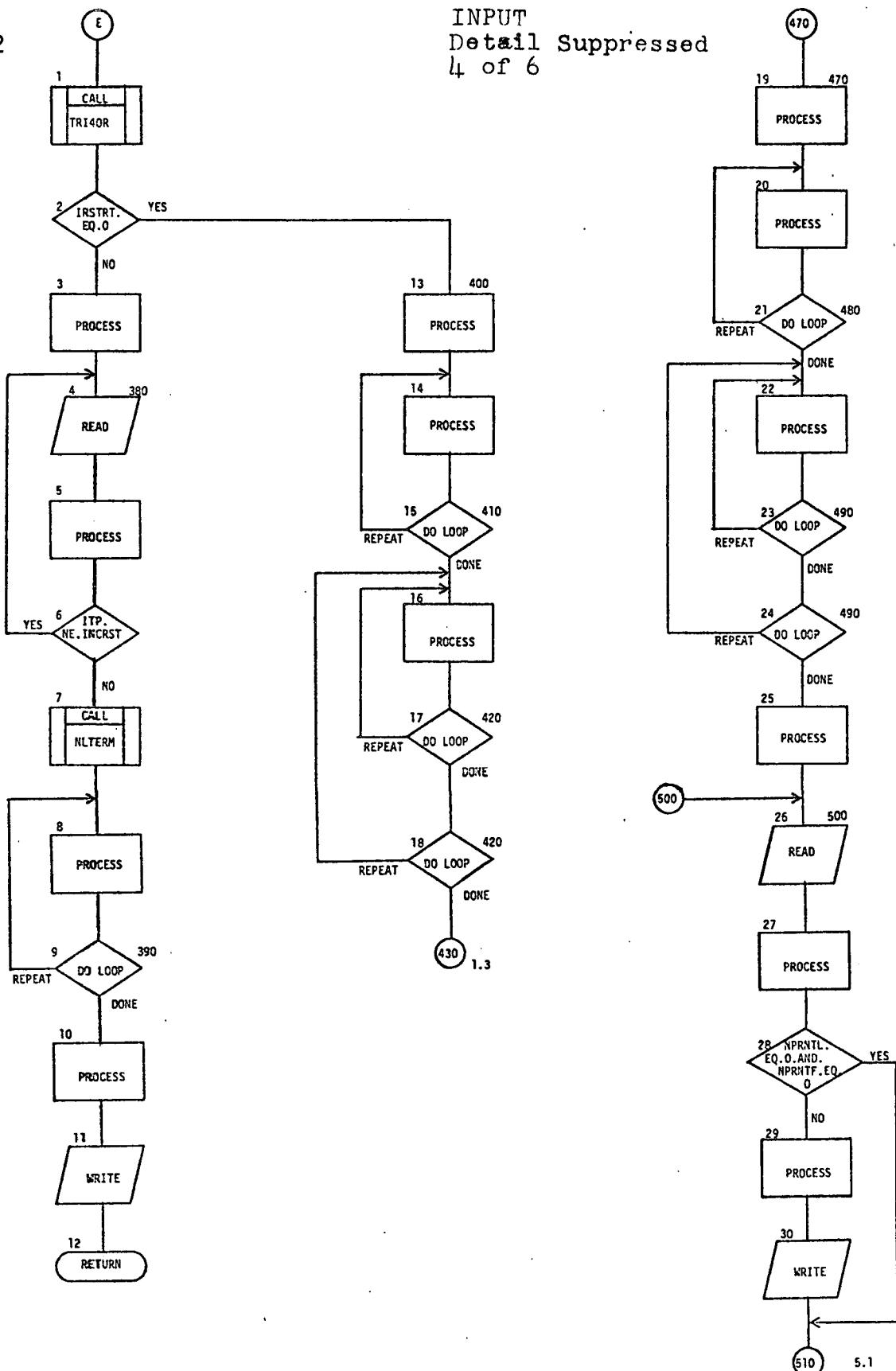
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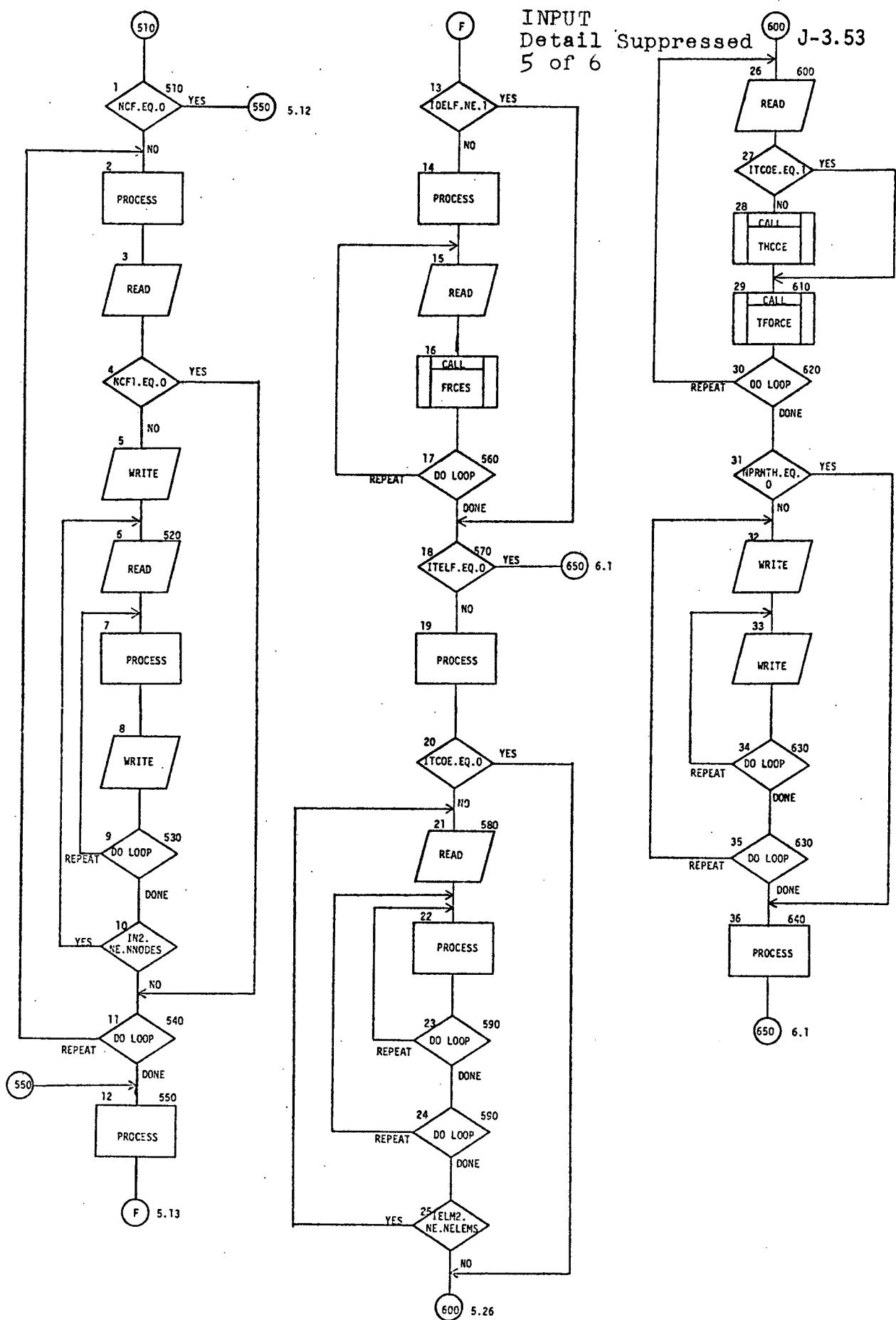


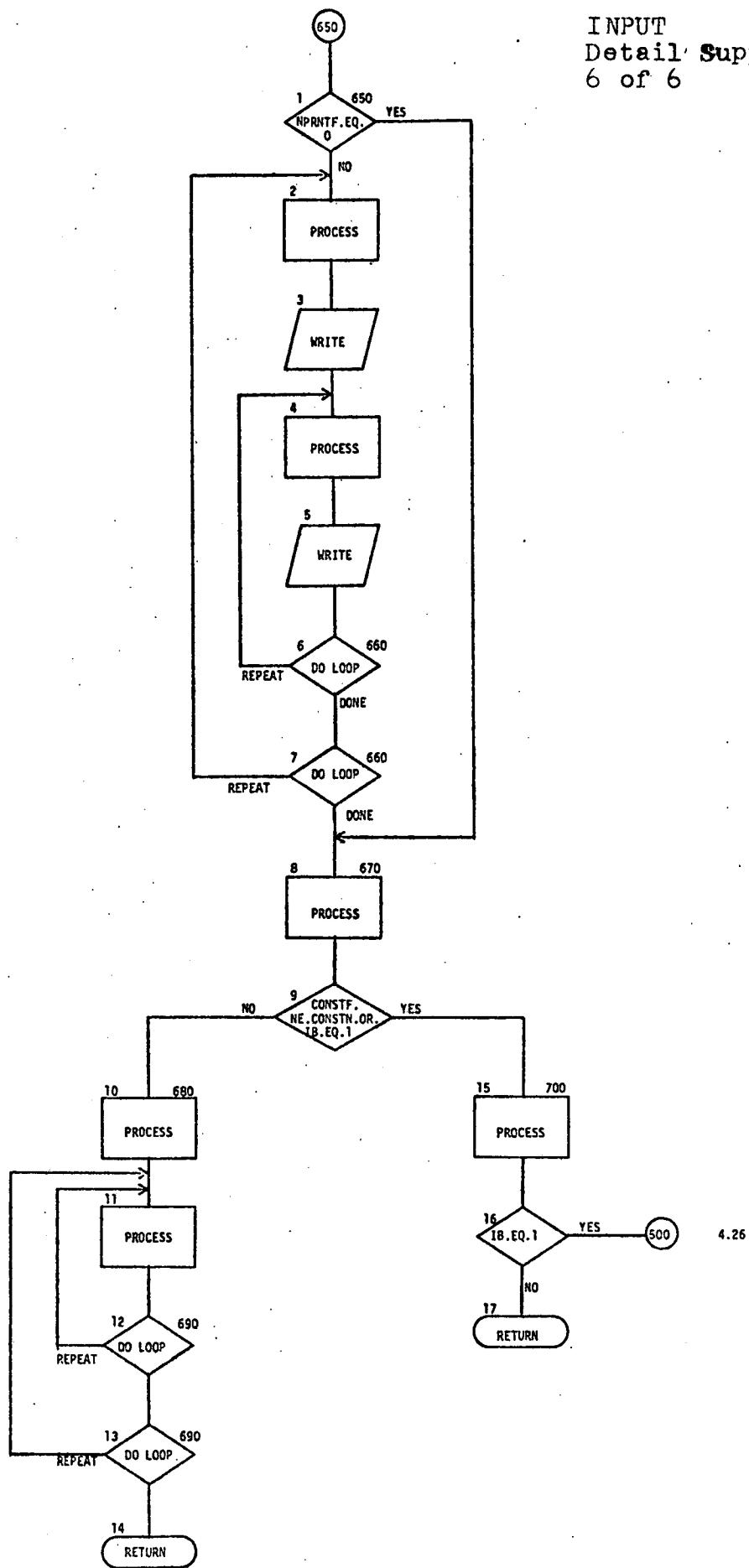
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INPUT
Detail Suppressed
4 of 6

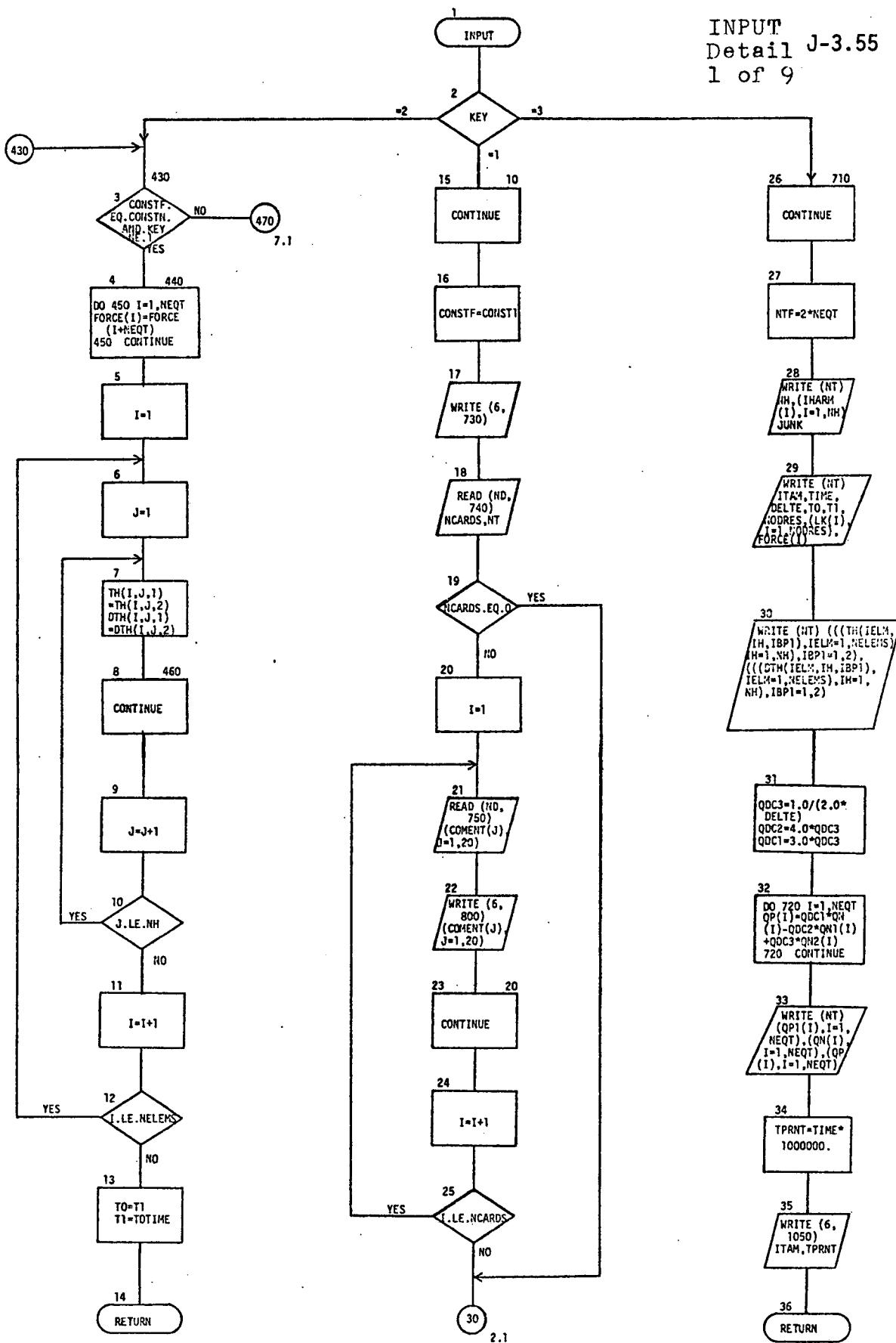


INPUT Detail Suppressed
5 of 6 J-3.53

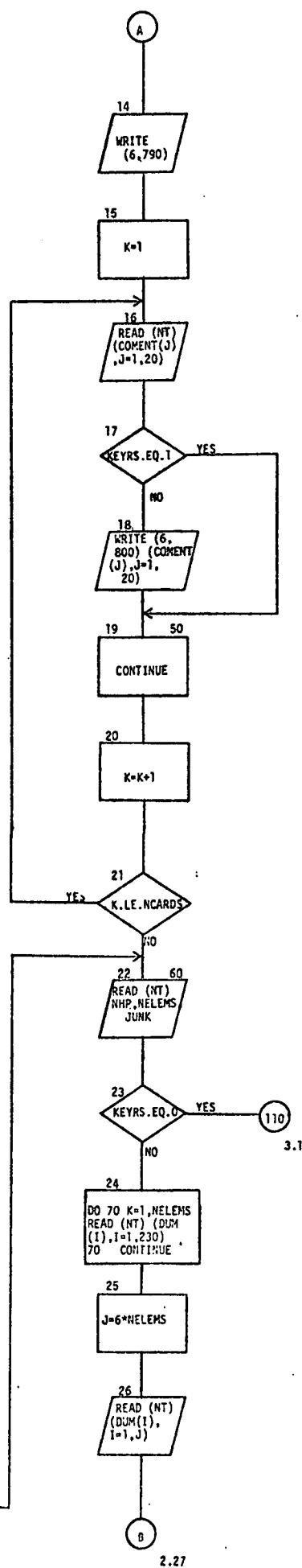
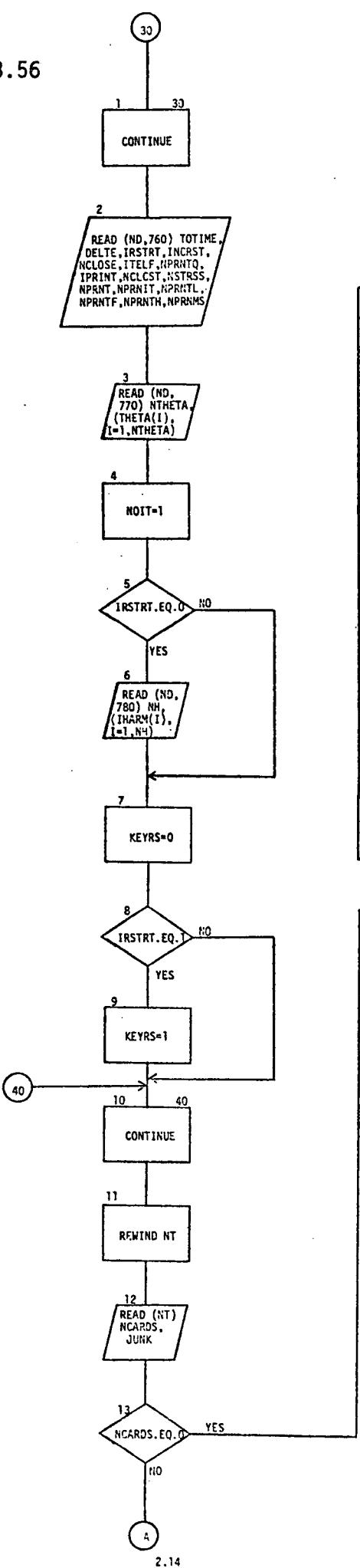
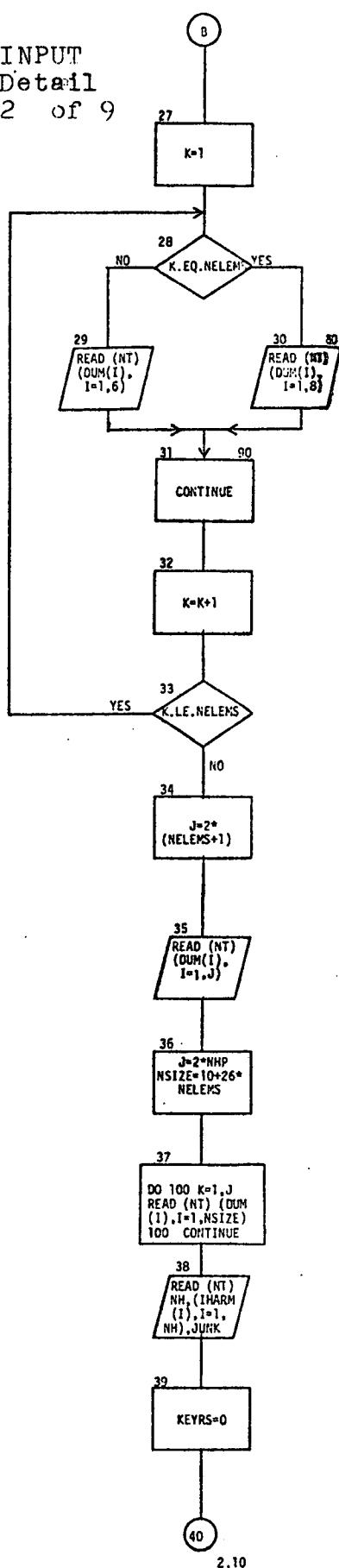


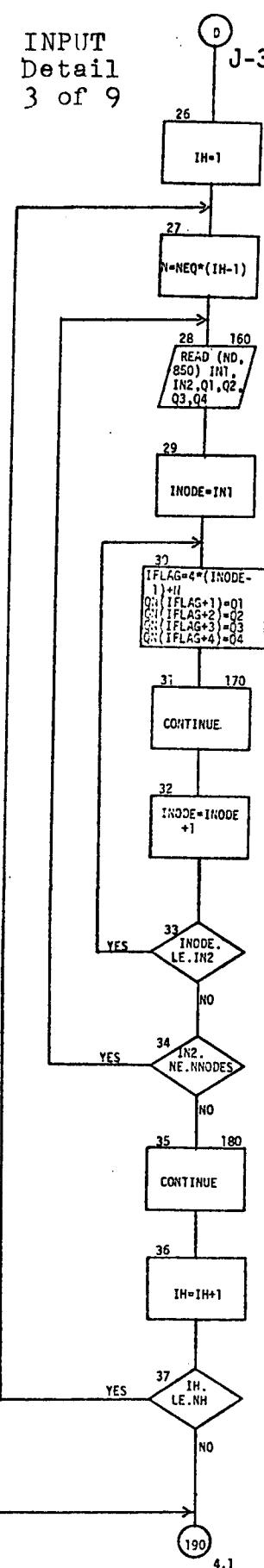
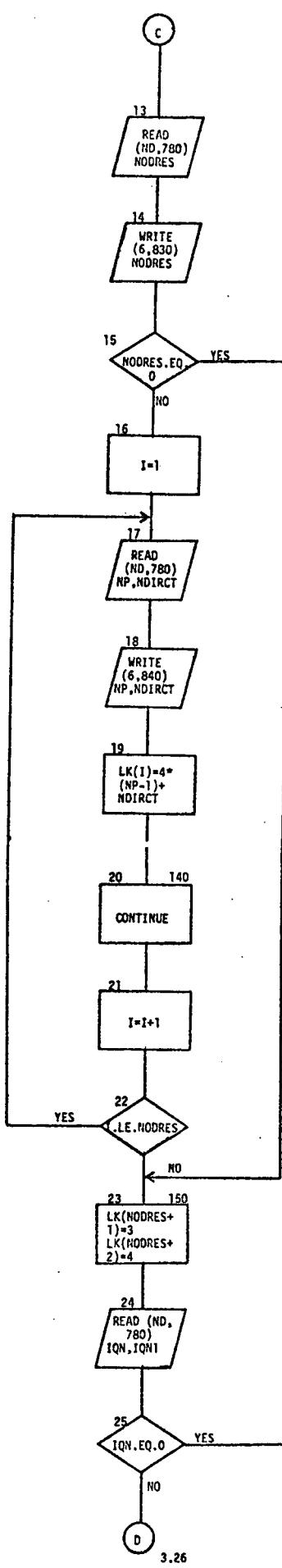
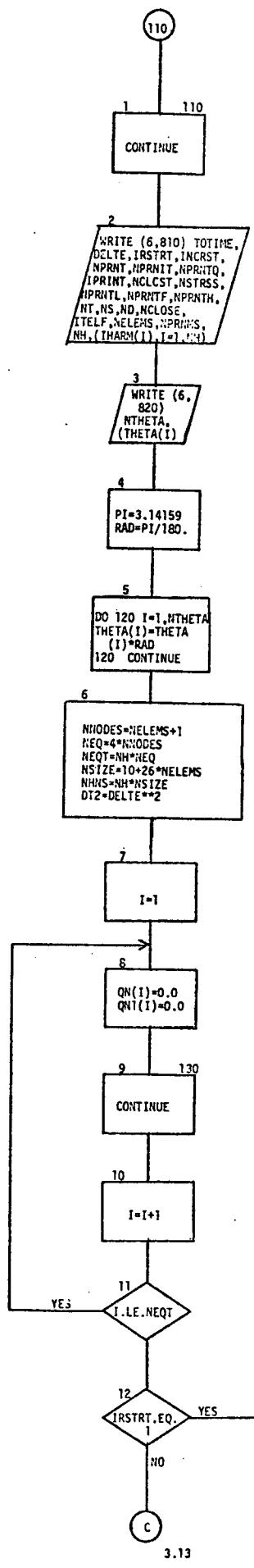


INPUT
Detail J-3.55
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J-3.56

INPUT Detail
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INPUT
Detail
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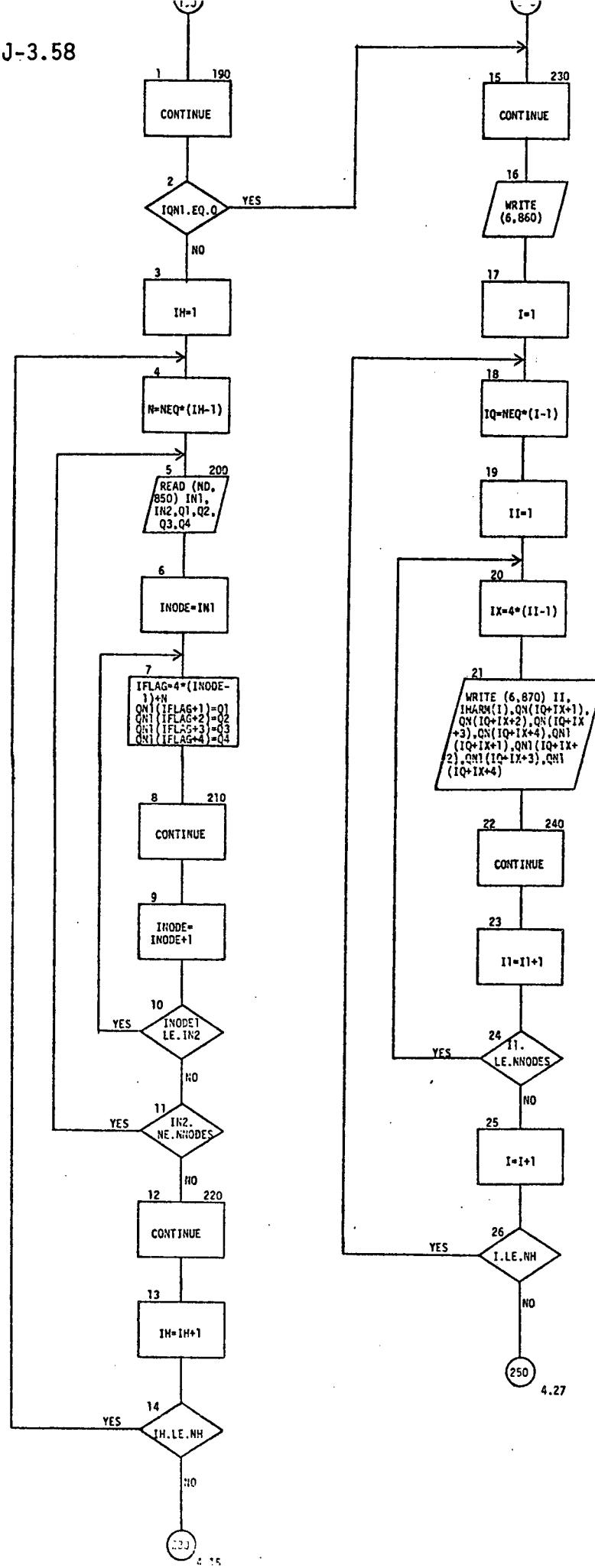
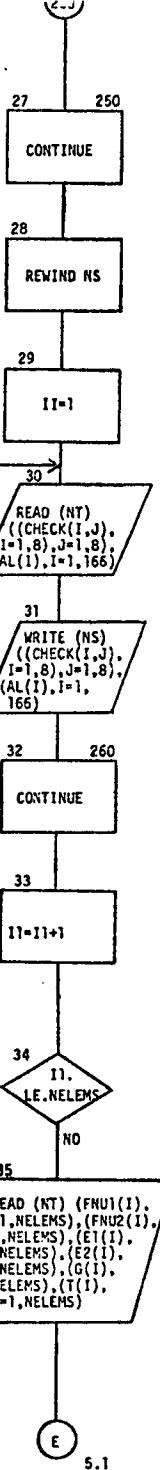
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3.13

3.26

41

J-3.58

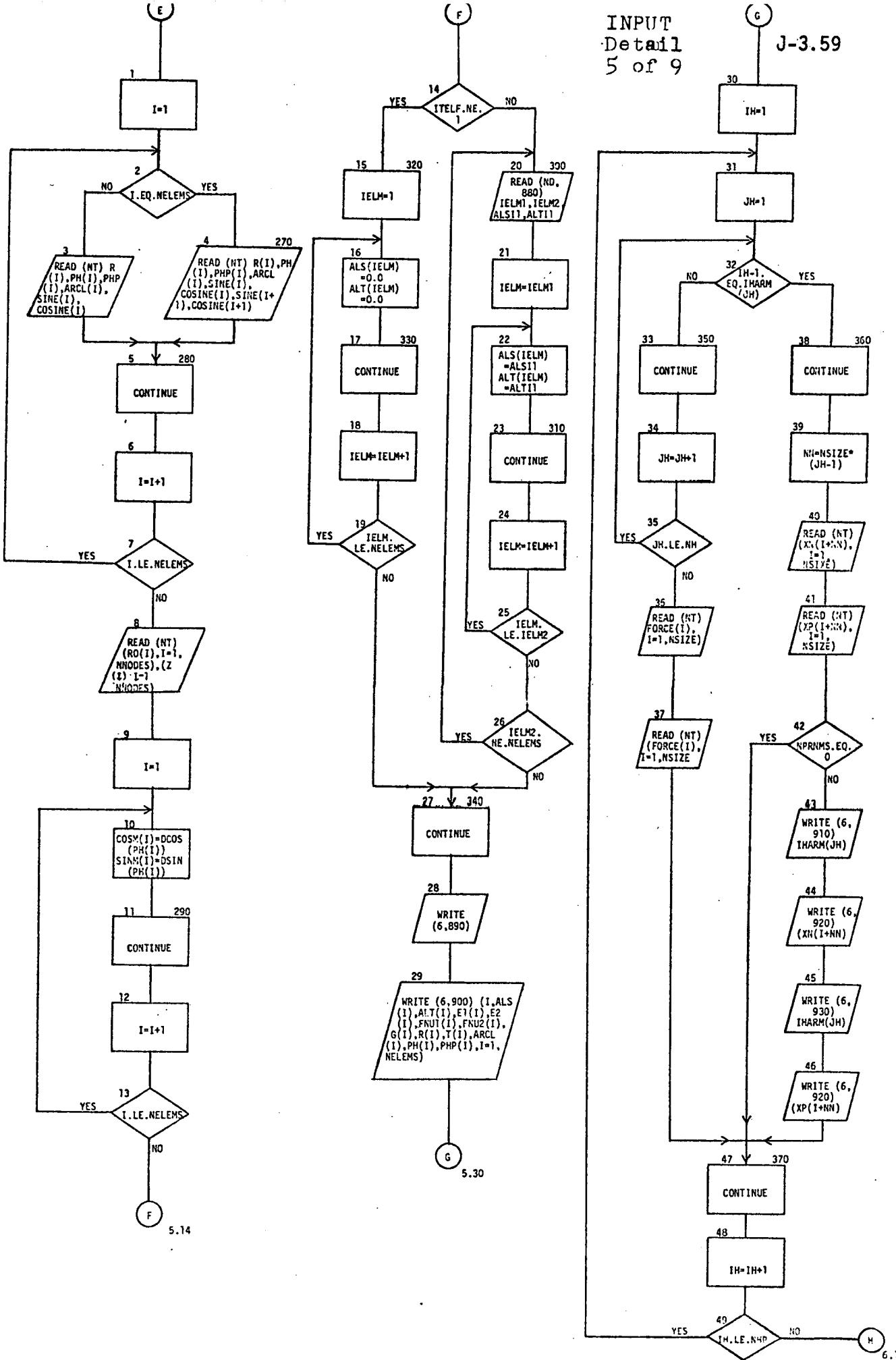
INPUT
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4.27

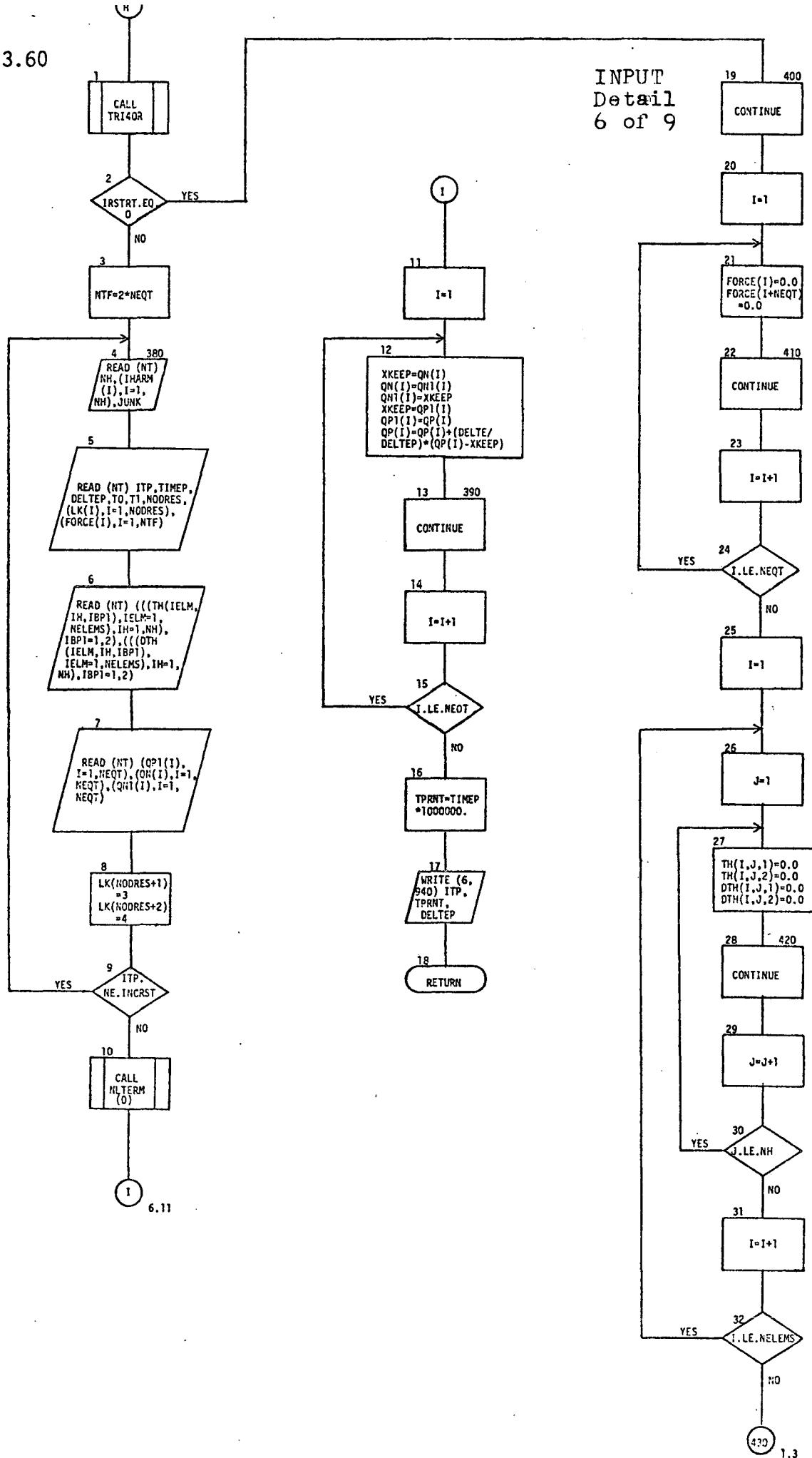
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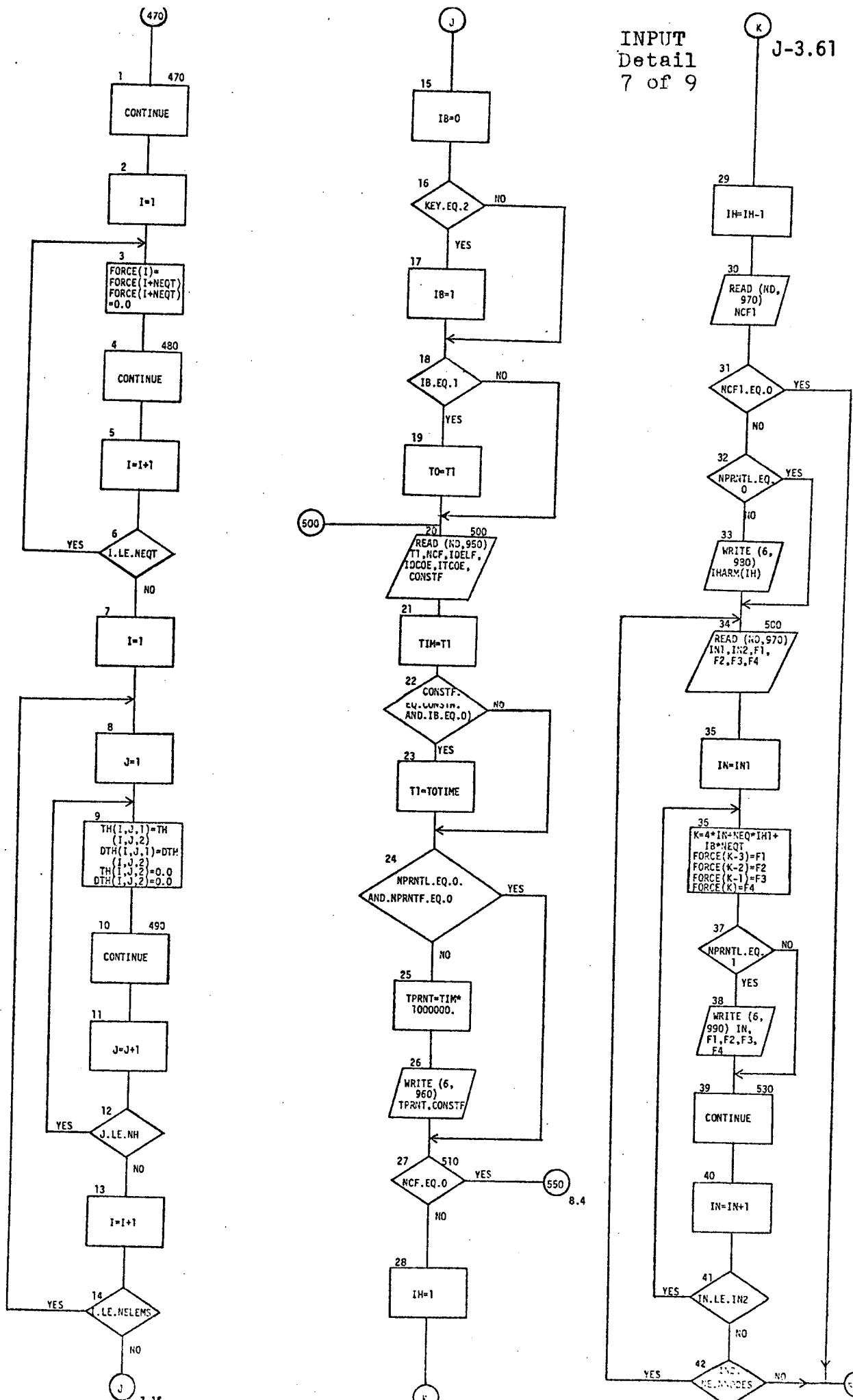
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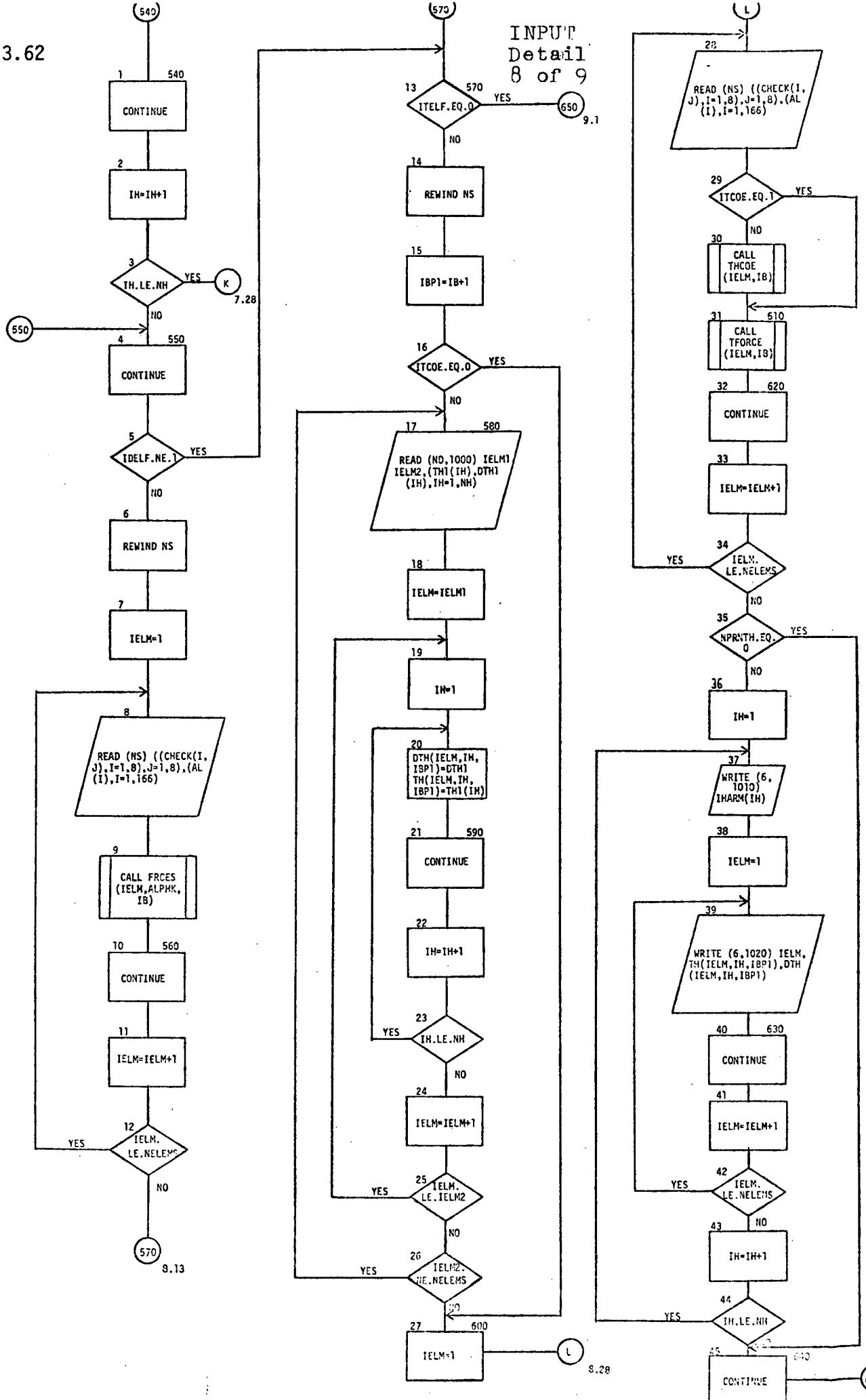


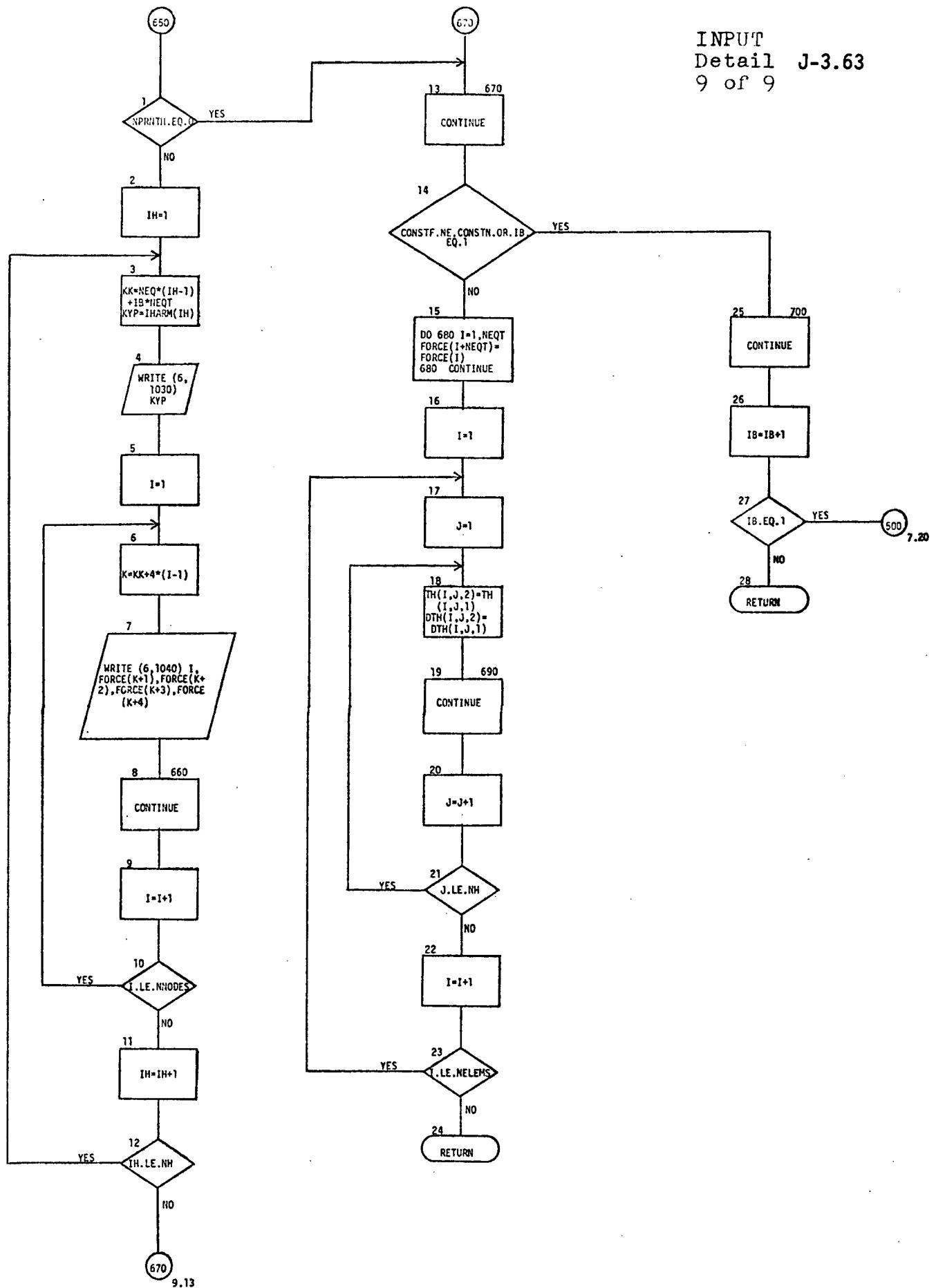
J-3.60



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C      DYNASOR II ***** VERSION 6 ***** DOUBLE PRECISION *****
C      CE(MAIN)          DYN00010
C      DESCRIPTION - TO CONTROL PROGRAM FLOW. IT PERFORMS THE
C      INPUT/OUTPUT FUNCTIONS FOR CASE DATA. PROCESSING          DYN00012
C      IS CONTROLLED BY INCREMENTING THE INDEPENDENT           DYN00014
C      VARIABLE, TIME, WHOSE INDIVIDUAL VALUES ARE USED          DYN00016
C      TO SUPPLY THE SHELL DISPLACEMENTS THROUGH INTEGRATION    DYN00018
C      OF THE EQUATIONS OF MOTION. THE NONLINEAR LOADS          DYN00020
C      AND STRESS RESULTANTS FOR THE SHELL ARE ALSO CALCULATED. DYN00022
C
C      INPUT ARGUMENTS.                                         DYN00024
C      LARGE = CONSTANT WHICH CONTROLS TERMINATION OF THE PROBLEM DYN00026
C                  IF DISPLACEMENTS BECOME EXCESSIVE.             DYN00028
C      NEQT = TOTAL NUMBER OF EQUILIBRIUM EQUATIONS FOR ALL HARMONICS. DYN00030
C
C      EXTERNALS.                                              DYN00032
C      CALLS
C          INPUT
C          NLTERM
C          SETUP
C
C      IMPLICIT REAL*8 (A-H,O-Z)
C      COMMON /QS/ QN(1020),QN1(1020),FORCE(2040),QP(1020),QP1(1020),
C      1          QN2(1020)                                     DYN00034
C      COMMON /CONST/ NH,NELEMS,NNODES,NSIZE,NPRNTQ,NEQ,NEQT,N,NN,NHNS,
C      1          DT2,NPRNTL,NPRNTF,IDEF,IODE                         DYN00036
C      COMMON /TMFT/ TOTIME,DELTE,TIME,T0,T1                     DYN00038
C      COMMON /PRINT/ IPRINT,NOIT,LL                           DYN00040
C      COMMON /HARM/ NHP,IHARM(5)                            DYN00042
C      COMMON /RESTR/ IRSTRT,NPRNT,NPRNIT,ITP,TIMEP,DELTEP   DYN00044
C      COMMON /CYCLE/ ITAM                                DYN00046
C      COMMON /TAPES/ NT,ND,NS                           DYN00048
C      DIMENSION CARD(20)
C      EQUIVALENCE (QN(1),CARD(1))
C      DATA TEST/4HEND /
C
C      C1 (IO) READ AND WRITE THE NUMBER OF DATA CASES AND INPUT DATA FOR ALL
C      CASES
C
C      READ INPUT DATA FOR CARD TYPE I
C      READ (5,110) NCASES,ND,NS
C      WRITE (6,120) NCASES
C      NCASE=0
C      C2 READ AND WRITE INPUT DATA FOR ALL CASES
C      REWIND ND
C      10 NCARD=0
C      NCASE=NCASE+1

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FORTRAN IV G LEVEL 20	MAIN	DATE = 72353	11/03/29	PAGE 0002
0019	MPRINT=0		DYN0290	
0020	20 READ (5,130) CARD		DYN0300	
0021	IF (CARD(1).EQ.TEST.AND.NCARD.EQ.0) GO TO 40		DYN0310	
0022	NCARD=NCARD+1		DYN0320	
0023	IF (CARD(1).NE.TEST) WRITE (ND,130) CARD		DYN0330	
0024	IF (MPRINT.NE.0) GO TO 30		DYN0340	
0025	WRITE (6,140) NCASE		DYN0350	
0026	WRITE (6,150)		DYN0360	
0027	MPRINT=5000		DYN0370	
0028	30 MPRINT=MPRINT-1		DYN0380	
0029	WRITE (6,160) CARD		DYN0390	
0030	IF (CARD(1).NE.TEST) GO TO 20		DYN0400	
0031	IF (NCARD.NE.1) GO TO 10		DYN0410	
0032	40 NCASE=NCASE-1		DYN0420	
0033	IF (NCASE.NE.NCASES) WRITE (6,170)		DYN0430	
0034	REWIND ND		DYN0440	
0035	NCASE=0		DYN0460	
C			DYN0462	
0036	50 CALL INPUT (1)		DYN0470	
0037	NCASE=NCASE+1		DYN0480	
0038	LARGE=0		DYN0490	
C			DYN0492	
C2	IS THIS A PROGRAM RESTART //YES(70)		DYN0494	
0039	IF (IRSTRT.EQ.1) GO TO 70		DYN0500	
C			DYN0508	
0040	DO 60 I=1,NEQT		DYN0510	
0041	QP1(I)=0.0		DYN0520	
0042	60 CONTINUE		DYN0530	
C			DYN0533	
C2	BEGIN TIME INCREMENTS		DYN0535	
0043	ITP=0		DYN0550	
0044	TIMEP=0.0		DYN0560	
0045	T0=0.0		DYN0570	
0046	70 KKP2=ITP+(TOTIME-TIMEP+DELTE*.001)/DELTE		DYN0580	
0047	NOIT=KKP2		DYN0590	
0048	LL=1		DYN0600	
0049	IF (IRSTRT.EQ.1) LL=ITP+1		DYN0610	
C1DO	PROCESS ALL TIME CYCLES		DYN0612	
C			DYN0618	
0050	DO 90 ITAM=LL,KKP2		DYN0620	
0051	TIME=TIMEP+(ITAM-ITP)*DELTE		DYN0630	
C1IF	TIME ,GT. T1(I)/NO(80)		DYN0632	
0052	IF (TIME.LE.T1) GO TO 80		DYN0640	
0053	IF (ITAM.EQ.KKP2) GO TO 80		DYN0650	
0054	TO=T1		DYN0660	
C1	CALCULATE GENERALIZED FORCES FOR TIME T1(I+1)		DYN0662	
0055	CALL INPUT (2)		DYN0670	
0056	80 CONTINUE		DYN0680	

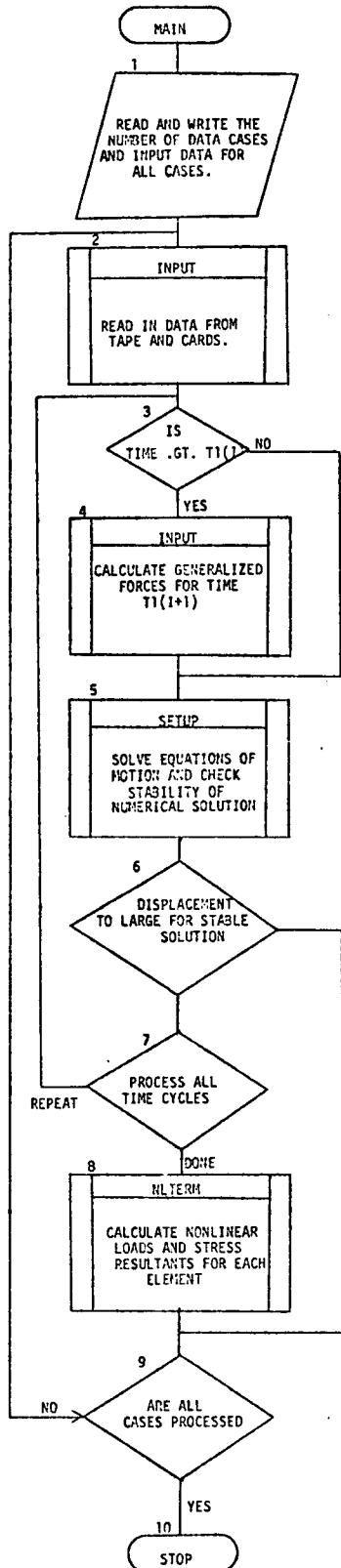
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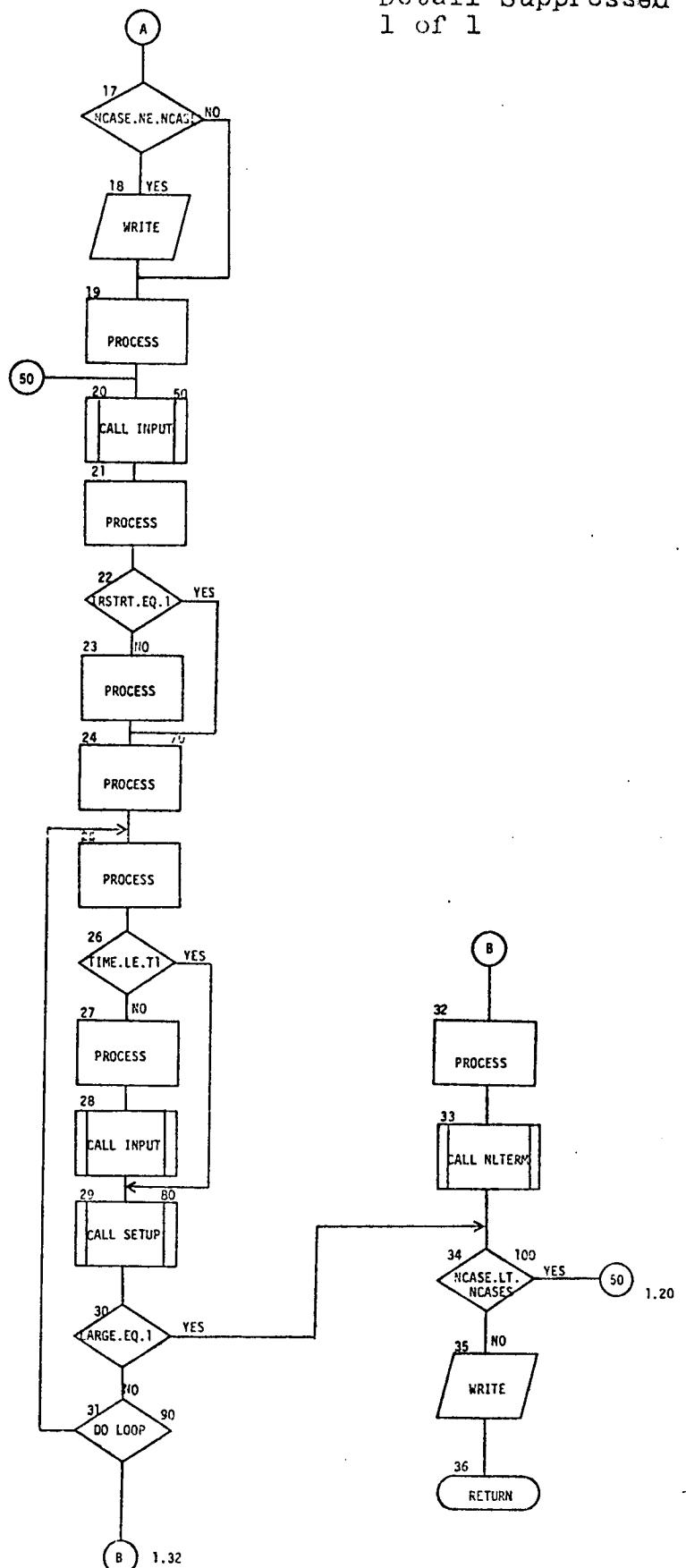
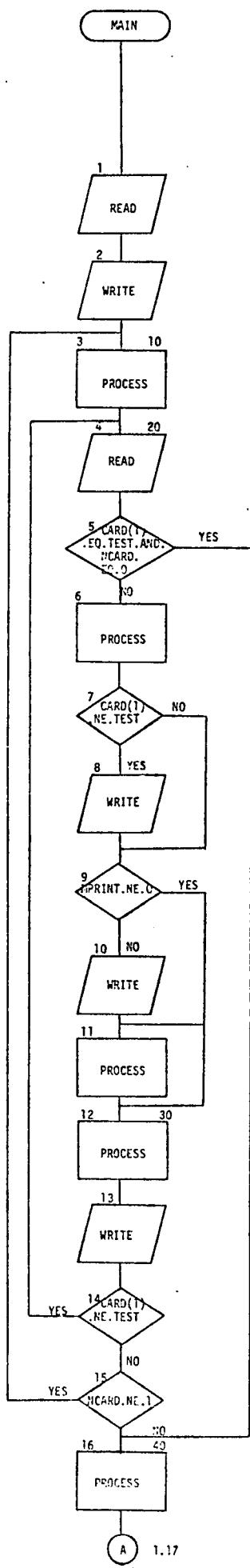
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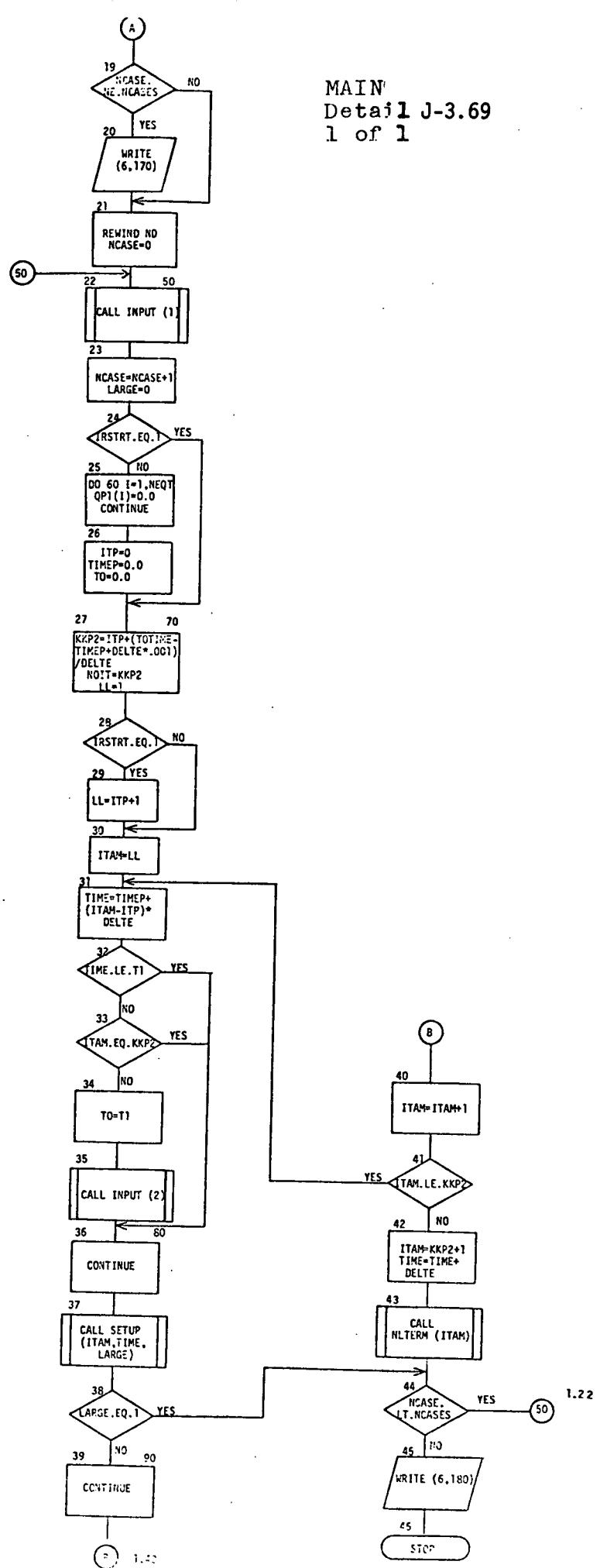
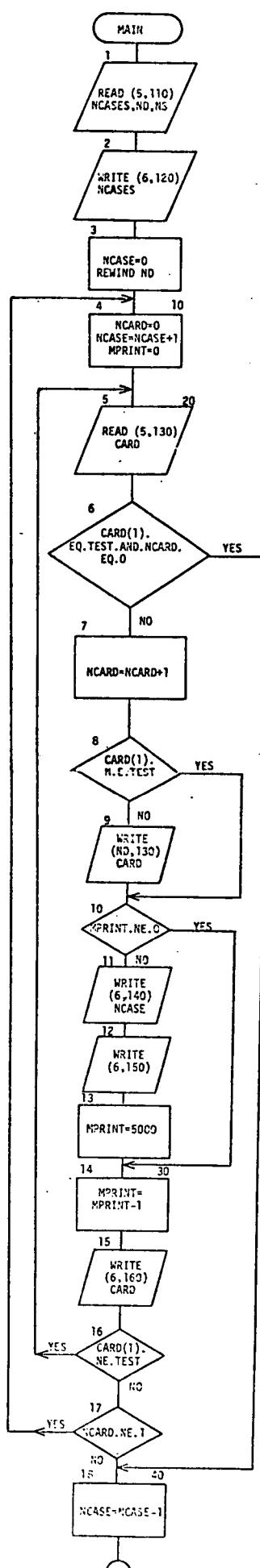
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0057      C1      SOLVE EQUATIONS OF MOTION AND CHECK STABILITY OF NUMERICAL
C1C      SOLUTION.
0058      C1      CALL SETUP (ITAM,TIME,LARGE)
0059      C1      DISPLACEMENT TOO LARGE FOR STABLE SOLUTION//YES(100)
                  IF (LARGE.EQ.1) GO TO 100
JC59      90 CONTINUE
0060      C
0061      ITAM=KKP2+1
0062      TIME=TIME+DELTE
0063      C1      CALCULATE NONLINEAR LOADS AND STRESS RESULTANTS FOR EACH ELEMENT
0064      CALL NLTERM (ITAM)
0065      C1      ARE ALL CASES PROCESSED//NO(50)
0066      100 IF (NCASE.LT.NCASES) GO TO 50
0067      WRITE (6,180)
0068      STOP
0069      C
0070      110 FORMAT (3I5)
0071      120 FORMAT (1H1,//,30X,31HTHE NUMBER OF CASES TO BE RUN =,I5)
0072      130 FORMAT (20A4)
0073      140 FORMAT (//8H1 NCASE=,I1//,28X,22HPRINTOUT OF INPUT DATA,/)
0074      150 FORMAT (13X,2H10,8X,2H20,8X,2H30,8X,2H40,8X,2H50,8X,2H60,8X,2H70,
                  1          8X,2H80/
                  1          5X,8(10H1234567890)/)
0075      160 FORMAT (5X,20A4)
0076      170 FORMAT (50H THE NUMBER OF INPUT CASES DOES NOT AGREE WITH THE,
                  1          22H VALUE OF NCASES INPUT)
0077      180 FORMAT (1H1//10X,18HALL DATA PROCESSED//10X,11H . . . STOP)
0078      END

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CE(MATMUT)                               DYN10852
C                                         DYN1C854
C      DESCRIPTION - TO MULTIPLY AN INPUT VECTOR BY THE STIFFNESS MATRIX DYN10856
C                                         DYN10858
C      INPUT ARGUMENTS.                  DYN10860
C      FORCE = MATRIX OF GENERALIZED FORCES DUE TO EXTERNAL LOADS AND DYN10862
C          TEMPERATURES.                DYN10864
C      IH     = HARMONIC KEY.           DYN10866
C      IID    = VECTOR RANK IN MATMUT. DYN10868
C      STIFM = STIFFNESS MATRIX.       DYN10870
C                                         DYN10872
C      EXTERNALS.                     DYN10874
C      CALLED BY                      DYN10876
C          HOUHQ1                      DYN10878
C          HOUHQN                      DYN10880
C                                         DYN10882
0001      SUBROUTINE MATMUT (IH,FORCE,STIFM,A,IID) DYN10884
0002      IMPLICIT REAL*8 (A-H,O-Z)          DYN1C886
0003      DIMENSION A(204), STIFM(6550), FORCE(1020) DYN10888
C1      MULTIPLY INPUT VECTOR BY MATRIX DYN10890
C                                         DYN10938
0004      DO 10 I=1,IID                 DYN10940
0005          A(I)=0.0                  DYN10950
0006      10 CONTINUE                   DYN10952
C                                         DYN1C955
0007          NN=IID/4                  DYN10960
0008          NT=26*(NN-1)+10            DYN10970
0009          NK=NT*(IH-1)              DYN10980
0010          NF=IID*(IH-1)             DYN10990
0011          NA=NK                     DYN11000
C                                         DYN11008
0012          DO 20 J=1,4                DYN11010
C                                         DYN11018
0013          DO 20 I=1,J                DYN11020
0014              NA=NA+1                DYN11030
0015              A(I)=A(I)+STIFM(NA)*FORCE(NF+J) DYN11040
0016          20 CONTINUE                  DYN11042
C                                         DYN11045
0017          A(2)=A(2)+STIFM(NK+2)*FORCE(NF+1) DYN11050
0018          A(3)=A(3)+STIFM(NK+4)*FORCE(NF+1)+STIFM(NK+5)*FORCE(NF+2) DYN11060
0019          A(4)=A(4)+STIFM(NK+7)*FORCE(NF+1)+STIFM(NK+8)*FORCE(NF+2)+ DYN11070
1              STIFM(NK+9)*FORCE(NF+3)          DYN11080
0020          NKK=NK+10                  DYN11090
0021          NM1=NN-1                  DYN11100
C                                         DYN11108
0022          DO 40 I=1,NM1               DYN11110
0023              NI=4*(I-1)              DYN11120
0024              NFF=NF+NI              DYN11130

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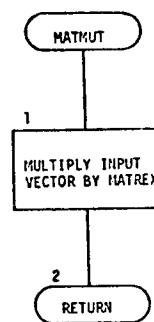
MATMUT

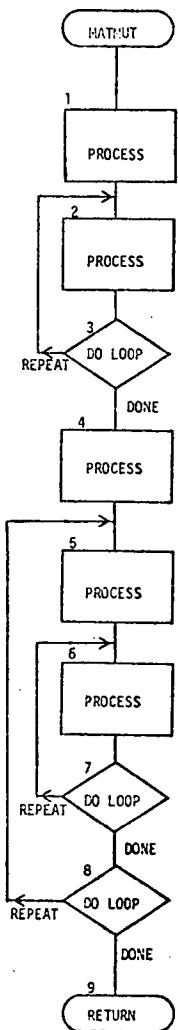
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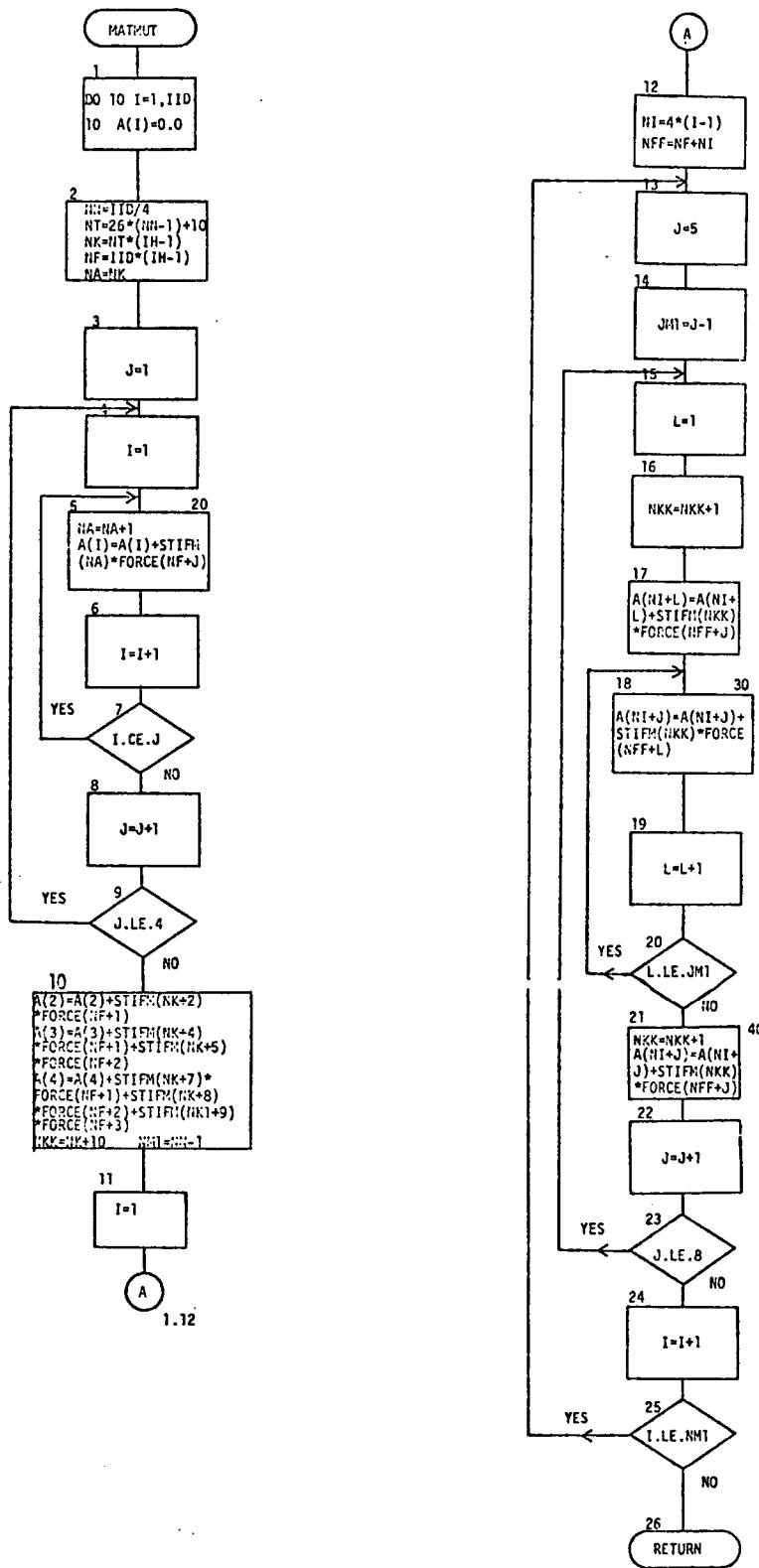
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	C		DYN11138
0025		DO 40 J=5,8	DYN11140
0026		JM1=J-1	DYN11150
	C		DYN11158
0027		DO 30 L=1,JM1	DYN11160
0028		NKK=NKK+1	DYN11170
0029		A(NI+L)=A(NI+L)+STIFM(NKK)*FORCE(NFF+J)	DYN11180
0030		A(NI+J)=A(NI+J)+STIFM(NKK)*FORCE(NFF+L)	DYN11190
0031	30	CONTINUE	DYN11192
	C		DYN11195
0032		NKK=NKK+1	DYN11200
0033		A(NI+J)=A(NI+J)+STIFM(NKK)*FORCE(NFF+J)	DYN11210
0034		40 CONTINUE	DYN11212
	C		DYN11215
0035		RETURN	DYN11220
0036		END	DYN11230







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CE(NLTERM)                               DYN06532
C                                         DYN06534
C   DESCRIPTION - TO PROCESS ALL ELEMENTS TO OBTAIN THE      DYN06536
C   GENERALIZED NONLINEAR LOADS. IF STRESS COMPUTATIONS      DYN06538
C   ARE REQUIRED, THEN THE STRESS RESULTANTS AND STRESSES      DYN06540
C   ON THE UPPER AND LOWER SHELL SURFACES ARE COMPUTED      DYN06542
C   AND PRINTED OUT.                                         DYN06544
C                                         DYN06546
C   INPUT ARGUMENTS.                                         DYN06548
C     E1    = MATRIX CONTAINING THE YOUNG'S MODULUS IN THE MERIDIANAL DYN06550
C             DIRECTION FOR EACH HARMONIC.                      DYN06552
C     E2    = MATRIX CONTAINING THE YOUNG'S MODULUS IN CIRCUMFERENTIAL DYN06554
C             DIRECTION FOR EACH ELEMENT.                     DYN06556
C     FNU1   = MATRIX CONTAINING THE VALUES OF POISSON'S RATIO FOR DYN06558
C             EACH ELEMENT.                                DYN06560
C     FNU2   = MATRIX CONTAINING THE VALUES OF POISSON'S RATION FOR EACH DYN06562
C             ELEMENT.                                DYN06564
C     G      = SHEAR MODULUS, G (FOR AN ISOTROPIC MATERIAL      DYN06566
C             G = (E/2)*(1 + NU)).                         DYN06568
C     QPR    = - PARTIAL DERIVATIVE OF U-NL WITH RESPECT TO LOWER CASE Q DYN06570
C     T      = MATRIX OF ELEMENT THICKNESSES.                  DYN06572
C                                         DYN06574
C   OUTPUT ARGUMENTS.                                         DYN06576
C     QP    = Q - PARTIAL DERIVATIVE OF U-NL WITH RESPECT TO LOWER DYN06578
C             CASE Q AT TIME STEP (N-1).                   DYN06580
C                                         DYN06582
C   EXTERNALS.                                              DYN06584
C     CALLED BY
C       MAIN                                         DYN06586
C       INPUT                                         DYN06588
C       SETUP                                         DYN06590
C     CALLS
C       QPRIME                                         DYN06594
C       STRESS                                         DYN06596
C                                         DYN06598
C                                         DYN06600
0001   SUBROUTINE NLTERM (ITAM)                           DYN06602
0002   IMPLICIT REAL*8 (A-H,O-Z)                         DYN06604
0003   COMMON /CONST/ NH,NELEMS,NNODES,NSIZE,NPRNTQ,NEQ,NEQT,N,NN,NHNS, DYN06606
        1 DT2,NPRNTL,NPRNTF,IDEF,IODE
0004   COMMON /TMFT/ TOTIME,DELTE,TIMF,T0,T1              DYN06608
0005   COMMON /QS/ QN(1020),QN1(1020),FORCE(2040),QP(1020),QP1(1020), DYN06610
        1 QN2(1020)
0006   COMMON /GECM/ FNU1(50),FNU2(50),E1(50),E2(50),G(50),T(50), DYN06612
        1 SINE(51),COSINE(51),SINM(50),COSM(50),R(50),PH(50),
        1 PHP(50),ARCL(50)                                 DYN06614
0007   COMMON /EES/ ES(5),ET(5),EST(5),E13(5),E23(5)      DYN06616
0008   COMMON /NLTRMS/ QPR(8,5)                            DYN06618
0009   COMMON /GCD/ CC1,CC2,DD1,DD2,GG1,GG2                DYN06619
                                         DYN06620
                                         DYN06630
                                         DYN06640

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0010      COMMON /THETAS/ THETA(20),NTHETA,NCLCST,NSTRSS      DYN06650
0011      COMMON /PRINT/ IPRINT,NOIT,LL                      DYN06660
          C
          C      CALCULATION OF NONLINEAR TERMS             DYN06670
          C
          C      THE MIDSURFACE STRAINS AND ROTATIONS AND NONLINEAR TERMS   DYN06700
          C      ARE BASED ON A CONICAL FRUSTUM ELEMENT. THIS IS THE ONLY PLACE A   DYN06710
          C      CONICAL FRUSTUM ELEMENT IS USED.                         DYN06720
          C
          C      DO 10 I=1,NEQT                                     DYN06728
0012      QP(I)=0.0
0013
0014      10 CONTINUE
          C
          C1DO  PROCESS ALL ELEMENTS                         DYN06750
          C
          C      DO 40 II=1,NELEMS                           DYN06753
0015      FN=1.-FNU1(II)*FNU2(II)                         DYN06760
0016      CC1=E1(II)*T(II)/FN                            DYN06770
0017      CC2=E2(II)*T(II)/FN                            DYN06780
0018      GG1=G(II)*T(II)                                DYN06790
0019      GG2=G(II)*T(II)**3/12.                         DYN06800
0020      DD1=E1(II)*T(II)**3/(12.*FN)                  DYN06810
0021      DD2=E2(II)*T(II)**3/(12.*FN)                  DYN06820
0022
          C
          C      FORM QPRIMES                               DYN06830
          C
          C1      CALCULATE GENERALIZED NONLINEAR LOADS        DYN06840
0023      CALL QPRIME (II)                                DYN06850
          C
          C      FORM STRESS RESULTANTS                     DYN06860
          C
0024      IF (NSTRSS.EQ.0) GO TO 20
          C1IF     STRESS COMPUTATION REQUIRED .THEN. CALCULATE AND PRINT STRESS   DYN06862
          C1C     RESULTANTS AND STRESSES ON UPPER AND LOWER FACES           DYN06870
          C
          C      IF (((ITAM-(ITAM/(NSTRSS))*(NSTRSS)).EQ.1
0025      1      .OR.ITAM.EQ.2                          DYN06880
          1      .OR.ITAM.EQ.NOIT+1                      DYN06890
          1      .OR.NSTRSS.EQ.1                         DYN06900
          1      .AND.NCLCST.EQ.1                         DYN06910
          1      CALL STRESS (II,ITAM)
          C
0026      20      CONTINUE                                DYN06912
          C
          C      DO 30 II=1,NH
          C          KA=NEQ*(II-1)+4*(II-1)                  DYN06914
          C
          C      DO 30 JJ=1,4
          C          KK=KA+JJ
          C          QP(KK)=QP(KK)-QPR(JJ,II)                DYN06920
          C
0027
0028
0029
0030
0031
  
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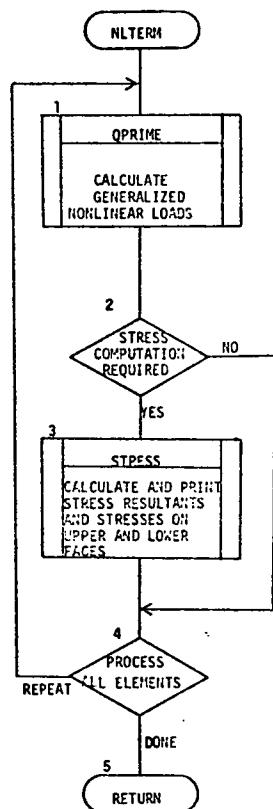
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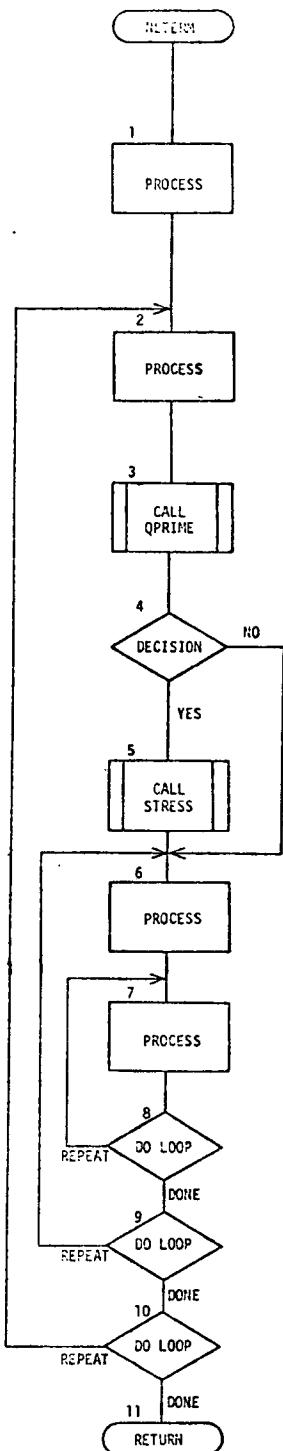
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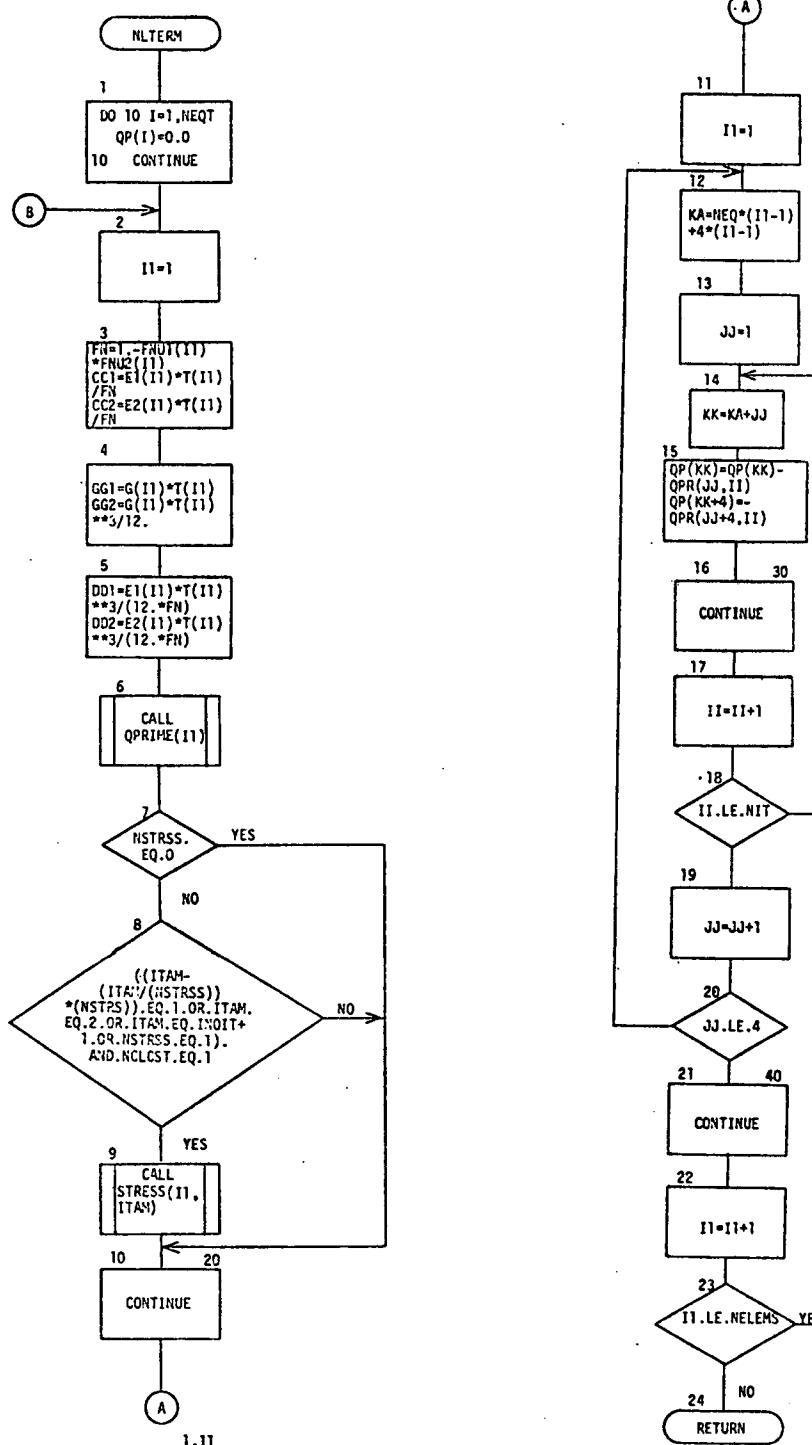
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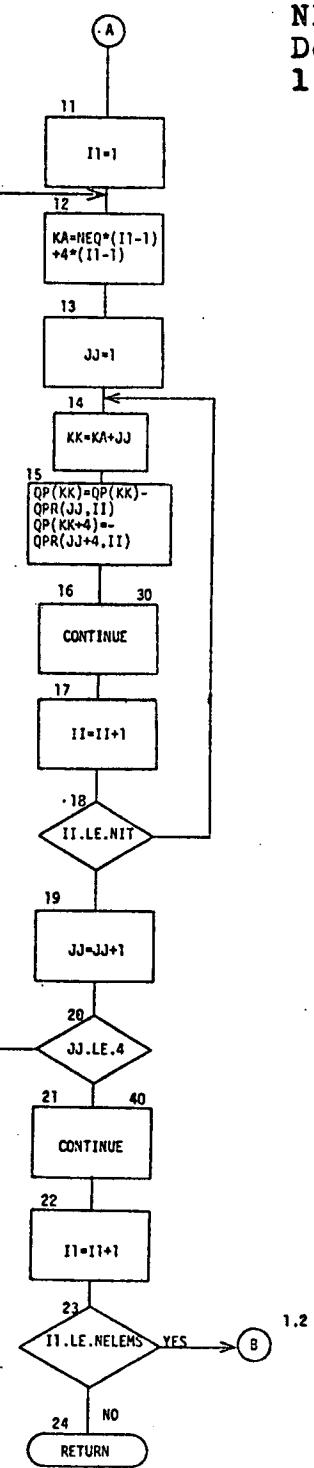
0032	QP(KK+4)=-QPR(JJ+4,II)	DYN07000
0033	30 CONTINUE	DYNG7010
C		DYN07013
0034	40 CONTINUE	DYNC7020
C		DYNC7023
0035	RETURN	DYN07030
0036	END	DYN07040







1.11



1.2

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CE(NRESTR)
C
C      DESCRIPTION - TO APPLY THE DESIRED BOUNDARY CONDITIONS TO
C          THE LEFT SIDE OF THE EQUATIONS OF MOTION. INSERT
C          ONES ON THE DIAGONAL OF THE STIFFNESS MATRIX FOR
C          THE FIRST HARMONIC ONLY.
C
C      INPUT ARGUMENTS.
C      KY    = RESTART KEY.                               DYN10252
C      LK    = MATRIX INDICATING THE NODAL RESTRAINTS WHICH ARE APPLIED DYN10254
C          ON THE SHELL.                                DYN10256
C      NCLOSE = CONSTANT USED TO INDICATE THE PRESENCE OF A SINGULARITY DYN10258
C          AT THE FIRST NODE OF A CLOSED SHELL.          DYN10260
C      NN    = STORAGE BLOCK INDICATOR FLAG FOR STIFFNESS AND MASS DYN10262
C          MATRICES.                                 DYN10264
C      NODRES = NUMBER OF DISPLACEMENT CONSTRAINTS APPLIED TO THE SHELL. DYN10266
C
C      OUTPUT ARGUMENTS.
C      FORCE = MATRIX OF GENERALIZED FORCES DUE TO EXTERNAL LOADS AND DYN10268
C          TEMPERATURES.                                DYN10270
C      STIFM = STIFFNESS MATRIX.                      DYN10272
C
C      EXTERNALS.
C      CALLED BY
C          HOU8Q1                                     DYN10274
C
C001      SUBROUTINE NRESTR (KY)                         DYN10276
C002      IMPLICIT REAL*8 (A-H,O-Z)                   DYN10278
C003      COMMON /SLVEEQ/ STIFM(6550),FORCE(204)       DYN10280
C004      COMMON /CONST/ NH,NELEMS,NNODES,NSIZE,NPRNTQ,NEQ,NEQT,N,NN,NHNS, DYN10282
C005      1      DT2,NPRNTL,NPRNTF,IDEFL,IDCOE        DYN10284
C006      COMMON /RSTRNT/ NODRES,NCLOSE,LK(204)       DYN10286
C007      C1      APPLY BOUNDARY CONDITIONS TO THE LEFT HAND AND RIGHT HAND SIDES DYN10288
C008      C1C     OF THE EQUATIONS OF MOTION            DYN10290
C009      NODRE=NODRES                            DYN10292
C010      IF (KY.EQ.0.AND.NCLOSE.EQ.1) NODRE=NODRE+2 DYN10294
C011      IF (NODRE.EQ.0) GO TO 90                  DYN10296
C012      C
C013      DO 80 L=1,NODRE
C014          NEQ=LK(L)                           DYN10298
C015          IELM=(NEQ-1)/4                     DYN10300
C016          IF (IELM.GT.0) GO TO 30             DYN10302
C017          I=NEQ
C
C          DO 10 J=1,NFQ
C              K=(I*I-I)/2+J+NN
C              STIFM(K)=0.0
C
C10      CONTINUE

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0018	C	J=NEQ	DYN10455	
	C		DYN10460	
0019	DO 20 I=NEQ,8	K=(I*I-I)/2+J+NN	DYN10468	
0020		STIFM(K)=0.0	DYN10470	
0021			DYN10480	
0022	20 CONTINUE		DYN10490	
	C		DYN10492	
0023	K=(NEQ*NEQ-NEQ)/2+NEQ+NN		DYN10495	
0024	STIFM(K)=1.0		DYN10500	
0025	GO TO 70		DYN10510	
0026	30 CONTINUE		DYN10520	
0027	I=NEQ-4*IELM		DYN10530	
0028	N=I+4		DYN10540	
	C		DYN10550	
0029	DO 40 J=1,N	K=10+26*(IELM-1)+4*(I-1)+(I*I-I)/2+J+NN	DYN10558	
0030		STIFM(K)=0.0	DYN10560	
0031			DYN10570	
0032	40 CONTINUE		DYN10580	
	C		DYN10582	
0033	J=NEQ-4*(IELM-1)		DYN10585	
0034	N=NEQ-4*IELM		DYN10590	
	C		DYN10600	
0035	DO 50 I=N,4	K=10+26*(IELM-1)+4*(I-1)+(I*I-I)/2+J+NN	DYN10608	
0036		STIFM(K)=0.0	DYN10610	
0037			DYN10620	
0038	50 CONTINUE		DYN10630	
	C		DYN10632	
0039	K=10+26*(IELM-1)+4*(N-1)+(N*N-N)/2+J+NN		DYN10635	
0040	STIFM(K)=1.0		DYN10640	
0041	IF (IELM.EQ.NELEMS) GO TO 70		DYN10650	
0042	IELM=IELM+1		DYN10660	
0043	J=J-4		DYN10670	
	C		DYN10680	
0044	DO 60 I=1,4	K=10+26*(IELM-1)+4*(I-1)+(I*I-I)/2+J+NN	DYN10688	
0045		STIFM(K)=0.0	DYN10690	
0046			DYN10700	
0047	60 CONTINUE		DYN10710	
	C		DYN10712	
0048	70 FORCE(NEQ)=0.0		DYN10715	
0049	80 CONTINUE		DYN10720	
	C		DYN10730	
0050	90 CONTINUE		DYN10733	
	C1	IF NOT FIRST HARMONIC .THEN. RETURN	DYN10740	
0051		IF (KY.NE.0) RETURN	DYN10742	
	C1	INSERT ONES ON THE DIAGONALS OF THE STIFFNESS MATRIX	DYN10780	
0052		STIFM(3)=1.0	DYN10782	
	C		DYN10790	
			DYN10798	

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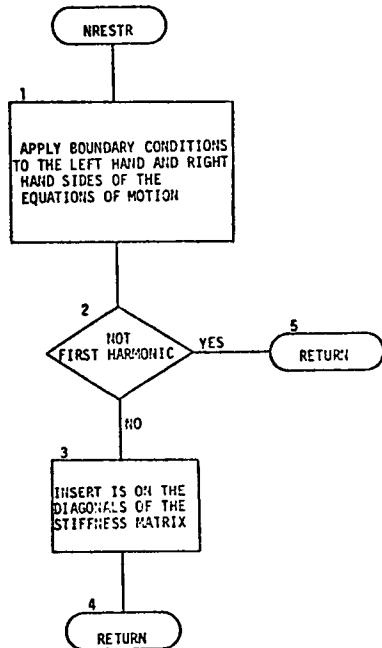
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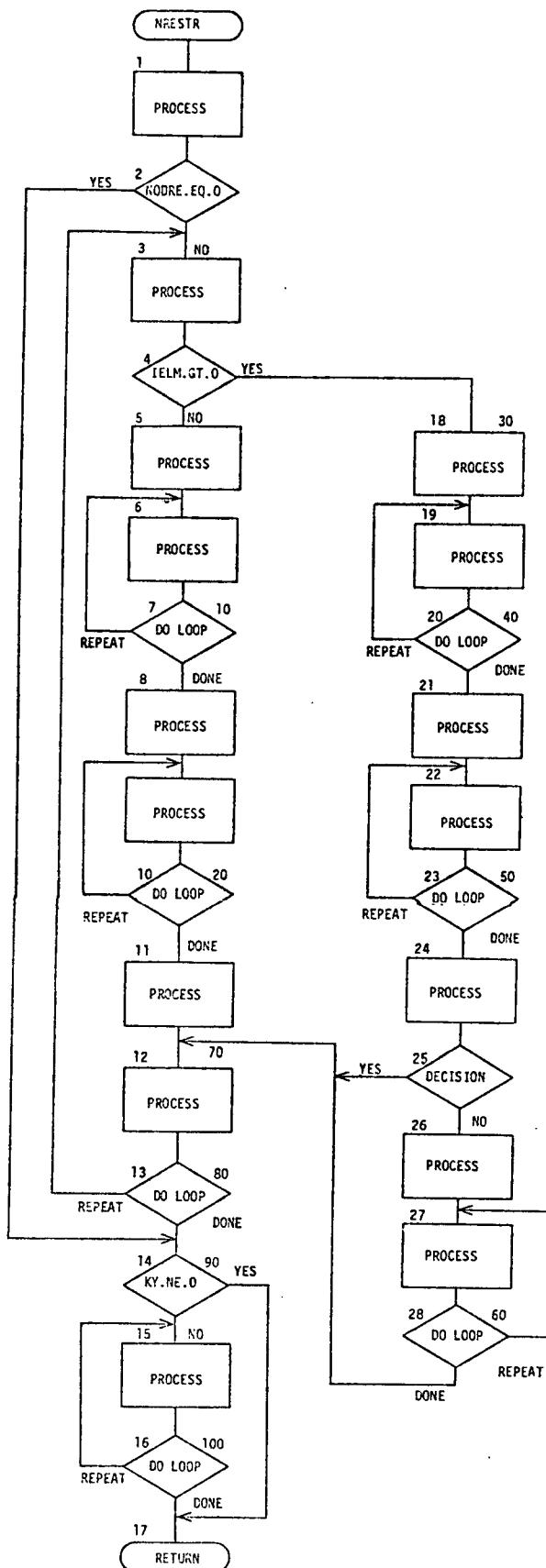
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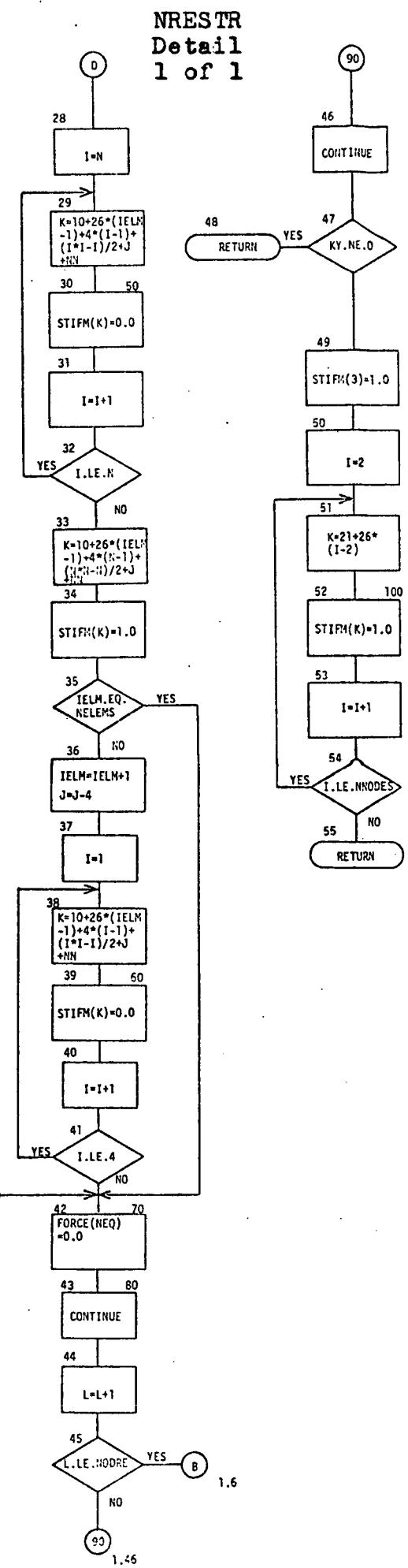
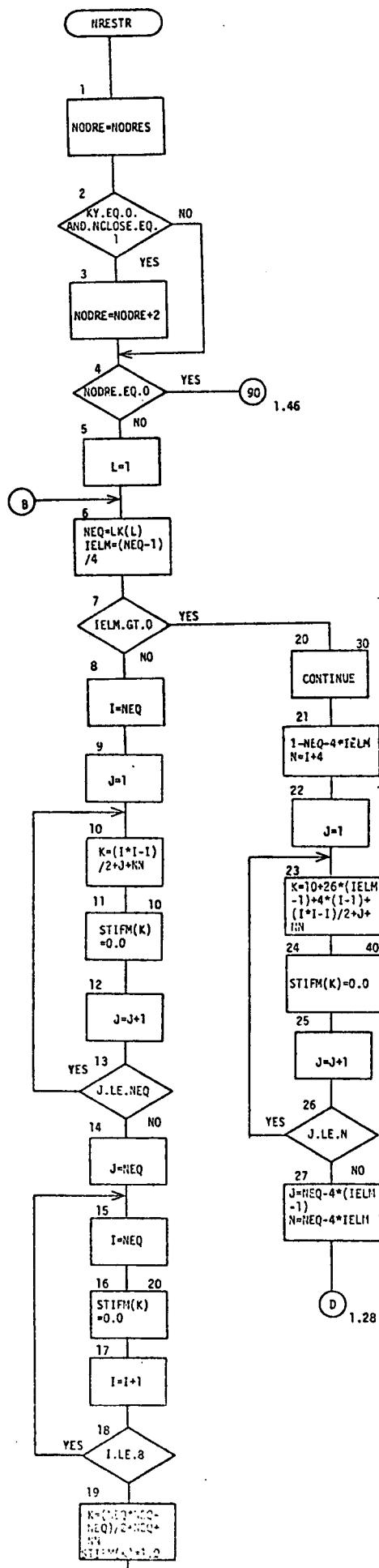
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0053	DO 100 I=2,NNODES	DYN10800
0054	K=21+26*(I-2)	DYN10810
0055	STIFM(K)=1.0	DYN10820
0056	100 CONTINUE	DYN10822
C		DYN10825
0057	RETURN	DYN10830
0058	END	DYN10840







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CE(QPRIME)                               DYN07052
C                                         DYN07054
C   DESCRIPTION - TO COMPUTE THE GENERALIZED NONLINEAR LOADS.      DYN07056
C   FOURIER COEFFICIENTS AND Q-PRIMES ARE COMPUTED. IF             DYN07058
C   NECESSARY, COEFFICIENTS AND Q-PRIMES ARE UPDATED               DYN07060
C   BY INCLUDING THERMAL EFFECTS.                                     DYN07062
C                                         DYN07064
C   INPUT ARGUMENTS.                                                 DYN07066
C   CCC    = MATRIX CONTAINING INTEGRALS FROM 0 TO 2*PI OF          DYN07068
C           COS(I*THETA) * COS(J*THETA) * COS(K*THETA) * DTHETA.     DYN07070
C   CC1    = YOUNG'S MODULUS TIMES SHELL THICKNESS, NORMALIZED WITH DYN07072
C           RESPECT TO POISSON RATIOS (MERIDIANAL DIRECTION).        DYN07074
C   CC2    = YOUNG'S MODULUS TIMES SHELL THICKNESS, NORMALIZED WITH DYN07076
C           RESPECT TO POISSON RATIOS (CIRCUMFERENTIAL DIRECTION).   DYN07078
C   CSS    = MATRIX CONTAINING INTEGRALS FROM 0 TO 2*PI OF          DYN07080
C           COS(I*THETA) * SIN(J*THETA) * SIN(K*THETA) * DTHETA.     DYN07082
C   E13    = MATRIX OF NONLINEAR STRAINS USED IN THE CALCULATION OF DYN07084
C           EACH HARMONIC.                                         DYN07086
C   E23    = MATRIX OF NONLINEAR STRAINS USED IN THE CALCULATION OF DYN07088
C           EACH HARMONIC.                                         DYN07090
C   FNU1   = MATRIX CONTAINING THE VALUES OF POISSON'S RATIO FOR    DYN07092
C           EACH ELEMENT.                                         DYN07094
C   GG1    = SHEAR MODULUS TIMES SHELL THICKNESS (MERIDIANAL        DYN07096
C           DIRECTION).                                         DYN07098
C   IHARM  = MATRIX OF HARMONIC NUMBERS FOR WHICH DISPLACEMENTS     DYN07100
C           AND/OR STRESSES WILL BE CALCULATED.                      DYN07102
C   QN     = DISPLACEMENTS AT TIME INCREMENT (N-1) UP TO STATEMENT 20 DYN07104
C           AFTER STATEMENT 30 THIS MATRIX HAS BEEN CHANGED TO       DYN07106
C           THE DISPLACEMENTS AT TIME STEP (N).                      DYN07108
C   RO     = RADIAL DISTANCE OF ELEMENT FROM ORIGIN.                 DYN07110
C   SSC    = MATRIX CONTAINING INTEGRALS FROM 0 TO 2*PI OF          DYN07112
C           SIN(I*THETA) * SIN(J*THETA) * COS(K*THETA) * DTHETA.     DYN07114
C   Z      = Z-DISTANCE OF ELEMENT FROM ORIGIN.                     DYN07116
C                                         DYN07118
C   OUTPUT ARGUMENTS.                                              DYN07120
C   ES     = MATRIX OF THE LINEAR STRAINS, USED IN THE CALCULATION DYNC7122
C           OF EACH HARMONIC.                                         DYNC7124
C   EST    = MATRIX OF THE LINEAR STRAINS, USED IN THE CALCULATION DYN07126
C           OF EACH HARMONIC.                                         DYN07128
C   ET     = MATRIX OF THE LINEAR STRAINS, USED IN THE CALCULATION DYN07130
C           OF EACH HARMONIC.                                         DYN07132
C   E13    = MATRIX OF NONLINEAR STRAINS USED IN THE CALCULATION OF DYNC7134
C           EACH HARMONIC.                                         DYN07136
C   E23    = MATRIX OF NONLINEAR STRAINS USED IN THE CALCULATION OF DYN07138
C           EACH HARMONIC.                                         DYN07140
C   QPR   = - PARTIAL DERIVATIVE OF U-NL WITH RESPECT TO LOWER CASE QDYN07142
C                                         DYN07144
C   EXTERNALS.                                                       DYN07146

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C      CALLED BY          DYN07148
C      NLTERM             DYN07150
C
0001    SUBROUTINE QPRIME (I1)          DYN07152
0002    IMPLICIT REAL*8 (A-H,O-Z)        DYN07154
0003    COMMON /CONST/ NH,NELEMS,NNODES,NSIZE,NPRNTQ,NEQ,NEQT,N,NN,NHNS,
1           DT2,NPRNTL,NPRNTF,IDEL,F,IDCOE   DYN07156
0004    COMMON /CS/ CCC(125),SSC(125),CSS(125)  DYN07158
0005    COMMON /CS4/ CCCC(625),SSSS(625),SSCC(625),SCCS(625)  DYN07160
0006    COMMON /EES/ ES(5),ET(5),EST(5),E13(5),E23(5)        DYN07162
0007    COMMON /NLTRMS/ QPR(8,5)          DYN07164
0008    COMMON /GEOM/ FNU1(50),FNU2(50),E1(50),E2(50),G(50),T(50),
1           SINE(51),COSINE(51),SINM(50),COSM(50),R(50),PH(50),
1           PHP(50),ARCL(50)            DYN07166
0009    COMMON /GCD/ CC1,CC2,DD1,DD2,GG1,GG2  DYN07168
0010    COMMON /HARM/ NHP,IHARM(5)         DYN07170
0011    COMMON /THER/ TH(50,5,2),DTH(50,5,2),ALS(50),ALT(50)  DYN07172
0012    COMMON /THCON/ ITEL,F,ITCOE,NPRNTH  DYN07174
0013    COMMON /TMFT/ TOTIME,DELTE,TIME,TC,T1  DYN07176
0014    COMMON /QS/ QN(1020),QN1(1020),FORCE(2040),QP(1020),QP1(1020),
1           QN2(1020)            DYN07178
0015    COMMON /RZ/ R0(51),Z(51)          DYN07180
0016    DIMENSION E23Q1(5), E23Q3(5), E23Q5(5), E23Q7(5), ESTQ1(5),
1           ESTQ3(5), ESTQ5(5), ESTQ7(5), ETQ2(5), ETQ6(5)  DYN07182
C      CALCULATE GENERALIZED NONLINEAR LOADS      DYN07190
C      COMPUTE OFTEN USED QUANTITIES            DYN07200
0017    J1=I1          DYN07210
0018    J11=I1+1        DYN07220
0019    DRO=R0(J11)-R0(J1)      DYN07230
0020    DZ=Z(J11)-Z(J1)          DYN07240
0021    ARL=DSQRT(DRO*DRO+DZ*DZ)  DYN07260
0022    SIPH=DRO/ARL          DYN07280
0023    COPH=DZ/ARL          DYN07290
0024    RM=(R0(J1)+R0(J11))/2.0  DYN07310
0025    R2I=1.0/(2.0*RM)        DYN07320
0026    ARCLI=1.0/ARL          DYN07330
C      COMPUTE DERIVATES INDEPENDENT OF I          DYN07340
0027    ETQ3=R2I          DYN07350
0028    ETQ7=R2I          DYN07360
0029    E23Q2=-R2I*COPH      DYN07370
0030    E23Q6=E23Q2          DYN07380
0031    E13Q1=ARCLI*SIPH      DYN07390
0032    E13Q3=-ARCLI*COPH      DYN07400
0033    E13Q5=-ARCLI*SIPH      DYN07410
0034    E13Q7=ARCLI*COPH      DYN07420
0035    ESTQ2=-SIPH*R2I-ARCLI  DYN07430
0036    ESTQ6=-SIPH*R2I+ARCLI  DYN07440
0037    ESQ1=E13Q3          DYN07450

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0038      ESQ3=-E13Q1          DYNC7510
0039      ESQ5=E13Q7          DYN07520
0040      ESQ7=-E13Q5          DYN07530
0041      C1      COMPUTE DERIVATES THAT ARE A FUNCTION OF I   DYNC7532
0042          CO2R=COPH*R2I          DYN07550
0043          SL2R=SIPH*R2I          DYN07560
0044          CL2R=COPH*R2I          DYN07570
0045          SO2R=SIPH*R2I          DYN07580
0046          C      DO 10 IH=1,NH          DYN07588
0047              K=IHARM(IH)          DYNC7590
0048              XK=K          DYNC7600
0049              E23Q1(IH)=SO2R*XK          DYNC7610
0050              E23Q3(IH)=-CO2R*XK          DYNC7620
0051              E23Q5(IH)=SL2R*XK          DYNC7630
0052              E23Q7(IH)=-CL2R*XK          DYNC7640
0053              ESTQ1(IH)=E23Q3(IH)          DYN07650
0054              ESTQ3(IH)=-E23Q1(IH)          DYN07660
0055              ESTQ5(IH)=E23Q7(IH)          DYN07670
0056              ESTQ7(IH)=-E23Q5(IH)          DYN07680
0057              ETQ2(IH)=R2I*XK          DYN07690
0058              ETQ6(IH)=ETQ2(IH)          DYN07700
0059              C      COMPUTE ET, ES, EST, E13, E23          DYN07710
0060          KK=NEQ*(IH-1)+4*(II-1)          DYN07720
0061          KK1=KK+1          DYN07730
0062          KK2=KK+2          DYN07740
0063          KK3=KK+3          DYN07750
0064          KK5=KK+5          DYN07760
0065          KK6=KK+6          DYN07770
0066          KK7=KK+7          DYN07780
0067          ET(IH)=+ETQ2(IH)*QN(KK2)+ETQ3*QN(KK3)+ETQ6(IH)*QN(KK6)+ETQ7*   DYN07790
0068          1      QN(KK7)          DYNC7800
0069          ES(IH)=ESQ1*QN(KK1)+ESQ3*QN(KK3)+ESQ5*QN(KK5)+ESQ7*QN(KK7)          DYN07810
0070          EST(IH)=ESTQ1(IH)*QN(KK1)+ESTQ2*QN(KK2)+ESTQ3(IH)*QN(KK3)+          DYN07820
0071          1      ESTQ5(IH)*QN(KK5)+ESTQ6*QN(KK6)+FSTQ7(IH)*QN(KK7)          DYNC7830
0072          E13(IH)=E13Q1*QN(KK1)+E13Q3*QN(KK3)+E13Q5*QN(KK5)+E13Q7*QN(KK7)          DYN07840
0073          E23(IH)=E23Q1(IH)*QN(KK1)+E23Q2*QN(KK2)+E23Q3(IH)*QN(KK3)+          DYN07850
0074          1      E23Q5(IH)*QN(KK5)+E23Q6*QN(KK6)+E23Q7(IH)*QN(KK7)          DYN07860
0075          10 CONTINUE          DYN07870
0076          C      ITH=0          DYN07880
0077          RSL=RM*ARL/2.0          DYN07890
0078          C1      COMPUTE COEFFICIENTS AND Q-PRIMES          DYN07900
0079          C      DO 40 M=1,NH          DYN07902
0080              CES=0.0          DYN07908
0081              CET=0.0          DYNC7910
0082              CEST=0.0          DYN07920
0083              CES=0.0          DYN07930
0084              CET=0.0          DYN07940

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0077      CE13=0.0          DYN07950
0078      CE23=0.0          DYN07960
0079      K=IHARM(M)        DYN07970
0080      C                 DYN07978
0080      DO 20 I=1,8        DYN07980
0081      QPR(I,M)=0.0      DYN07990
0082      20    CONTINUE     DYN08000
0082      C                 DYN08C03
0082      C                 DYN08008
0083      C                 DYN08010
0084      DO 30 I=1,NH       DYN08020
0084      II=IHARM(I)        DYN08028
0085      C                 DYN08030
0086      JJ=IHARM(J)        DYN08040
0087      IPJ=II+JJ          DYN08050
0088      IMJ=II-JJ          DYN08060
0089      IF (IPJ.NE.K.AND.IABS(IMJ).NE.K) GO TO 30 DYN08070
0090      ITH=ITH+1          DYN08080
0091      C                 DYN08082
0091      COMPUTE COEFFICIENTS
0091      CES=CC1*(CCC(ITH)*E13(I)*E13(J)+FNU1(I1)*SSC(ITH)*E23(I)*DYN08100
0091      E23(J))+CFS        DYN08110
0092      CET=SSC(ITH)*CC2*E23(I)*E23(J)+FNU1(I1)*CC1*CCC(ITH)* DYN08120
0092      E13(I)*E13(J)+CET  DYN08130
0093      CEST=2.0*GG1*CSS(ITH)*E13(J)*E23(I)+CEST          DYN08140
0094      CE13=2.0*CC1*CCC(ITH)*E13(I)*(ES(J)+FNU1(I1)*ET(J))+2.0* DYN08150
0094      GG1*SSC(ITH)*EST(I)*E23(J)+CE13          DYN08152
0095      CE23=2.0*CSS(ITH)*(E23(I)*(CC2*ET(J)+FNU1(I1)*CC1*ES(J))+DYN08170
0095      GG1*E13(J)*EST(I))+CE23          DYN08180
0096      30    CONTINUE     DYN08190
0096      C                 DYN08193
0097      C                 DYN08200
0097      COMPUTE Q PRIMES
0097      QPR(1,M)=(CE13*E13Q1+CES*ESQ1+CEST*ESTQ1(M)+CE23*E23Q1(M))*RSL+DYN08210
0097      1      QPR(1,M)          DYN08220
0098      1      QPR(2,M)=(CE23*E23Q2+CEST*ESTQ2+CET*ETQ2(M))*RSL+QPR(2,M) DYN08230
0099      1      QPR(3,M)=(CE13*E13Q3+CET*ETQ3+CES*ESQ3+CE23*E23Q3(M)+CEST* DYN08240
0099      1      ESTQ3(M))*RSL+QPR(3,M)          DYN08250
0100      1      QPR(5,M)=(CE13*E13Q5+CES*ESQ5+CE23*E23Q5(M)+CEST*ESTQ5(M))*RSL+DYN08260
0100      1      QPR(5,M)          DYN08270
0101      1      QPR(6,M)=(CET*ETQ6(M)+CE23*E23Q6+CEST*ESTQ6)*RSL+QPR(6,M) DYN08280
0102      1      QPR(7,M)=(CE13*E13Q7+CET*ETQ7+CES*ESQ7+CE23*E23Q7(M)+CEST* DYN08290
0102      1      ESTQ7(M))*RSL+QPR(7,M)          DYN08300
0103      40 CONTINUE     DYN08310
0104      C                 DYN08313
0104      IFO=0             DYN08320
0105      C                 DYN08328
0105      DO 60 L=1,NH       DYN08330
0106      CE413=0.0          DYN08340
0107      CE423=0.0          DYN08350
  
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0108      LL=IHARM(L)                               DYN08360
0109      C                                     DYN08368
0110          DO 50 I=1,NH
0111              II=IHARM(I)                         DYN08370
0112          C                                     DYN08380
0113              DO 50 J=1,NH
0114                  JJ=IHARM(J)                         DYN08388
0115                  IPJ=II+JJ                         DYN08390
0116                  IMJ=IABS(II-JJ)                      DYN08400
0117          C                                     DYN08410
0118              KML=IABS(KK-LL)                      DYN08420
0119              IF (IPJ.NE.KPL.AND.IPJ.NE.KML.AND.IMJ.
0120                  NE.KPL.AND.IMJ.NE.KML) GO TO 50      DYN08428
0121          C1                                     DYN08430
0122          COMPUTE COEFFICIENTS AND FOURTH ORDER Q-PRIMES DYN08440
0123          FOR=(FNU1(I1)*CC1+2.0*GG1)*E23(I)*E13(K) DYN08450
0124          CE413=CC1*E13(I)*E13(J)*E13(K)*CCCC(IF0)+FOR*E23(J)*
0125              SSCC(IF0)+CE413                         DYN08520
0126          CE423=CC2*E23(I)*E23(J)*E23(K)*SSSS(IF0)+FOR*E13(J)*
0127              SCCS(IF0)+CE423                         DYN08530
0128          50 CONTINUE                                DYN08540
0129          C                                     DYN08550
0130          QPR(1,L)=QPR(1,L)+RSL*(CE413*E13Q1+CE423*E23Q1(L)) DYN08560
0131          QPR(2,L)=QPR(2,L)+RSL*(CE423*E23Q2)           DYN08563
0132          QPR(3,L)=QPR(3,L)+RSL*(CE413*E13Q3+CE423*E23Q3(L)) DYN08580
0133          QPR(5,L)=QPR(5,L)+RSL*(CE413*E13Q5+CE423*E23Q5(L)) DYN08590
0134          QPR(6,L)=QPR(6,L)+RSL*(CE423*E23Q6)           DYN08600
0135          QPR(7,L)=QPR(7,L)+RSL*(CE413*E13Q7+CE423*E23Q7(L)) DYN08610
0136          60 CONTINUE                                DYN08620
0137          C1                                     DYN08630
0138          THERMAL EFFECTS//NO(90)                   DYN08640
0139          IF (ITELF.EQ.0) GO TO 90                 DYN08643
0140          C1                                     DYN08650
0141          UPDATE COEFFICIENTS AND Q-PRIMES BY INCLUDING THERMAL DFFECTS DYN08652
0142          ITH=0                                    DYN08660
0143          RL=RM*ARL                                DYN08670
0144          C                                     DYN08678
0145          DO 80 M=1,NH                            DYN08680
0146              CE13=0.0                           DYN08690
0147              CE23=0.0                           DYN08700
0148              K=IHARM(M)                         DYN08710
0149          C                                     DYN08718
0150          DO 70 I=1,NH
0151              II=IHARM(I)                         DYN08720
0152          C                                     DYN08730
0153          DO 70 J=1,NH
0154              DO 70 J=1,NH

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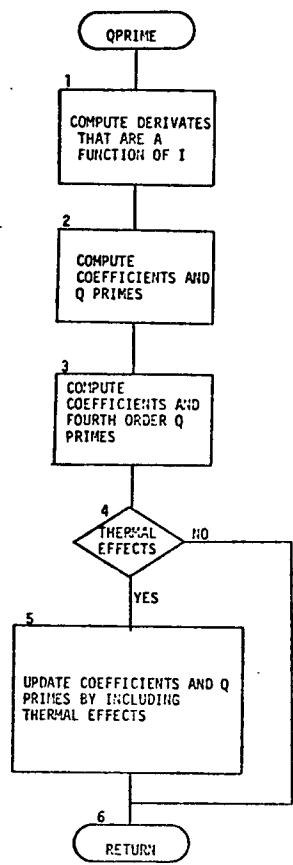
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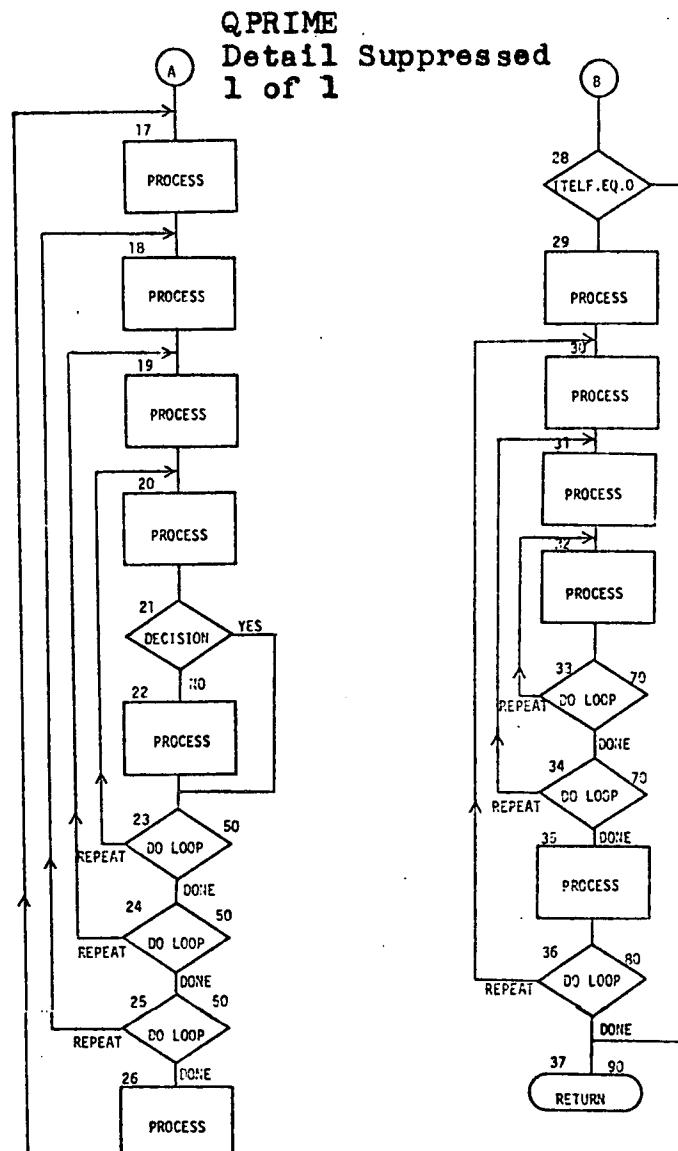
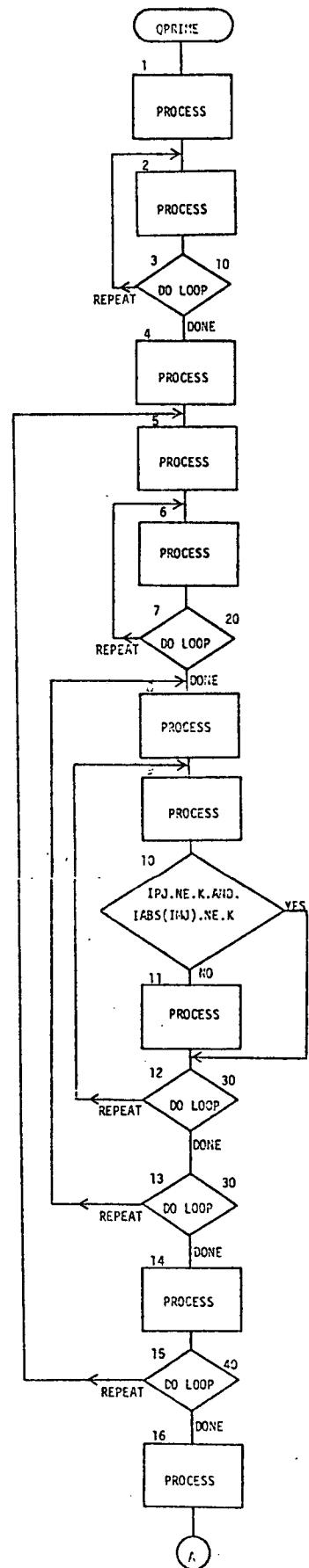
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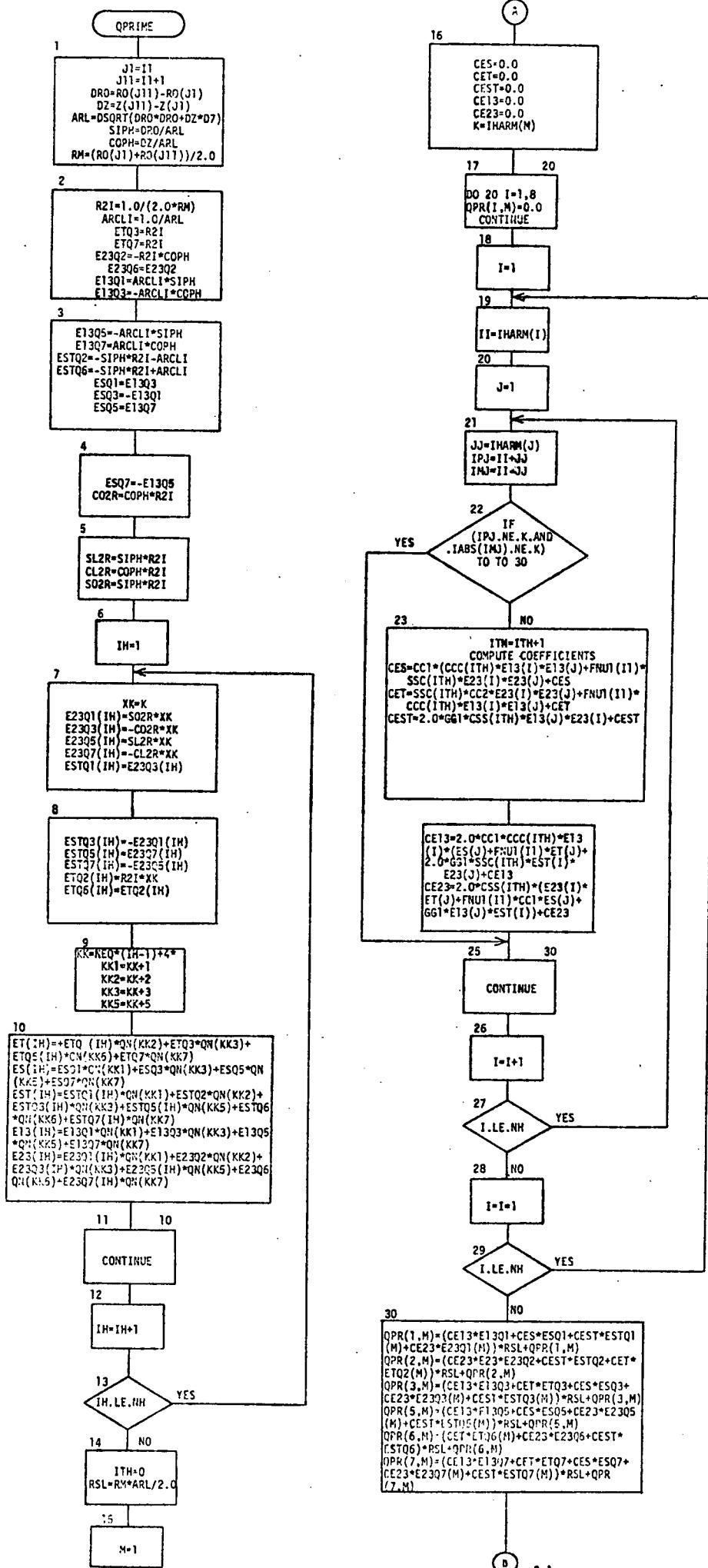
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0142          JJ=IHARM(J)                      DYN08750
0143          IPJ=II+JJ                      DYN08760
0144          IMJ=II-JJ                      DYN08770
0145          IF (IPJ.NE.K.AND.|ABS(IMJ).NE.K) GO TO 70    DYN08780
0146          THT=TH(I1,J,1)+(TH(I1,J,2)-TH(I1,J,1))*(TIME-T0)/(T1-T0) DYN08790
0147          ITH=ITH+1                      DYN08800
0148          C COMPUTE COEFFICIENTS           DYN08810
0149          1 CE13=-CC1*(ALS(I1)+FNU1(I1)*ALT(I1))*THT*CCC(ITH)*E13(I)+DYN08820
0149          1 CE13                         DYN08822
0149          1 CE23=-CC2*(ALT(I1)+FNU2(I1)*ALS(I1))*THT*CSS(ITH)*E23(I)+DYN08830
0149          1 CE23                         DYN08832
0150          70  CONTINUE                   DYN08840
0150          C COMPUTE Q PRIMES            DYN08843
0151          QPR(1,M)=QPR(1,M)+(CE13*E13Q1+CE23*E23Q1(M))*RL   DYN08850
0152          QPR(2,M)=QPR(2,M)+CE23*E23Q2*RL                  DYN08860
0153          QPR(3,M)=QPR(3,M)+(CE13*E13Q3+CE23*E23Q3(M))*RL   DYN08870
0154          QPR(5,M)=QPR(5,M)+(CE13*E13Q5+CE23*E23Q5(M))*RL   DYN08880
0155          QPR(6,M)=QPR(6,M)+CE23*E23Q6*RL                  DYN08890
0156          QPR(7,M)=QPR(7,M)+(CE13*E13Q7+CE23*E23Q7(M))*RL   DYN08900
0157          80 CONTINUE                   DYN08910
0158          C 90 CONTINUE                 DYN08920
0159          RETURN                      DYN08930
0160          END                         DYN08940
                                         DYN08950

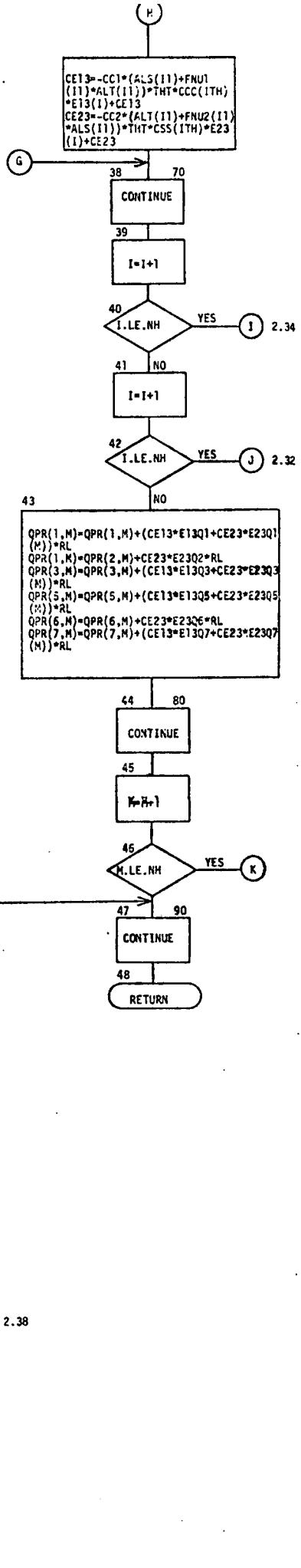
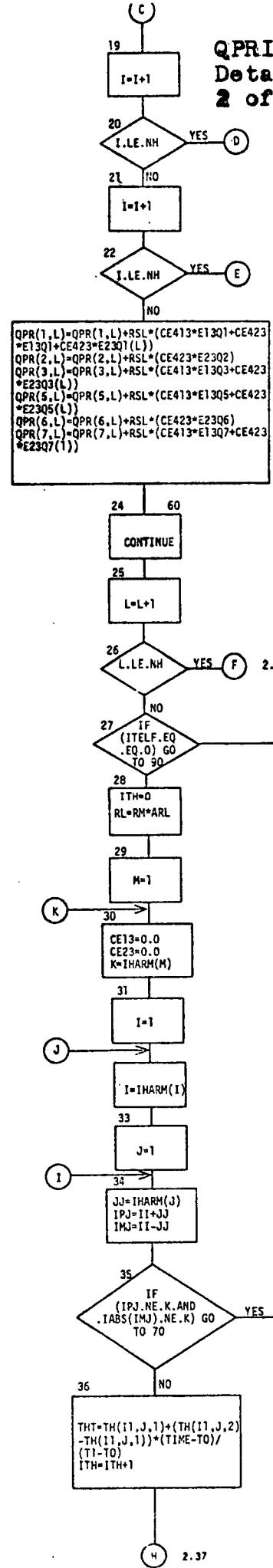
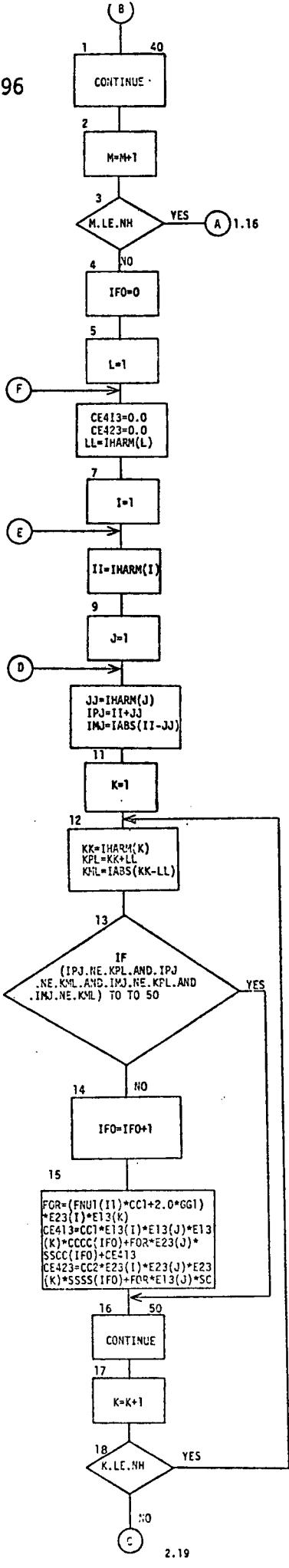
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CE(SETUP)                               DYN05662
C                                         DYN05664
C   DESCRIPTION - TO OBTAIN THE SHELL DISPLACEMENTS BY SOLVING      DYN05666
C       THE EQUATIONS OF MOTION. THESE DISPLACEMENTS ARE           DYN05668
C       CHECKED IN MAGNITUDE FOR BEING TOO LARGE TO ALLOW          DYN05670
C       STABLE SOLUTIONS. THE AXIAL DISPLACEMENT OF THE SECOND     DYN05672
C       NODE IS CHECKED.                                         DYN05674
C                                         DYN05676
C INPUT ARGUMENTS.                      DYN05678
C   NH    = TOTAL NUMBER OF HARMONICS USED IN THE DYNAMIC ANALYSIS. DYN05680
C   QN    = DISPLACEMENTS AT TIME INCREMENT (N-1) UP TO STATEMENT 20 DYN05682
C           AFTER STATEMENT 30 THIS MATRIX HAS BEEN CHANGED TO        DYN05684
C           THE DISPLACEMENTS AT TIME STEP (N).                         DYN05686
C   THETA = MATRIX CONTAINING CIRCUMFERENTIAL ANGLES AT WHICH      DYN05688
C           STRESSES AND/OR DISPLACEMENTS ARE TO BE CALCULATED.       DYN05690
C                                         DYN05692
C OUTPUT ARGUMENTS.                     DYN05694
C   LARGE = CONSTANT WHICH CONTROLS TERMINATION OF THE PROBLEM      DYN05696
C           IF DISPLACEMENTS BECOME EXCESSIVE.                      DYN05698
C   QLOAD = RIGHT-HAND SIDE OF THE DYNAMIC EQUATIONS OF MOTION      DYN05700
C           BEFORE CALLING SOLVEQ.                           DYN05702
C                                         DYN05704
C EXTERNALS.                           DYN05706
C   CALLED BY                         DYN05708
C       MAIN                           DYN05710
C   CALLS                            DYN05712
C       NLTERM                         DYN05714
C       HOUBQN                         DYN05716
C       HOUBQ1                         DYN05718
C       INPUT                          DYN05720
C                                         DYN05722
C
0001      SUBROUTINE SETUP (ITAM,TIME,LARGE)                         DYN05724
0002      IMPLICIT REAL*8 (A-H,O-Z)                                DYN05726
0003      COMMON /SLVEEQ/ XN(6550),QLOAD(204)                      DYN05728
0004      COMMON /QS/ QN(1020),QN1(1020),FORCE(2040),QP(1020),QP1(1020), DYN05730
0005      1      QN2(1020)                                         DYN05732
0005      COMMON /CONST/ NH,NELEMS,NNODES,NSIZE,NPRNTQ,NEQ,NEQT,N,NN,NHNS, DYN05734
0006      1      DT2,NPRNTL,NPRNTF,IDEFL,IDCOE                      DYN05736
0006      COMMON /GCD/ CC1,CC2,DD1,DD2,GG1,GG2                      DYN05738
0007      COMMON /THETAS/ THETA(20),NTHETA,NCLCST,NSTRSS            DYN05740
0008      COMMON /PRINT/ IPRINT,NOIT,LL                           DYN05750
0009      COMMON /HARM/ NHP,IHARM(5)                         DYN05760
0010      COMMON /RESTRT/ IRSTRT,NPRNT,NPRNIT,ITP,TIMEP,DELTEP      DYN05770
0011      C1IF NOT FIRST POINT .THEN. CALCULATE GENERALIZED NONLINEAR LOADS AND DYN05772
0011      C1C      STRESS RESULTANTS                           DYN05774
0011      C1D      IF (ITAM.NE.LL) CALL NLTERM (ITAM)             DYN05820
0011      C1D0     PROCESS HARMONICS                         DYN05822
C                                         DYN05828

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0012	DO 90 IH=1,NH		DYN05830	
0013	KY=IHARM(IH)		DYN05840	
0014	NN=NSIZE*(IH-1)		DYN05850	
0015	N=NEQ*(IH-1)		DYN05860	
C1IF	NOT FIRST POINT .THEN. SET UP EQUATIONS FOR CALCULATING		DYN05862	
C1C	DISPLACEMENTS AT EACH TIME INCREMENT EXCEPT THE FIRST		DYN05864	
0016	IF (ITAM.NE.LL) CALL HOURQN (KY,IH)		DYN05870	
C1IF	FIRST POINT .THEN. SET UP EQUATIONS FOR CALCULATING DISPLACEMENTS		DYN05872	
C1C	AT FIRST TIME INCREMENT AND PREPARE COEFFICIENT		DYN05874	
C1C	MATRICES		DYN05876	
0017	IF (ITAM.EQ.LL) CALL HOURQ1 (KY,IH)		DYN05880	
0018	IT=ITAM-(ITAM/IPRINT)*IPRINT		DYN05890	
0019	IF (ITAM.EQ.NOIT) GO TO 10		DYN05900	
C1	FIRST TIME THRU WITH PRINT REQUIREMENTS//NO(90)		DYN05902	
0020	IF (IT.NE.0.AND.ITAM.NE.1) GO TO 90		DYN05910	
0021	10 IF (NPRNTQ.FQ.0) GO TO 90		DYN05920	
0022	TPRNT=TIME*100000.		DYN05930	
0023	WRITE (6,110) ITAM,TPRNT		DYN05940	
0024	WRITE (6,120) KY		DYN05950	
C			DYN05958	
0025	DO 20 I=1,NNODES		DYN05960	
0026	K=4*(I-1)+N		DYN05970	
0027	WRITE (6,130) I,(QN(K+J),J=1,4)		DYN05980	
0028	20 CONTINUE		DYN05990	
C			DYN05993	
0029	C1 INTERMEDIATE HARMONIC//YES(80)		DYN05995	
0030	IF (IH.NE.NH) GO TO 80		DYN06000	
C1	IF (NH.EQ.1) GO TO 80		DYN06010	
C1C	CALCULATE AND PRINT DISPLACEMENTS AT DESIRED CIRCUMFERENTIAL		DYN06012	
C	ANGLE		DYN06014	
0031	DO 70 IT=1,NTHETA		DYN06048	
C			DYN06050	
0032	DO 30 I=1,NEQ		DYN06060	
0033	QLOAD(I)=0.0		DYN06070	
0034	30 CONTINUE		DYN06072	
C			DYN06075	
C			DYN06078	
0035	DO 50 JH=1,NH		DYN06080	
0036	N=NEQ*(JH-1)		DYN06090	
0037	XIH1=IHARM(JH)		DYN06100	
0038	SN=DSIN(XIH1*THETA(IT))		DYN06110	
0039	CS=DCOS(XIH1*THETA(IT))		DYN06120	
C			DYN06128	
0040	DO 50 II=1,NNODES		DYN06130	
0041	K=4*(II-1)		DYN06140	
0042	NPK=N+K		DYN06150	
C			DYN06158	

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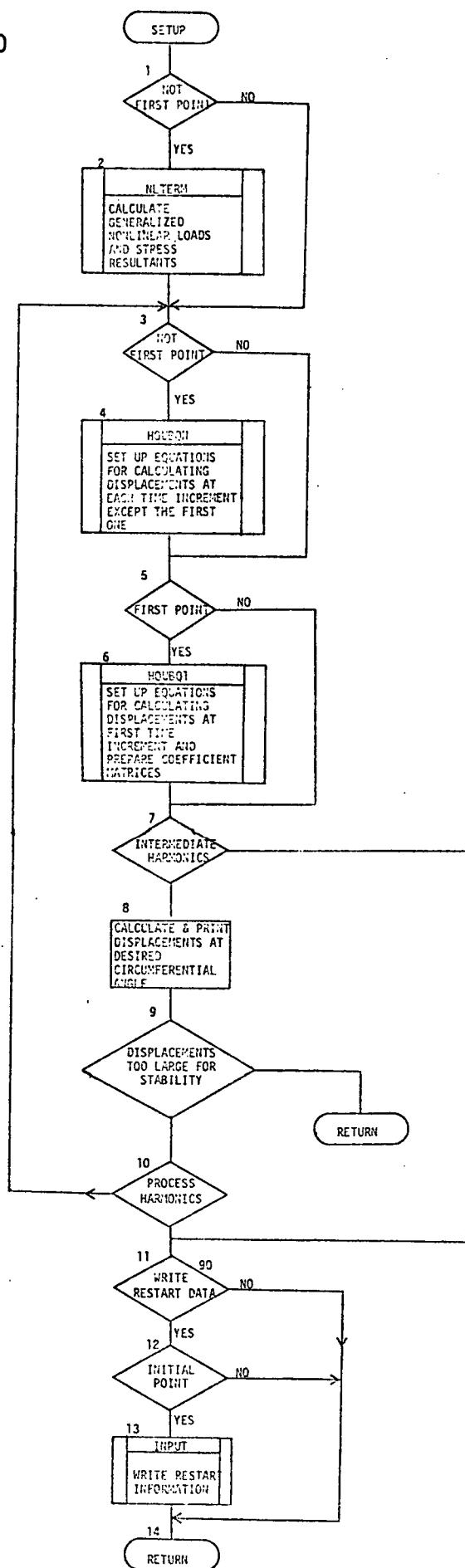
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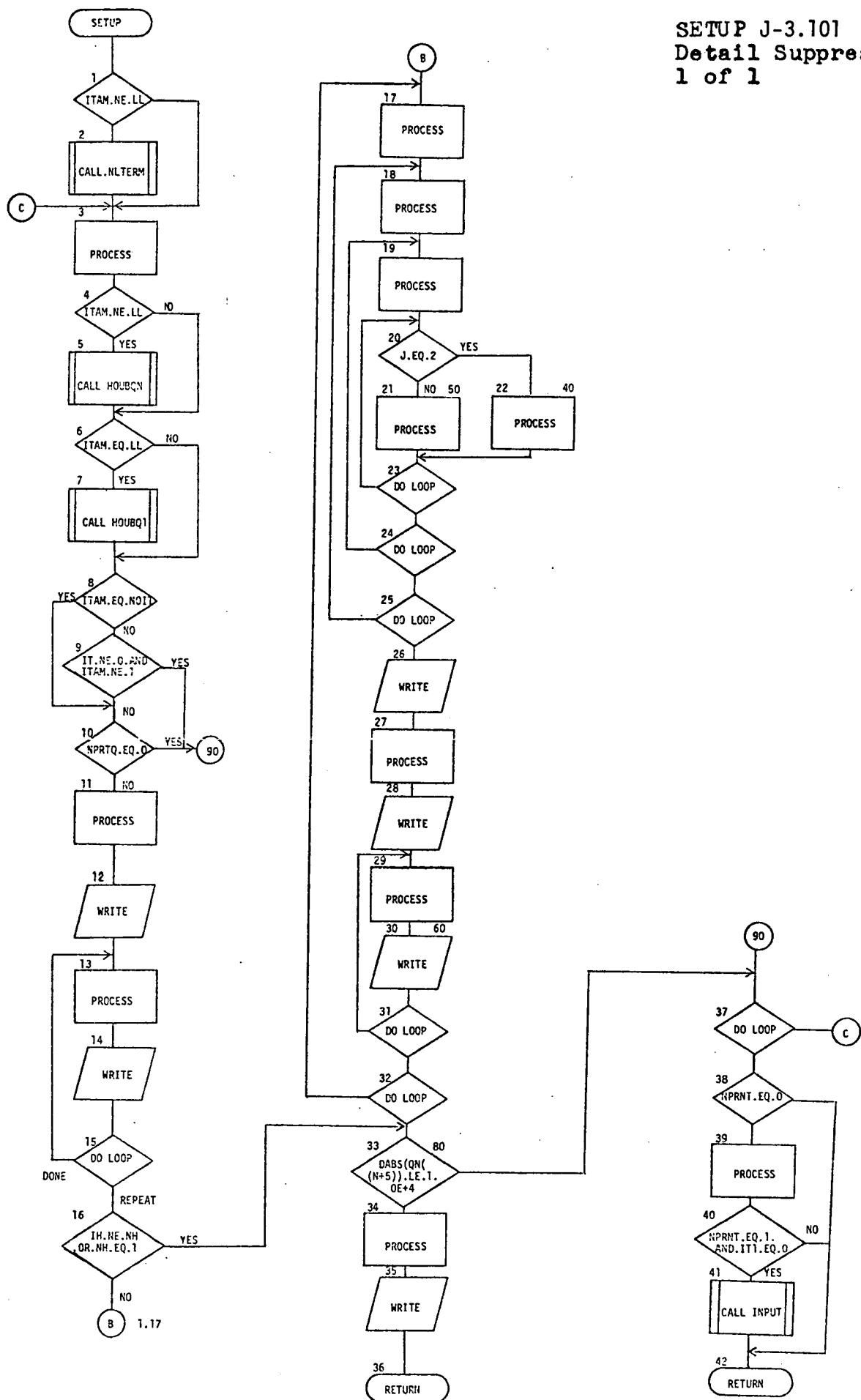
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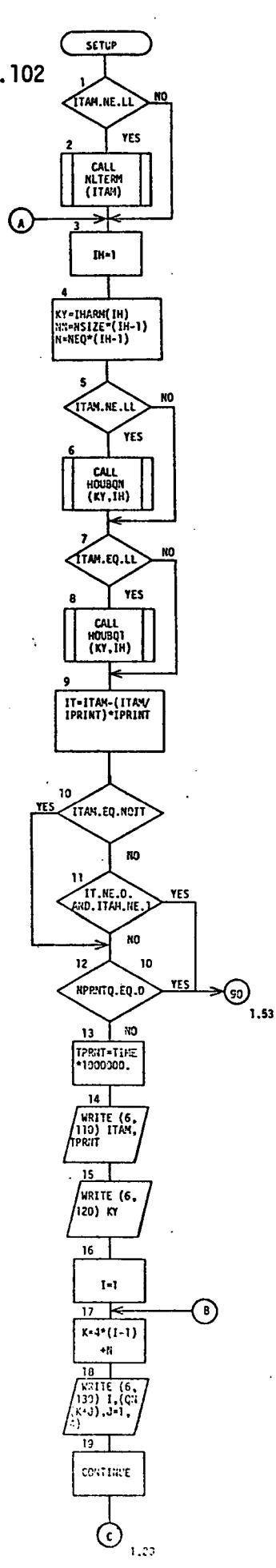
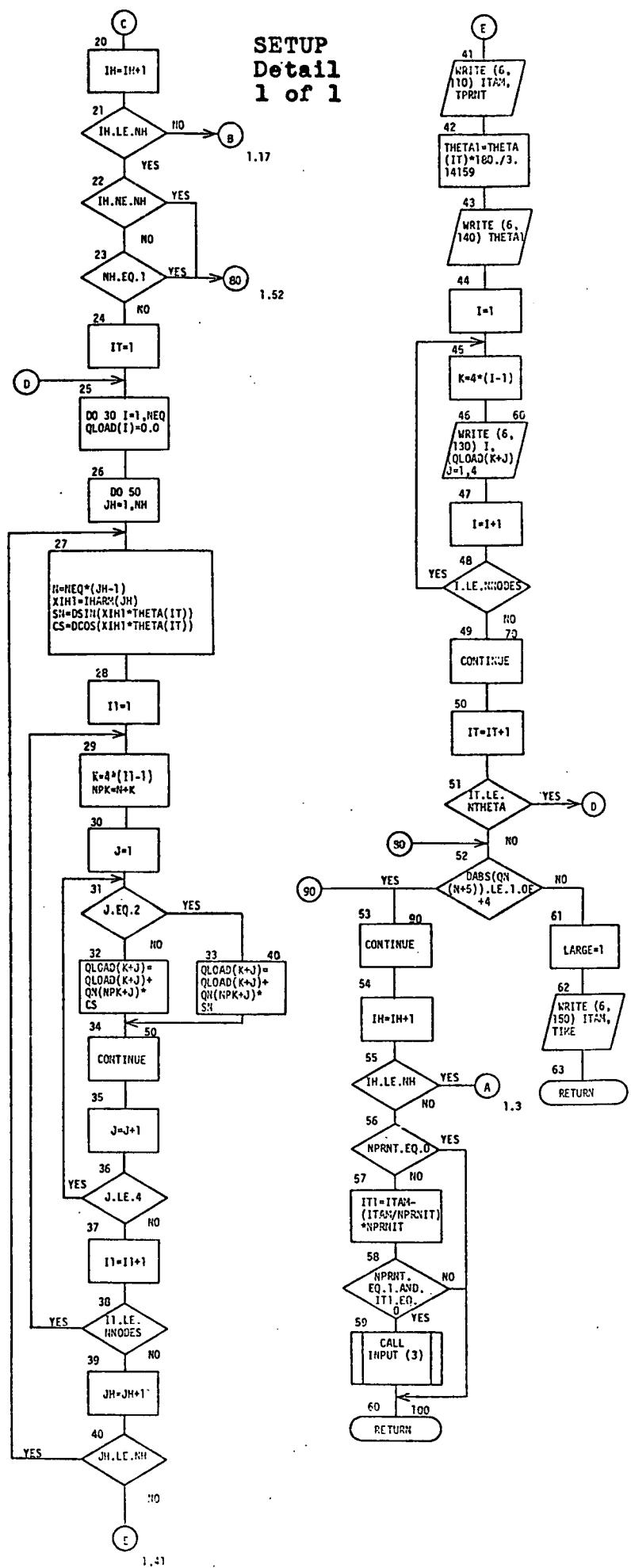
0043      DO 50 J=1,4                               DYN06160
0044      IF (J.EQ.2) GO TO 40                   DYN06170
0045      QLOAD(K+J)=QLOAD(K+J)+QN(NPK+J)*CS   DYN06180
0046      GO TO 50                               DYN06190
0047      40      QLOAD(K+J)=QLOAD(K+J)+QN(NPK+J)*SN DYN06200
0048      50      CONTINUE                         DYN06210
0049      C      WRITE (6,110) ITAM,TPRNT          DYN06213
0050      C      THETA1=THETA(IT)*180./3.14159    DYN06220
0051      C      WRITE (6,140) THETA1            DYN06230
0052      C      DO 60 I=1,NNODES                DYN06240
0053      C      K=4*(I-1)                      DYN06248
0054      C      WRITE (6,130) I,(QLOAD(K+J),J=1,4) DYN06250
0055      60      CONTINUE                         DYN06260
0056      C      70      CONTINUE                         DYN06270
0057      C1     DISPLACEMENTS TOO LARGE FOR STABILITY//NO(90) DYN06272
0058      C1     80      IF (DABS(QN(N+5)).LE.1.0E+4) GO TO 90 DYN06280
0059      C1     LARGE=1                          DYN06283
0060      C1     WRITE (6,150) ITAM,TIME           DYN06285
0061      C1     RETURN                           DYN06290
0062      C1     90      CONTINUE                         DYN06330
0063      C1     WRITE RESTART DATA//NO(100)        DYN06340
0064      C1     IF (NPRNT.EQ.0) GC TO 100          DYN06350
0065      C1     IT1=ITAM-(ITAM/NPRNIT)*NPRNIT      DYN06360
0066      C1     IF (NPRNT.EQ.1.AND.IT1.EQ.0) CALL INPUT (3) DYN06370
0067      C1     100 RETURN                         DYN06373
0068      C1     110 FORMAT (1H1,30X,6HITAM =,I5,5X,6HTIME =,F12.4,13H MICROSECONDS//) DYN06375
0069      C1     120 FORMAT (36X,22HDISPLACEMENTS OF NODES/38X,9HHARMONIC ,I5// DYN06440
0070      C1     1       6X,8HNODE NO.,6X,5HAXIAL,13X,10HTANGENTIAL,11X,6HRADIAL, DYN06450
0071      C1     1       13X,7HANGULAR//)           DYN06452
0072      C1     130 FORMAT (I10,4D2C.8)             DYN06460
0073      C1     140 FORMAT (25X,34HDISPLACEMENTS OF NODES AT THETA = ,F8.3, DYN06470
0074      C1     1       9H DEGREES/38X,13HALL HARMONICS/ DYN06480
0075      C1     1       2X,8HNODE NO.,9X,5HAXIAL,12X,10HTANGENTIAL,12X,6HRADIAL, DYN06490
0076      C1     1       13X,7HANGULAR//)           DYN06492
0077      C1     150 FORMAT (1H1,5X,4HITAM,I5,5X,4HTIME,E12.5// DYN06500
0078      C1     1       6X,22HEXECUTION TERMINATED -, DYN06510
0079      C1     1       33H DISPLACEMENTS GREATER THAN 1.E+4) DYN06512
0080      END                                     DYN06520

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CE(SOLVEQ)
C
C      DESCRIPTION - TO SOLVE THE SET OF SIMULTANEOUS LINEAR
C      EQUATIONS USING A MODIFIED GAUSS ELIMINATION TECHNIQUE
C      WHICH TAKES INTO ACCOUNT DIAGONAL SYMMETRY OF THE
C      SYSTEM. THIS ROUTINE WILL ACCEPT ONLY SPECIAL BANDED
C      MATRICES (I.E., FORMED BY OVERLAPPING SUBMATRICES).
C      ELEMENTS OF THE UPPER BAND ARE STORED IN A 1-DIMENSIONAL
C      ARRAY BY COLUMNS. ALL ZEROS THAT FALL OUTSIDE OF
C      THE SUB-MATRICES ARE SUPPRESSED.
C
C      INPUT ARGUMENTS.
C      IH      = HARMONIC KEY.
C
C      OUTPUT ARGUMENTS.
C      SPR     = ALIAS FOR QLOAD.
C
C      EXTERNALS.
C      CALLED BY
C          HOUHQ1
C          HOUHQN
C
0001      SUBROUTINE SOLVEQ (IH)                               DYN11286
0002      IMPLICIT REAL*8 (A-H,O-Z)                         DYN11288
0003      COMMON /SLVEEQ/ SPA(6550),SPR(204)                 DYN11290
0004      COMMON /CONST/ NH,NELEMS,NNODES,NSIZE,NPRNTQ,NEQ,NEQT,N,NN,NHNS,
1          DT2,NPRNTL,NPRNTF,IDEL,F,DCOE                     DYN11292
0005      COMMON /PRINT/ IPRINT,NOIT,LL                      DYN11294
0006      COMMON /CYCLF/ ITAM                           DYN11300
0007      DIMENSION A(1310), R(204)                         DYN11310
C1      GAUSSIAN ELIMINATION PASS                         DYN11312
C
0008      DO 10 I=1,NSIZE                                     DYN11388
0009          NNPI=NN+I                                      DYN11390
0010          A(I)=SPA(NNPI)                                DYN11400
0011      10 CONTINUE                                         DYN11410
C
0012      DO 20 I=1,NEQ                                      DYN11412
0013          R(I)=SPR(I)                                  DYN11415
0014      20 CONTINUE                                         DYN11418
C
0015      IF (ITAM.GT.(LL+1)) GO TO 100                    DYN11420
0016      KEY=2                                           DYN11430
0017      A(2)=A(2)/A(1)                                 DYN11432
0018      A(3)=A(3)-A(2)*A(2)*A(1)                      DYN11435
0019      A(5)=A(5)-A(4)*A(2)                          DYN11440
0020      A(8)=A(8)-A(7)*A(2)                          DYN11450

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0021      A(4)=A(4)/A(1)          DYN11500
0022      A(5)=A(5)/A(3)          DYN11510
0023      A(6)=A(6)-A(4)*A(4)*A(1)-A(5)*A(5)*A(3)  DYN11520
0024      A(9)=A(9)-A(7)*A(4)-A(8)*A(5)          DYN11530
0025      A(7)=A(7)/A(1)          DYN11540
0026      A(8)=A(8)/A(3)          DYN11550
0027      A(9)=A(9)/A(6)          DYN11560
J028      A(10)=A(10)-A(7)*A(7)*A(1)-A(8)*A(8)*A(3)-A(9)*A(9)*A(6)  DYN11570
0C29      R(2)=R(2)-R(1)*A(2)          DYN11580
0C30      R(3)=R(3)-R(1)*A(4)-R(2)*A(5)          DYN11590
0031      R(4)=R(4)-R(1)*A(7)-R(2)*A(8)-R(3)*A(9)          DYN11600
C
0032      DO 90 K=1,NELEMS          DYN11608
0033          I=11+(K-1)*26          DYN11610
0034          J=5+(K-1)*4          DYN11620
0035          GO TO (40,30), KEY          DYN11630
0036      30      AM10=A(I-10)          DYN11640
0037          AM9=A(I-9)          DYN11650
0038          AM8=A(I-8)          DYN11660
0C39          AM7=A(I-7)          DYN11670
0040          AM6=A(I-6)          DYN11680
0041          AM5=A(I-5)          DYN11690
0042          GO TO 50          DYN11700
0043      40      AM10=A(I-22)          DYN11710
0044          AM9=A(I-17)          DYN11720
0045          AM8=A(I-16)          DYN11730
0046          AM7=A(I-11)          DYN11740
0047          AM6=A(I-10)          DYN11750
0048          AM5=A(I-9)          DYN11760
0049      50      AM4=A(I-4)          DYN11770
0050          AM3=A(I-3)          DYN11780
0051          AM2=A(I-2)          DYN11790
0052          AM1=A(I-1)          DYN11800
0053          A0=A(I)          DYN11810
0054          A1=A(I+1)          DYN11820
0055          A2=A(I+2)          DYN11830
0056          A3=A(I+3)          DYN11840
0057          A4=A(I+4)          DYN11850
0058          A5=A(I+5)          DYN11860
0059          A6=A(I+6)          DYN11870
0060          A7=A(I+7)          DYN11880
0061          A8=A(I+8)          DYN11890
0062          A9=A(I+9)          DYN11900
0063          A10=A(I+10)         DYN11910
0064          A11=A(I+11)         DYN11920
0065          A12=A(I+12)         DYN11930
0066          A13=A(I+13)         DYN11940
0067          A14=A(I+14)         DYN11950

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0068	A15=A(I+15)	DYN11970
0069	A16=A(I+16)	DYN11980
0070	A17=A(I+17)	DYN11990
0071	A18=A(I+18)	DYN12000
0072	A19=A(I+19)	DYN12010
0073	A20=A(I+20)	DYN12020
0074	A21=A(I+21)	DYN12030
0075	A22=A(I+22)	DYN12040
0076	A23=A(I+23)	DYN12050
0077	A24=A(I+24)	DYN12060
0078	A25=A(I+25)	DYN12070
0079	A1=A1-A0*AM9	DYN12080
0080	A6=A6-A5*AM9	DYN12090
0081	A12=A12-A11*AM9	DYN12100
0082	A19=A19-A18*AM9	DYN12110
0083	A2=A2-A0*AM7-A1*AM6	DYN12120
0084	A7=A7-A5*AM7-A6*AM6	DYN12130
0085	A13=A13-A11*AM7-A12*AM6	DYN12140
0086	A20=A20-A18*AM7-A19*AM6	DYN12150
0087	A3=A3-A0*AM4-A1*AM3-A2*AM2	DYN12160
0088	A8=A8-A5*AM4-A6*AM3-A7*AM2	DYN12170
0089	A14=A14-A11*AM4-A12*AM3-A13*AM2	DYN12180
0090	A21=A21-A18*AM4-A19*AM3-A20*AM2	DYN12190
0091	AC=A0/AM10	DYN12200
0092	A1=A1/AM8	DYN12210
0093	A2=A2/AM5	DYN12220
0094	A4=A4-A0*AM10-A1*AM8-A2*AM5-A3*AM1	DYN12230
0095	A9=A9-A5*AO-A6*A1-A7*A2-A8*A3	DYN12240
0096	A15=A15-A11*AO-A12*A1-A13*A2-A14*A3	DYN12250
0097	A22=A22-A18*A0-A19*A1-A20*A2-A21*A3	DYN12260
0098	R(J)=R(J)-R(J-4)*A0-R(J-3)*A1-R(J-2)*A2-R(J-1)*A3	DYN12270
0099	A5=A5/AM10	DYN12280
0100	A6=A6/AM8	DYN12290
0101	A7=A7/AM5	DYN12300
0102	A8=A8/AM1	DYN12310
0103	A9=A9/A4	DYN12320
0104	A10=A10-A5*AM10-A6*AM8-A7*AM5-A8*AM1-A9*A4	DYN12330
0105	A16=A16-A5*A11-A6*A12-A7*A13-A8*A14-A9*A15	DYN12340
0106	A23=A23-A5*A18-A6*A19-A7*A20-A8*A21-A9*A22	DYN12350
0107	R(J+1)=R(J+1)-R(J-4)*A5-R(J-3)*A6-R(J-2)*A7-R(J-1)*A8-R(J)*A9	DYN12360
0108	A11=A11/AM10	DYN12370
0109	A12=A12/AM8	DYN12380
0110	A13=A13/AM5	DYN12390
0111	A14=A14/AM1	DYN12400
0112	A15=A15/A4	DYN12410
0113	A16=A16/A10	DYN12420
0114	A17=A17-A11*AM10-A12*AM8-A13*AM5-A14*A14*AM1-A15*	DYN12430
	A15*A4-A16*A16*A10	DYN12440

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0115		A24=A24-A11*A18-A12*A19-A13*A20-A14*A21-A15*A22-A16*A23	DYN12450		
0116		R(J+2)=R(J+2)-R(J-4)*A11-R(J-3)*A12-R(J-2)*A13-R(J-1)*A14-R(J)*DYN12460			
	1	A15-R(J+1)*A16	DYN12470		
0117		A18=A18/AM10	DYN12480		
0118		A19=A19/AM8	DYN12490		
0119		A20=A20/AM5	DYN12500		
0120		A21=A21/AM1	DYN12510		
0121		A22=A22/A4	DYN12520		
0122		A23=A23/A10	DYN12530		
0123		A24=A24/A17	DYN12540		
0124		A25=A25-A18*A18*AM10-A19*A19*AM8-A20*A20*AM5-A21*A21*AM1-A22*	DYN12550		
	1	A22*A4-A23*A23*A10-A24*A24*A17	DYN12560		
0125		R(J+3)=R(J+3)-R(J-4)*A18-R(J-3)*A19-R(J-2)*A20-R(J-1)*A21-R(J)*DYN12570			
	1	A22-R(J+1)*A23-R(J+2)*A24	DYN12580		
0126		GO TO (70,60), KEY	DYN12590		
0127	60	A(I-10)=AM10	DYN12600		
0128		A(I-9)=AM9	DYN12610		
0129		A(I-8)=AM8	DYN12620		
0130		A(I-7)=AM7	DYN12630		
0131		A(I-6)=AM6	DYN12640		
0132		A(I-5)=AM5	DYN12650		
0133		KEY=1	DYN12660		
0134		GO TO 80	DYN12670		
0135	70	A(I-22)=AM10	DYN12680		
0136		A(I-17)=AM9	DYN12690		
0137		A(I-16)=AM8	DYN12700		
0138		A(I-11)=AM7	DYN12710		
0139		A(I-10)=AM6	DYN12720		
0140		A(I-9)=AM5	DYN12730		
0141	80	A(I-4)=AM4	DYN12740		
0142		A(I-3)=AM3	DYN12750		
0143		A(I-2)=AM2	DYN12760		
0144		A(I-1)=AM1	DYN12770		
0145		A(I)=A0	DYN12780		
0146		A(I+1)=A1	DYN12790		
0147		A(I+2)=A2	DYN12800		
0148		A(I+3)=A3	DYN12810		
0149		A(I+4)=A4	DYN12820		
0150		A(I+5)=A5	DYN12830		
0151		A(I+6)=A6	DYN12840		
0152		A(I+7)=A7	DYN12850		
0153		A(I+8)=A8	DYN12860		
0154		A(I+9)=A9	DYN12870		
0155		A(I+10)=A10	DYN12880		
0156		A(I+11)=A11	DYN12890		
0157		A(I+12)=A12	DYN12900		
0158		A(I+13)=A13	DYN12910		
0159		A(I+14)=A14	DYN12920		

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0160      A(I+15)=A15          DYN12930
0161      A(I+16)=A16          DYN12940
0162      A(I+17)=A17          DYN12950
0163      A(I+18)=A18          DYN12960
0164      A(I+19)=A19          DYN12970
0165      A(I+20)=A20          DYN12980
0166      A(I+21)=A21          DYN12990
0167      A(I+22)=A22          DYN13000
0168      A(I+23)=A23          DYN13010
0169      A(I+24)=A24          DYN13020
0170      A(I+25)=A25          DYN13030
0171      90 CONTINUE          DYN13032
C
0172      GO TO 120            DYN13035
0173      100 CONTINUE          DYN13040
0174      R(2)=R(2)-R(1)*A(2)  DYN13050
0175      R(3)=R(3)-R(1)*A(4)-R(2)*A(5)  DYN13060
0176      R(4)=R(4)-R(1)*A(7)-R(2)*A(8)-R(3)*A(9)  DYN13070
C
0177      DO 110 K=1,NELEMS    DYN13080
0178      N=4*(K+1)-3          DYN13090
0179      L=26*K-15            DYN13100
0180      R(N)=R(N)-R(N-4)*A(L)-R(N-3)*A(L+1)-R(N-2)*A(L+2)-R(N-1)*A(L+3)  DYN13120
0181      R(N+1)=R(N+1)-R(N-4)*A(L+5)-R(N-3)*A(L+6)-R(N-2)*A(L+7)-          DYN13130
1      R(N-1)*A(L+8)-R(N)*A(L+9)          DYN13132
0182      R(N+2)=R(N+2)-R(N-4)*A(L+11)-R(N-3)*A(L+12)-R(N-2)*A(L+13)-          DYN13134
1      R(N-1)*A(L+14)-R(N)*A(L+15)-R(N+1)*A(L+16)          DYN13136
0183      R(N+3)=R(N+3)-R(N-4)*A(L+18)-R(N-3)*A(L+19)-R(N-2)*A(L+20)-          DYN13138
1      R(N-1)*A(L+21)-R(N)*A(L+22)-R(N+1)*A(L+23)-R(N+2)*          DYN13140
1      A(L+24)          DYN13142
0184      110 CONTINUE          DYN13142
C
0185      120 CONTINUE          DYN13190
C1      BACK SUBSTITUTIONS   DYN13193
0186      N=26*NELEMS+10        DYN13200
0187      M=(NELEMS+1)*4        DYN13202
0188      R(M)=R(M)/A(N)        DYN13220
0189      R(M-1)=R(M-1)/A(N-8)-R(M)*A(N-1)          DYN13230
0190      R(M-2)=R(M-2)/A(N-15)-R(M-1)*A(N-9)-R(M)*A(N-2)          DYN13240
0191      R(M-3)=R(M-3)/A(N-21)-R(M-2)*A(N-16)-R(M-1)*A(N-10)-R(M)*A(N-3)  DYN13250
C
0192      DO 150 K=1,NELEMS    DYN13260
0193      L=26*(NELEMS+1-K)-15  DYN13270
0194      N=4*(NELEMS+1-K)-3  DYN13280
0195      IF (L-11) 130,140,130  DYN13290
0196      130      R(N+3)=R(N+3)/A(L-1)-R(N+4)*A(L+3)-R(N+5)*A(L+8)-R(N+6)*  DYN13300
1      A(L+14)-R(N+7)*A(L+21)          DYN13310
0197      R(N+2)=R(N+2)/A(L-9)-R(N+3)*A(L-2)-R(N+4)*A(L+2)-R(N+5)*  DYN13320
1      DYN13330
DYN13340

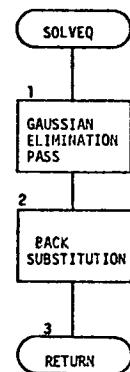
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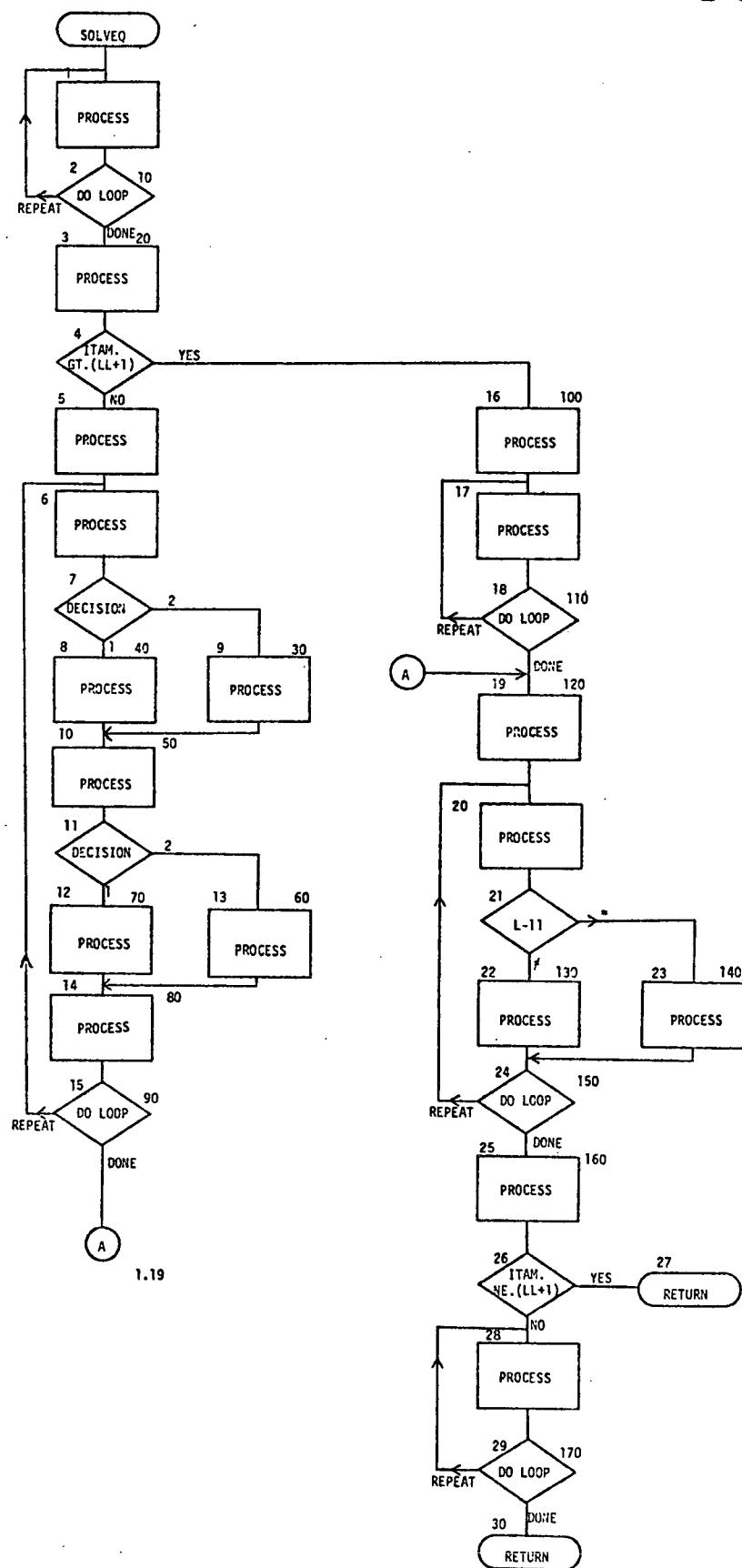
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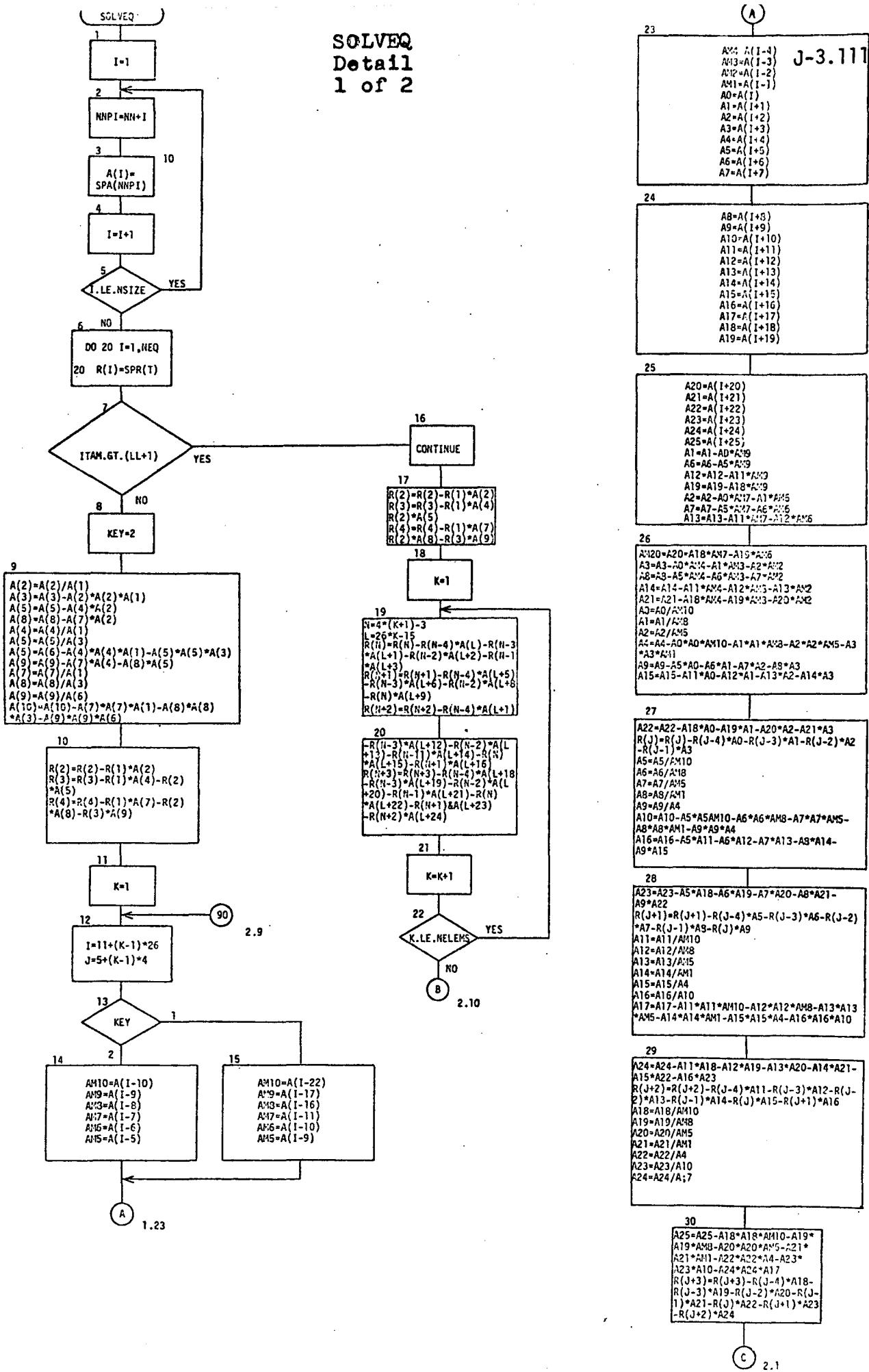
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      1           A(L+7)-R(N+6)*A(L+13)-R(N+7)*A(L+20)          DYN13350
0198     1           R(N+1)=R(N+1)/A(L-16)-R(N+2)*A(L-10)-R(N+3)*A(L-3)-R(N+4)*          DYN13360
      1           A(L+1)-R(N+5)*A(L+6)-R(N+6)*A(L+12)-R(N+7)*A(L+19)          DYN13370
0199     1           R(N)=R(N)/A(L-22)-R(N+1)*A(L-17)-R(N+2)*A(L-11)-R(N+3)*A(L-4)-          DYN13380
      1           R(N+4)*A(L)-R(N+5)*A(L+5)-R(N+6)*A(L+11)-R(N+7)*          DYN13390
      1           A(L+18)          DYN13391
0200     GO TO 150          DYN13400
0201     140           R(N+3)=R(N+3)/A(L-1)-R(N+4)*A(L+3)-R(N+5)*A(L+8)-R(N+6)*          DYN13410
      1           A(L+14)-R(N+7)*A(L+21)          DYN13420
0202     1           R(N+2)=R(N+2)/A(L-5)-R(N+3)*A(L-2)-R(N+4)*A(L+2)-R(N+5)*A(L+7)-          DYN13430
      1           R(N+6)*A(L+13)-R(N+7)*A(L+20)          DYN13440
0203     1           R(N+1)=R(N+1)/A(L-8)-R(N+2)*A(L-6)-R(N+3)*A(L-3)-R(N+4)*A(L+1)-          DYN13450
      1           R(N+5)*A(L+6)-R(N+6)*A(L+12)-R(N+7)*A(L+19)          DYN13460
0204     1           R(N)=R(N)/A(L-10)-R(N+1)*A(L-9)-R(N+2)*A(L-7)-R(N+3)*A(L-4)-          DYN13470
      1           R(N+4)*A(L)-R(N+5)*A(L+5)-R(N+6)*A(L+11)-R(N+7)*          DYN13480
      1           A(L+18)          DYN13481
C205      150 CONTINUE          DYN13490
C
C
0206      DO 160 I=1,NEQ          DYN13500
0207      SPR(I)=R(I)          DYN13510
0208      160 CONTINUE          DYN13512
C
0209      IF (ITAM.NE.(LL+1)) RETURN          DYN13515
C
0210      DO 170 I=1,NSIZE          DYN13520
0211      NNPI=NN+I          DYN13528
0212      SPA(NNPI)=A(I)          DYN13540
0213      170 CONTINUE          DYN13550
C
0214      RETURN          DYN13555
0215      END          DYN13560
                                         DYN13570

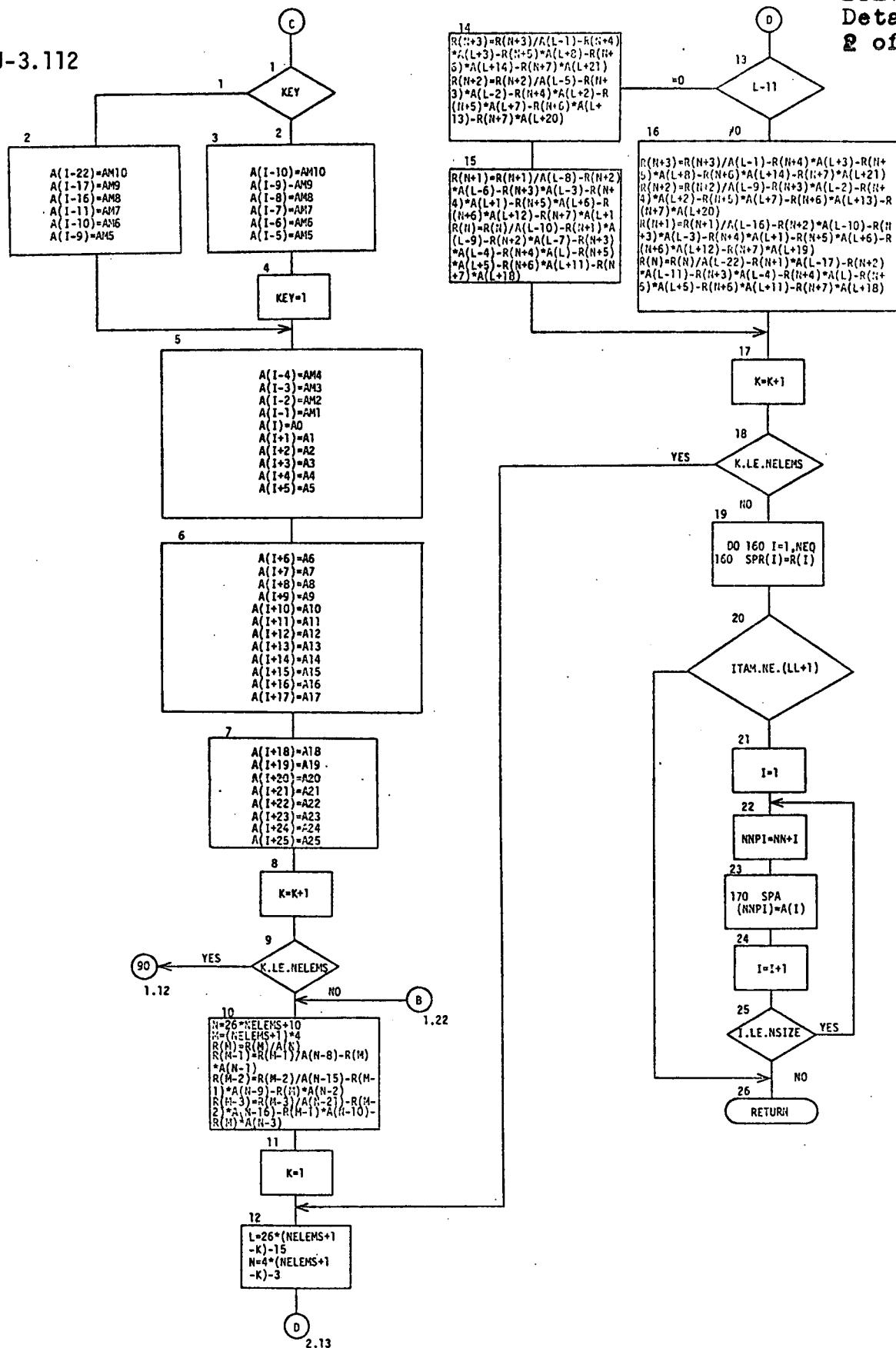
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CE(STRESS)                               DYN13582
C                                         DYN13584
C      DESCRIPTION - TO CALCULATE THE MIDSURFACE STRESSES AND      DYN13586
C      STRESS RESULTANTS ON THE UPPER AND LOWER SHELL SURFACES.      DYN13588
C                                         DYN13590
C      INPUT ARGUMENTS.                                              DYN13592
C      DTH    = MATRIX OF FOURIER COEFFICIENTS FOR THE CIRCUMFERENTIAL      DYN13594
C                  TEMPERATURE GRADIENT DISTRIBUTION.                      DYN13596
C      IHARM  = MATRIX OF HARMONIC NUMBERS FOR WHICH DISPLACEMENTS      DYN13598
C                  AND/OR STRESSES WILL BE CALCULATED.                      DYN13600
C      ITAM   = NUMBER OF TIME CYCLE.                                    DYN13602
C      I1     = PRINT FLAG FOR STRESSES.                                 DYN13604
C      NH     = TOTAL NUMBER OF HARMONICS USED IN THE DYNAMIC ANALYSIS. DYN13606
C      NTHETA = THE NUMBER OF CIRCUMFERENTIAL ANGLES AT WHICH DISPLACE- DYN13608
C                  MENTS AND/OR STRESSES ARE TO BE CALCULATED.              DYN13610
C      TH     = MATRIX WHOSE ELEMENTS ARE THE FOURIER COEFFICIENTS      DYN13612
C                  OF THE CIRCUMFERENTIAL TEMPERATURE DISTRIBUTION.          DYN13614
C      THETA  = MATRIX CONTAINING CIRCUMFERENTIAL ANGLES AT WHICH      DYN13616
C                  STRESSES AND/OR DISPLACEMENTS ARE TO BE CALCULATED.      DYN13618
C                                         DYN13620
C      EXTERNALS.                                                 DYN13622
C      CALLED BY                                                 DYN13624
C      NLTERM                                                 DYN13626
C                                         DYN13628
C      SUBROUTINE STRESS (I1,ITAM)                                     DYN13630
C      IMPLICIT REAL*8 (A-H,O-Z)                                      DYN13632
C      COMMON /EES/ ES(5),ET(5),EST(5),E13(5),E23(5)                 DYN13634
C      COMMON /CONST/ NH,NELEMS,NNODES,NSIZE,NPRNTQ,NEQ,NEQT,N,NN,NHNS, DYN13636
C      1           DT2,NPRNTL,NPRNTF,IDEF,IODE                           DYN13638
C      COMMON /THETAS/ THETA(20),NTHETA,NCLCST,NSTRSS                DYN13640
C      COMMON /GEOM/ FNU1(50),FNU2(50),E1(50),E2(50),G(50),T(50), DYN13642
C      1           SINE(51),COSINE(51),SINM(50),COSM(50),R(50),PH(50), DYN13650
C      1           PHP(50),ARCL(50)                                     DYN13652
C      COMMON /GCD/ CC1,CC2,DD1,DD2,GG1,GG2                         DYN13660
C      COMMON /HARM/ NHP,IHARM(5)                                    DYN13670
C      COMMON /TMFT/ TOTIME,DELTE,TIME,T0,T1                         DYN13680
C      COMMON /QS/ QN(1020),QN1(1020),FORCE(2040),QP(1020),QP1(1020), DYN13690
C      1           QN2(1020)                                       DYN13700
C      COMMON /THER/ TH(50,5,2),DTH(50,5,2),ALS(50),ALT(50)        DYN13710
C      DIMENSION BSTRMS(20), BSTRMT(20), BSTMST(20), BTMST(20),       DYN13720
C      1           BSTMT(20)                                       DYN13730
C      ITAM1=ITAM-1                                              DYN13780
C      TM1=TIME-DELTE                                           DYN13790
C      TPRINT=TM1*1000000.                                         DYN13800
C      IF (I1.EQ.1) WRITE (6,50) ITAM1,TPRINT                     DYN13810
C100  PROCESS ANGLES                                         DYN13812
C                                         DYN13818
C      DO 40 I=1,NTHETA                                     DYN13820

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    0018                    ESU=0.0                    DYN13830
    0019                    ETU=0.0                    DYN13840
    0020                    ESTU=0.0                    DYN13850
    0021                    E13U=0.0                    DYN13860
    0022                    E23U=0.0                    DYN13870
    0023                    CHIS=0.0                    DYN13880
    0024                    CHIT=0.0                    DYN13890
    0025                    CHIST=0.0                    DYN13900
    0026                    CTHIS=0.0                    DYN13910
    0027                    CTHIT=0.0                    DYN13920
    0028                    CTHIST=0.0                    DYN13930
    0029                    ESUT=0.0                    DYN13940
    C100                    PROCESS HARMONICS                    DYN13950
    C                                                    DYN13958
    0030                    DO 10 IH=1,NH                    DYN13960
    0031                    XIH1=IHARM(IH)                    DYN13970
    0032                    CS=DCOS(XIH1*THETA(I))                    DYN13980
    0033                    SN=DSIN(XIH1*THETA(I))                    DYN13990
    0034                    K=4*(I1-1)+NEQ*(IH-1)                    DYN14000
    0035                    THT=TH(I1,IH,1)+(TH(I1,IH,2)-TH(I1,IH,1))*(TIME-T0)/(T1-T0)                    DYN14010
    0036                    DTHT=DTH(I1,IH,1)+(DTH(I1,IH,2)-DTH(I1,IH,1))*(TIME-T0)/(T1-DYN14020
    1                                                    DYN14021
    C1                    CALCULATION OF LINEAR STRAINS AND ROTATIONS                    DYN14023
    0037                    ESU=ESU+ES(IH)*CS                    DYN14040
    0038                    ETU=ETU+ET(IH)*CS                    DYN14050
    0039                    ESTU=ESTU+EST(IH)*SN                    DYN14060
    0040                    E13U=E13U+E13(IH)*CS                    DYN14070
    0041                    E23U=E23U+E23(IH)*SN                    DYN14080
    0042                    ESUT=ESUT+ALS(I1)*THT*CS                    DYN14090
    0043                    ETUT=ETUT+ALT(I1)*THT*CS                    DYN14100
    C1                    CALCULATION OF CHANGES IN CURVATURE                    DYN14102
    0044                    QB3=-QN(K+1)*SINE(I1)+QN(K+3)*COSINE(I1)                    DYN14120
    0045                    QB7=-QN(K+5)*SINE(I1+1)+QN(K+7)*COSINE(I1+1)                    DYN14130
    0046                    CHIS1=(QN(K+4)-QN(K+8))/ARCL(I1)                    DYN14140
    0047                    CHIS2=ALS(I1)*DTHT                    DYN14150
    0048                    CHIS=CHIS+(CHIS1-CHIS2)*CS                    DYN14160
    0049                    CHIT1=(-XIHI*E23(IH)-SINM(I1)*E13(IH))/R(I1)                    DYN14170
    0050                    CHIT2=ALT(I1)*DTHT                    DYN14180
    0051                    CHIT=CHIT+(CHIT1-CHIT2)*CS                    DYN14190
    0052                    CHIST1=(XIHI*E13(IH)+SINM(I1)*E23(IH)-XIHI*SINM(I1)*(QB3+
    1                                                    DYN14200
    2                                                    DYN14210
    3                                                    DYN14220
    3                                                    DYN14230
    0053                    CHIST=CHIST+CHIST1*SN                    DYN14240
    0054                    CTHIS=CTHIS+XIHI*(CHIS1-CHIS2)*(-SN)                    DYN14250
    0055                    CTHIT=CTHIT+XIHI*(CHIT1-CHIT2)*(-SN)                    DYN14260
    0056                    CTHIST=CTHIST+XIHI*CHIST1*CS                    DYN14270
    0057                    10                    CONTINUE                    DYN14280
  
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C          CALCULATION OF MIDSURFACE STRAINS           DYN14283
0058      EPS=ESU+.5*E13U**2-ESUT                  DYN14285
0059      EPT=ETU+.5*E23U**2-ETUT                  DYN14300
0060      EPST=ESTU+E13U*E23U                      DYN14310
C          CALCULATION OF STRESS AND MOMENT RESULTANTS DYN14320
0061      STRNS=CC1*EPS+FNU1(I1)*CC1*EPT           DYN14322
0062      STRNT=FNU2(I1)*CC2*EPS+CC2*EPT           DYN14340
0063      STRNST=GG1*EPST                          DYN14350
0064      STRMS=DD1*CHIS+FNU1(I1)*DD1*CHIT         DYN14360
0065      STRMT=FNU2(I1)*DD2*CHIS+DD2*CHIT         DYN14370
0066      STRMST=GG2*CHIST                         DYN14380
C          CALCULATE STRESSES ON THE INNER AND OUTER SURFACES DYN14390
0067      C1ST=1.0/T(I1)                           DYN14392
0068      C2ST=6.0/T(I1)**2                         DYN14410
0069      BSU=C1ST*STRNS+C2ST*STRMS               DYN14420
0070      BTU=C1ST*STRNT+C2ST*STRMT               DYN14430
0071      BSTU=C2ST*STRMST+C1ST*STRNST            DYN14440
0072      BSL=C1ST*STRNS-C2ST*STRMS               DYN14450
0073      BTL=C1ST*STRNT-C2ST*STRMT               DYN14460
0074      BSTL=-C2ST*STRMST+C1ST*STRNST            DYN14470
C          CALCULATE SHEAR RESULTANTS AND PRINT OUTPUT INFORMATION DYN14480
0075      SSTMST=FNU2(I1)*DD2*CTHIS+DD2*CTHIT     DYN14482
0076      SSTMST=GG2*CTHIST                        DYN14500
0077      THETA1=THETA(I1)*180./3.14159           DYN14510
0078      IF (I1.NE.1) GO TO 20                     DYN14520
0079      WRITE (6,60) I1,THETA1,STRNS,STRNT,STRNST,STRMS,STRMT,STRMST, DYN14530
          1   BSU,BTU,BSTU,BSL,BTL,BSTL             DYN14540
          1   GO TO 30                                DYN14550
0080      20 RAV=(R(I1)+R(I1-1))/2.                  DYN14560
0081      PAV=(PH(I1)+PH(I1-1))/2.                  DYN14570
0082      AAV=(ARCL(I1)+ARCL(I1-1))/2.              DYN14580
0083      SHRS=1./RAV*((R(I1)*STRMS-R(I1-1)*BSTRMS(I1))/AAV+(SSTMST+ DYN14590
          1   BTTMST(I1))/2.-DSIN(PAV)*(STRMT+BSTRMT(I1))/2.) DYN14600
0084      SHRT=1./RAV*((R(I1)*STRMST-R(I1-1)*BSTMST(I1))/AAV+(SSTMST+ DYN14610
          1   BTTMST(I1))/2.+DSIN(PAV)*(STRMST+BSTMST(I1))/2.) DYN14620
0085      WRITE (6,70) I1,THETA1,STRNS,STRNT,STRNST,STRMS,STRMT,STRMST, DYN14630
          1   SHRS,SHRT,BSU,BTU,BSTU,BSL,BTL,BSTL             DYN14640
0086      30 BSTRMS(I)=STRMS                        DYN14650
0087      BSTRMT(I)=STRMT                         DYN14660
0088      BSTMST(I)=STRMST                        DYN14670
0089      BTTMST(I)=SSTMST                        DYN14680
0090      BTTMST(I)=SSTMST                        DYN14690
0091      BTTMST(I)=SSTMST                        DYN14700
0092      40 CONTINUE                               DYN14710
C          RETURN                                  DYN14713
0093      C          RETURN                         DYN14720
0094      50 FORMAT (1H1,3X,6HITAM =,I5,3X,6HTIME =,F12.4,13H MICROSECONDS,// DYN14730

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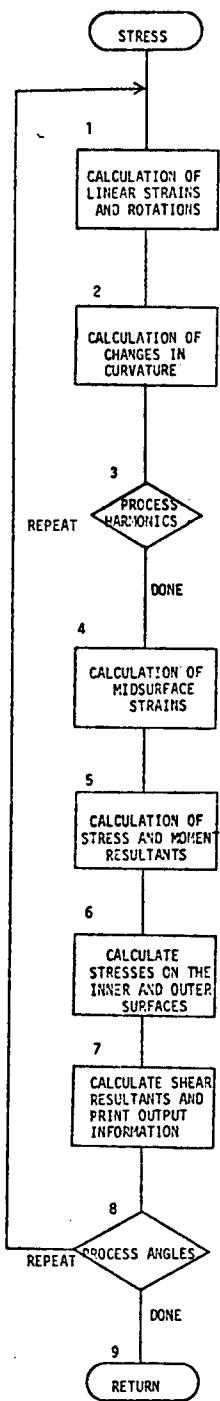
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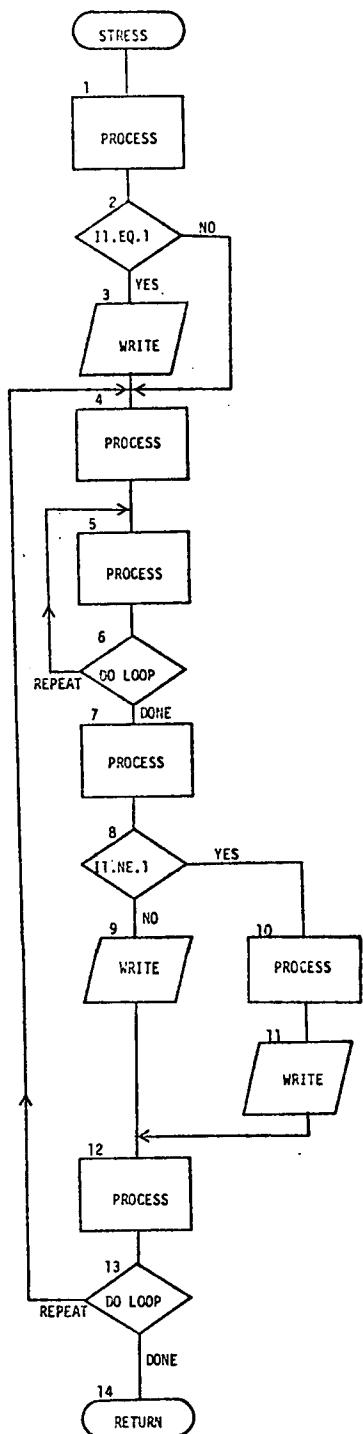
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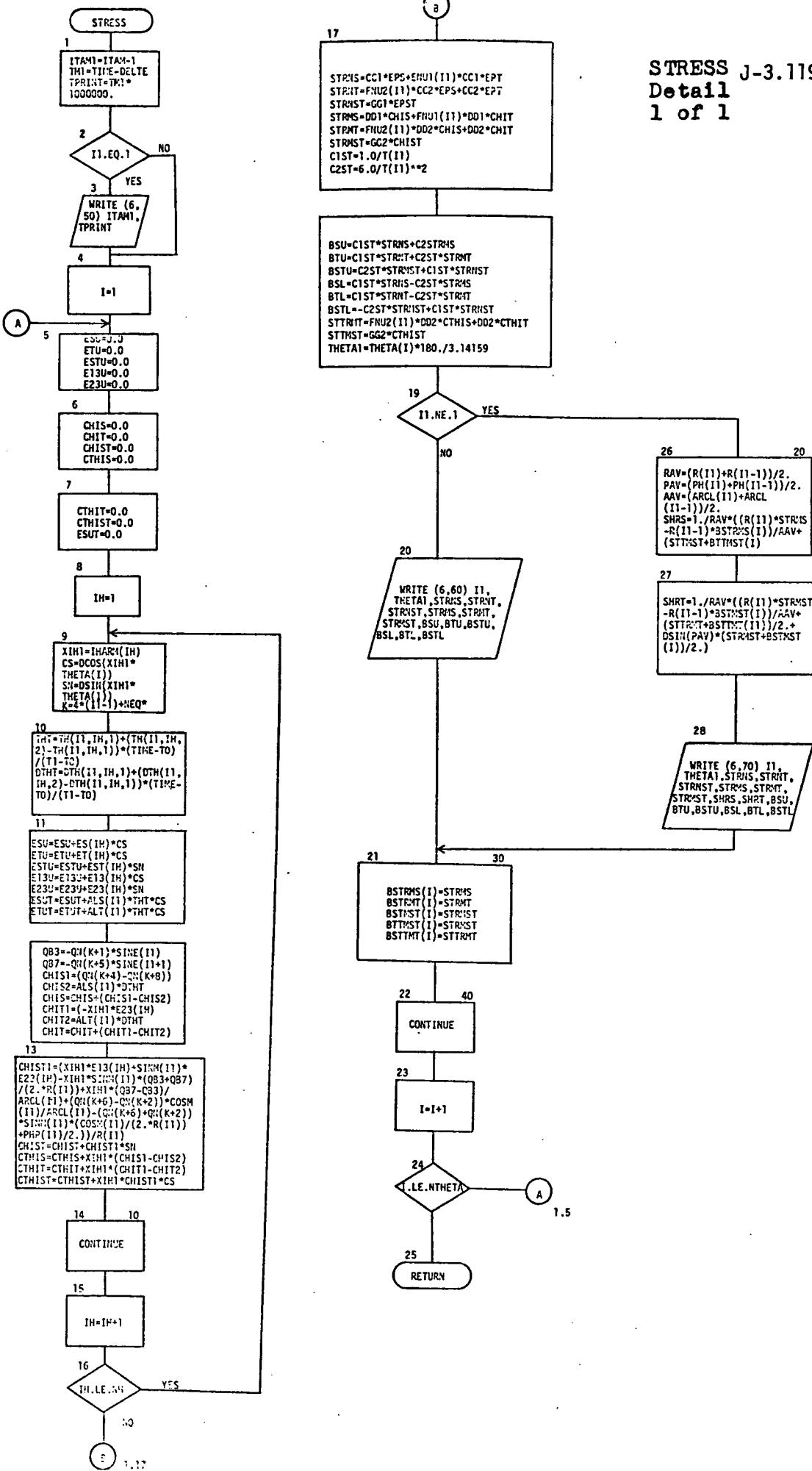
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1      47X,33HSTRESSES AND STRESS RESULTANTS,/          DYN14750
2      25X,17HFORCE RESULTANTS,31X,18HMOMFNT RESULTANTS,18X,  DYN14760
2      17HSHEAR RESULTANTS/                           DYN14770
2      19X,4HN(S),11X,4HN(T),11X,5HN(ST),10X,4HM(S),11X,4HM(T), DYN14780
2      11X,5HM(ST),10X,4HQ(S),11X,4HQ(T)//12H ELEM THETA,/ DYN14790
3      53H NO (DEG) ***** OUTER SURFACE STRESSES ,DYN14800
3      51H ***** INNER SURFACE STRESSES *****,/ DYN14810
4      15X,41H* SIGMA(S)      SIGMA(T)      SIGMA(ST), DYN14820
4      47H      SIGMA(S)      SIGMA(T)      SIGMA(ST) */ DYN14822
0095   60 FORMAT (I4,F8.2,6(1PD15.4),30H      XXXX      XXXX ,/ DYN14830
        1      12H STRESSES **,6(1PD15.4))           DYN14840
0096   70 FORMAT (I4,F8.2,8(1PD15.4),/,12H STRESSES **,6(1PD15.4)) DYN14850
3097   END                                         DYN14860
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CE(TFORCE) DYN16852
C DYN16854
C DESCRIPTION - TO CALCULATE THE LINEAR THERMAL LOADS ON DYN16856
C THE SHELL STRUCTURE. DYN16858
C DYN16860
C INPUT ARGUMENTS. DYN16862
C ARCL = MATRIX OF THE ARC LENGTHS OF THE ELEMENTS (S-DIRECTION). DYN16864
C IB = FORCE ARRAY STEPPING PARAMETER, USED TO MODIFY CURRENT DYN16866
C BLOCK OF STORAGE FOR FORCE. DYN16868
C IELM = NUMBER OF SHELL ELEMENTS. DYN16870
C IHARM = MATRIX OF HARMONIC NUMBERS FOR WHICH DISPLACEMENTS DYN16872
C AND/OR STRESSES WILL BE CALCULATED. DYN16874
C NELEMS = TOTAL NUMBER OF ELEMENTS USED TO IDEALIZE THE STRUCTURE. DYN16876
C NH = TOTAL NUMBER OF HARMONICS USED IN THE DYNAMIC ANALYSIS. DYN16878
C PHP = DPHI/DS AT THE MIDDLE OF AN ELEMENT. DYN16880
C TH = MATRIX WHOSE ELEMENTS ARE THE FOURIER COEFFICIENTS DYN16882
C OF THE CIRCUMFERENTIAL TEMPERATURE DISTRIBUTION. DYN16884
C DYN16886
C OUTPUT ARGUMENTS. DYN16888
C FORCE = MATRIX OF GENERALIZED FORCES DUE TO EXTERNAL LOADS AND DYN16890
C TEMPERATURES. DYN16892
C Q THERMAL COEFFICIENTS USED IN CALCULATING GENERALIZED DYN16894
C LINEAR LOADS DUE TO THERMAL EFFECTS. DYN16896
C QQ = GENERALIZED LINEAR LOADS DUE TO THERMAL EFFECTS. DYN16898
C DYN16900
C EXTERNALS. DYN16902
C CALLED BY DYN16904
C INPUT DYN16906
C DYN16908
0001 SUBROUTINE TFORCE (IELM,IB) DYN16910
0002 IMPLICIT REAL*8 (A-H,O-Z) DYN16912
0003 COMMON /GEOM/ FNU1(50),FNU2(50),E1(50),E2(50),G(50),T(50), DYN16914
1 SINE(51),COSINE(51),SINM(50),COSM(50),R(50),PH(50), DYN16916
1 PHP(50),ARCL(50) DYN16918
0004 COMMON /THER/ TH(50,5,2),DTH(50,5,2),ALS(50),ALT(50) DYN16920
0005 COMMON /HARM/ NHP,IHARM(5) DYN16922
0006 COMMON /CHALS/ AL(167),CHECK(6,8) DYN16924
0007 COMMON /CONST/ NH,NELEMS,NNODES,NSIZE,NPRNTQ,NEQ,NEQT,N,NN,NHNS, DYN16928
1 DT2,NPRNTL,NPRNTF,IDEFL,IDCDE DYN16930
0008 COMMON /QS/ QN(1020),QN1(1020),FORCE(2040),QP(1020),QP1(1020), DYN16940
1 QN2(1020) DYN16950
0009 COMMON /QUES/ Q(8),QQ(8) DYN16960
0010 DIMENSION CES(4) DYN16970
0011 C1 LINEAR THERMAL LOADS DYN16972
0012 PI=3.14159265 DYN17010
0012 CES(1)=PI*E1(IELM)*T(IELM)/(1.-FNU1(IELM)*FNU2(IELM))*(ALS(IELM)+ DYN17020
1 FNU1(IELM)*ALT(IELM)) DYN17030
0013 CES(2)=PI*E2(IELM)*T(IELM)/(1.-FNU1(IELM)*FNU2(IELM))*(ALT(IELM)+ DYN17040

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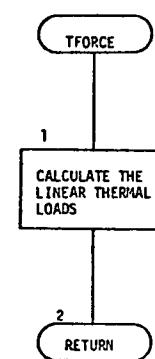
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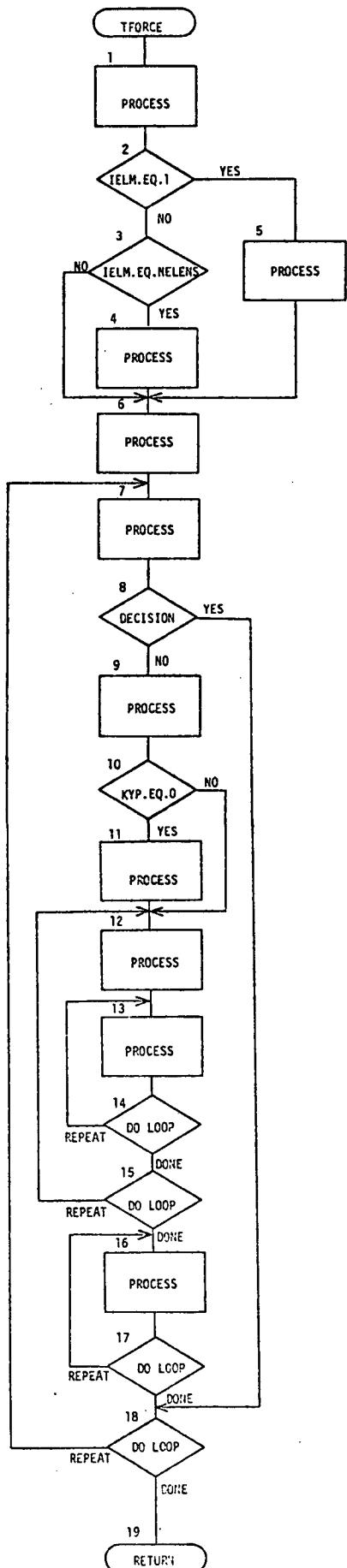
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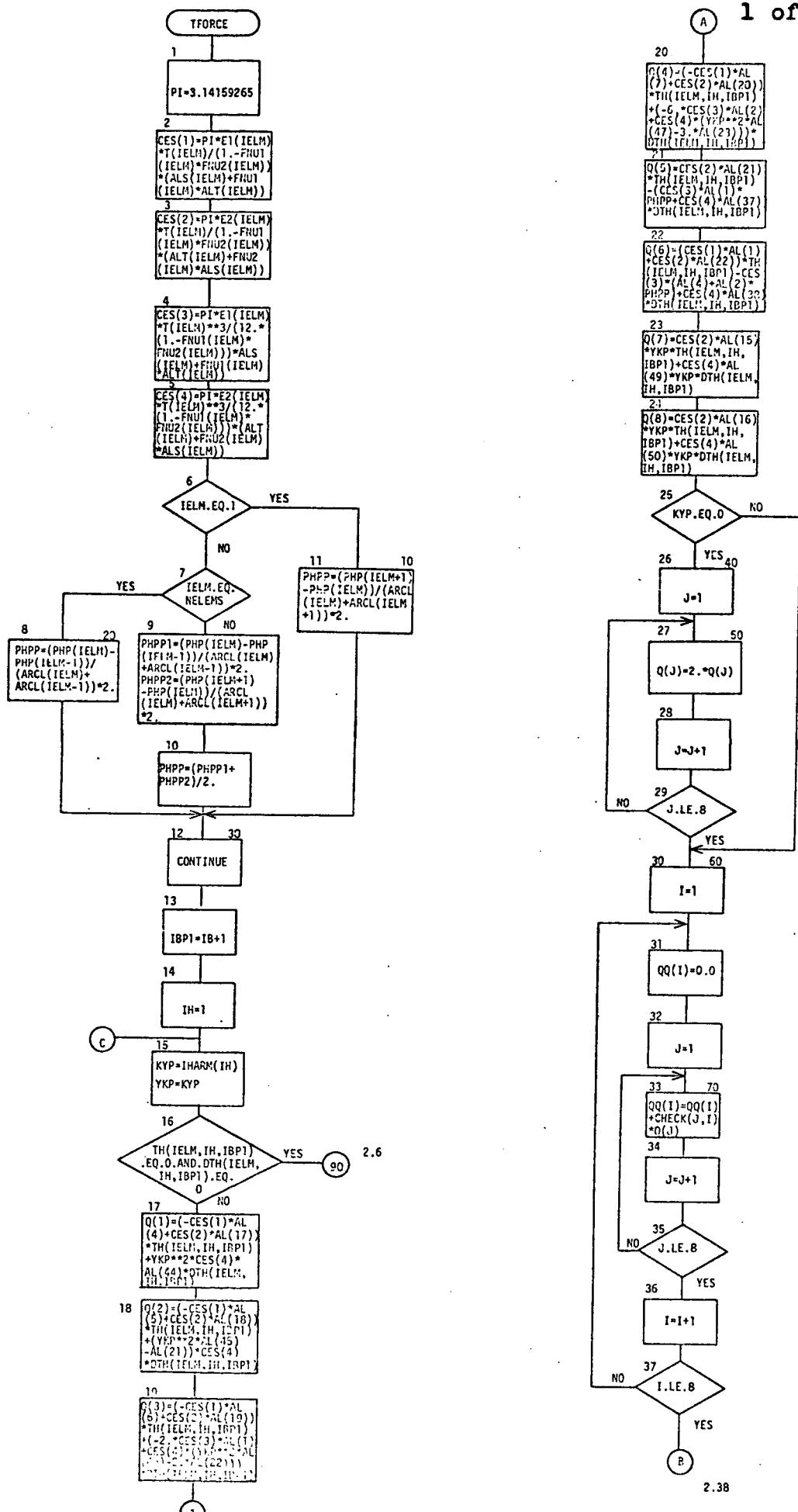
0014      FNU2IELM)*ALSIELM))*
          CES(3)=PI*E1IELM)*TIELM)**3/(12.*(1.-FNU1IELM)*FNU2IELM))**
          (ALSIELM)+FNU1IELM)*ALTIELM))
          CES(4)=PI*E2IELM)*TIELM)**3/(12.*(1.-FNU1IELM)*FNU2IELM))**
          (ALTIELM)+FNU2IELM)*ALSIELM))*
          C
          C   CALCULATE PHPPIELM)
          C
0016      IF (IELM.EQ.1) GO TO 10
0017      IF (IELM.EQ.NELEMS) GO TO 20
0018      PHPP1=(PHPIELM-PHPIELM-1)/(ARCLIELM)+ARCLIELM-1)*2.
0019      PHPP2=(PHPIELM+1-PHPIELM)/(ARCLIELM)+ARCLIELM+1)*2.
0020      PHPP=(PHPP1+PHPP2)/2.
0021      GO TO 30
0022      10 PHPP=(PHPIELM+1-PHPIELM)/(ARCLIELM)+ARCLIELM+1)*2.
0023      GO TO 30
0024      20 PHPP=(PHPIELM-PHPIELM-1)/(ARCLIELM)+ARCLIELM-1)*2.
0025      30 CONTINUE
0026      IBP1=IB+1
          C
0027      DO 90 IH=1,NH
          KYP=IHARMIH)
          YKP=YKP
          IF (THIELM,IH,IBP1).EQ.0. AND. DTHIELM,IH,IBP1).EQ.0) GO TO 90
          Q(1)=(-CES(1)*AL(4)+CES(2)*AL(17))*THIELM,IH,IBP1)+YKP**2*
          CES(4)*AL(44)*DTHIELM,IH,IBP1)
          Q(2)=(-CES(1)*AL(5)+CES(2)*AL(18))*THIELM,IH,IBP1)+(YKP**2*
          AL(45)-AL(21))*CES(4)*DTHIELM,IH,IBP1)
          Q(3)=(-CES(1)*AL(6)+CES(2)*AL(19))*THIELM,IH,IBP1)+(-2.*CES(3)*AL(1)+CES(4)*(YKP**2*AL(46)-2.*AL(22)))*
          DTHIELM,IH,IBP1)
          Q(4)=(-CES(1)*AL(7)+CES(2)*AL(20))*THIELM,IH,IBP1)+(-6.*CES(3)*AL(2)+CES(4)*(YKP**2*AL(47)-3.*AL(23)))*
          DTHIELM,IH,IBP1)
          Q(5)=CES(2)*AL(21)*THIELM,IH,IBP1)-(CES(3)*AL(1)*PHPP+CES(4)*
          AL(37))*DTHIELM,IH,IBP1)
          Q(6)=(CES(1)*AL(1)+CES(2)*AL(22))*THIELM,IH,IBP1)-(CES(3)*
          (AL(4)+AL(2)*PHPP)+CES(4)*AL(38))*DTHIELM,IH,IBP1)
          Q(7)=CES(2)*AL(15)*YKP*THIELM,IH,IBP1)+CES(4)*AL(49)*YKP*
          DTHIELM,IH,IBP1)
          Q(8)=CES(2)*AL(16)*YKP*THIELM,IH,IBP1)+CES(4)*AL(50)*YKP*
          DTHIELM,IH,IBP1)
          IF (KYP.EQ.0) GO TO 40
          GO TO 60
          C
0041      40 DO 50 J=1,8
          Q(J)=2.*Q(J)
0042
0043      50 CONTINUE

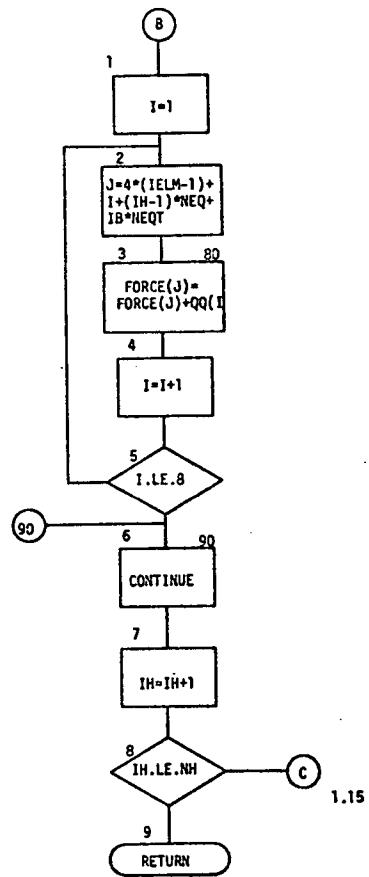
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C			DYN17475	
C			DYN17478	
0044	60 DO 70 I=1,8		DYN17480	
0045	QQ(I)=0.0		DYN17490	
C			DYN17498	
0046	DO 70 J=1,8		DYN17500	
0047	QQ(I)=QQ(I)+CHECK(J,I)*Q(J)		DYN17510	
0048	70 CONTINUE		DYN17512	
C			DYN17515	
C			DYN17518	
0049	DO 80 I=1,8		DYN17520	
0050	J=4*(IELM-1)+I+(IH-1)*NEQ+IB*NEQT		DYN17530	
0051	FORCE(J)=FORCE(J)+QQ(I)		DYN17540	
0052	80 CONTINUE		DYN17542	
C			DYN17545	
0053	90 CONTINUE		DYN17550	
C			DYN17553	
0054	RETURN		DYN17560	
0055	END		DYN17570	









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CE(THCOE)                               DYN16102
C                                         DYN16104
C      DESCRIPTION - TO READ IN THE TEMPERATURE AND TEMPERATURE      DYN16106
C          GRADIENTS FOR UTILIZATION IN COMPUTING THE THERMAL      DYN16108
C          FOURIER COEFFICIENTS.                                     DYN16110
C                                         DYN16112
C      INPUT ARGUMENTS.                                              DYN16114
C          IB     = FORCE ARRAY STEPPING PARAMETER, USED TO MODIFY CURRENT DYN16116
C                      BLOCK OF STORAGE FOR FORCE.                      DYN16118
C          IELM   = NUMBER OF SHELL ELEMENTS.                         DYN16120
C          IHARM  = MATRIX OF HARMONIC NUMBERS FOR WHICH DISPLACEMENTS DYN16122
C                      AND/OR STRESSES WILL BE CALCULATED.                DYN16124
C          NH     = TOTAL NUMBER OF HARMONICS USED IN THE DYNAMIC ANALYSIS. DYN16126
C                                         DYN16128
C      OUTPUT ARGUMENTS.                                             DYN16130
C          DTH    = MATRIX OF FOURIER COEFFICIENTS FOR THE CIRCUMFERENTIAL DYN16132
C                      TEMPERATURE GRADIENT DISTRIBUTION.                 DYN16134
C          TH     = MATRIX WHOSE ELEMENTS ARE THE FOURIER COEFFICIENTS DYN16136
C                      OF THE CIRCUMFERENTIAL TEMPERATURE DISTRIBUTION.       DYN16138
C                                         DYN16140
C      EXTERNALS.                                                 DYN16142
C          CALLED BY                                              DYN16144
C              INPUT                                              DYN16146
C                                         DYN16148
0001      SUBROUTINE THCOE (IELM,IB)                                DYN16150
0002      IMPLICIT REAL*8 (A-H,O-Z)                                DYN16152
0003      COMMON /CONST/ NH,NELEMS,NNODES,NSIZE,NPRNTQ,NEQ,NEQT,N,NN,NHNS, DYN16154
0004          1 DT2,NPRNTL,NPRNTF,IDELFL, IDCOE                     DYN16156
0005      COMMON /FRCE/ P(74),R(74),S(74),THETB(74)                  DYN16158
0006      COMMON /THER/ TH(5C,5,2),DTH(50,5,2),ALS(50),ALT(50)        DYN16160
0007      COMMON /HARM/ NHP,IHARM(5)                                DYN16162
0008      COMMON /TAPES/ NT,ND,NS                                 DYN16170
0009      IF (IELM.EQ.1) IELM2=0                                  DYN16220
0009      PI=3.14159265                                         DYN16230
0010      C1 FIRST ELEMENT//NO{3C}                                DYN16232
0010      IF (IELM.LE.IELM2.AND.IELM.NE.1) GO TO 30             DYN16240
0011      IF (NPRNTL.EQ.1.AND.IELM.EQ.1) WRITE (6,110)           DYN16250
0011      C
0011      C1S(IO) READ TEMPERATURE DISTRIBUTION                 DYN16260
0012      C
0012      READ INPUT DATA FOR CARD TYPE IX - D - 1            DYN16262
0012      READ (ND,120) IELM1,IELM2,NDP,(THETB(I),P(I),R(I),I=1,NDP) DYN16280
0013      NDP2=2*NDP+1                                         DYN16290
0013      C
0014      DO 10 IF=1,NDP                                         DYN16300
0015          ANG=360.0-THETB(NDP)                                DYN16310
0016          KEY=NDP2-IF                                         DYN16320
0016          THETB(KEY)=ANG                                    DYN16330
0017                                         DYN16340
0017                                         DYN16350

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0018      P(KEY)=P(IF)          DYN16360
0019      R(KEY)=R(IF)          DYN16370
0020      10 CONTINUE           DYN16380
0021      C                      DYN16383
0021      IF (NPRNTL.EQ.1) WRITE (6,130) IELM1,IELM2,(P(I),R(I),THETB(I),
0021      1           THETB(I+1),I=1,NDP)          DYN16390
0022      ND2=2*NDP              DYN16400
0023      C                      DYN16410
0023      DO 20 IDP=1,ND2        DYN16418
0024      THETB(IDP)=THETB(IDP)/57.2957795   DYN16420
0025      20 CONTINUE            DYN16430
0026      C                      DYN16432
0026      30 CONTINUE            DYN16435
0027      C1                     CALCULATE THERMAL FOURIER COEFFICIENTS DYN16440
0027      C                      DYN16442
0027      DO 100 IH=1,NH         DYN16448
0028      KYP=IHARM(IH)          DYN16450
0029      YKP=KYP                DYN16460
0030      PINT=0.0                DYN16470
0031      RINT=0.0                DYN16480
0032      IF (NDP.EQ.1) GO TO 70   DYN16490
0033      IF (KYP.GT.0) GO TO 50   DYN16500
0034      C                      DYN16510
0034      DO 40 I=1,NDP          DYN16518
0035      PINT=PINT+P(I)*(THETB(I+1)-THETB(I))   DYN16520
0036      RINT=RINT+R(I)*(THETB(I+1)-THETB(I))   DYN16530
0037      40 CONTINUE             DYN16540
0038      C                      DYN16542
0038      PINT=PINT/(2.*PI)       DYN16545
0039      RINT=RINT/(2.*PI)       DYN16550
0040      GO TO 90                DYN16560
0041      C                      DYN16570
0041      50 DO 60 I=1,NDP        DYN16578
0042      X1=THETB(I)*YKP        DYN16580
0043      X2=THETB(I+1)*YKP      DYN16590
0044      PINT=PINT+P(I)*(DSIN(X2)-DSIN(X1))/YKP   DYN16600
0045      RINT=RINT+R(I)*(DSIN(X2)-DSIN(X1))/YKP   DYN16610
0046      60 CONTINUE             DYN16620
0047      C                      DYN16622
0047      PINT=PINT/PI            DYN16625
0048      RINT=RINT/PI            DYN16630
0049      GO TO 90                DYN16640
0050      70 IF (KYP.GT.0) GO TO 80   DYN16650
0051      PINT=P(1)               DYN16660
0052      RINT=R(1)               DYN16670
0053      GO TO 90                DYN16680
0054      80 PINT=0.0              DYN16690
0055      RINT=0.0                DYN16700

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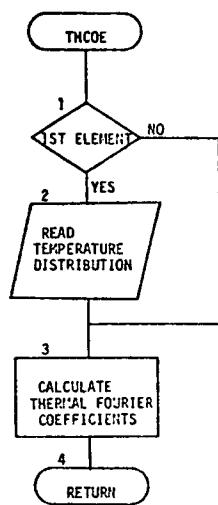
THCOE

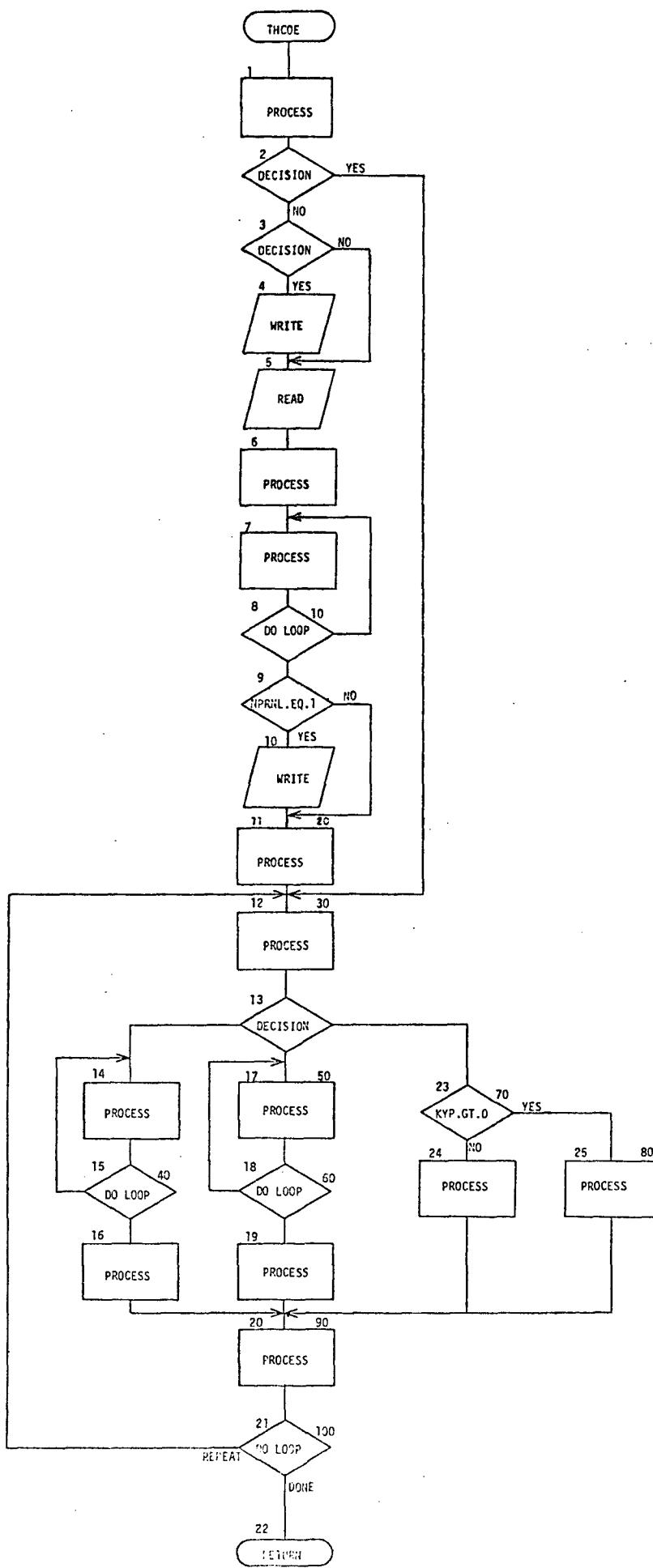
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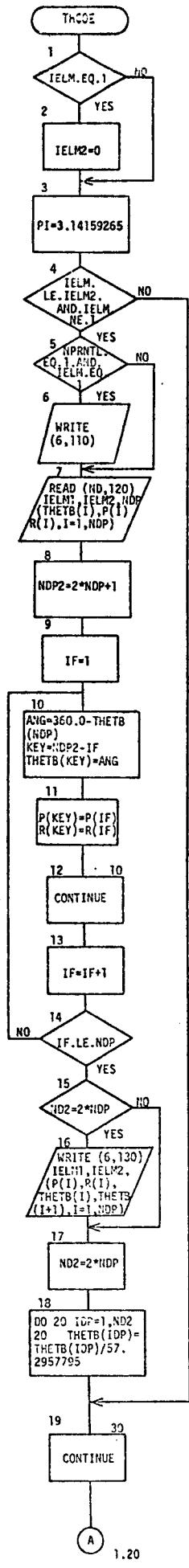
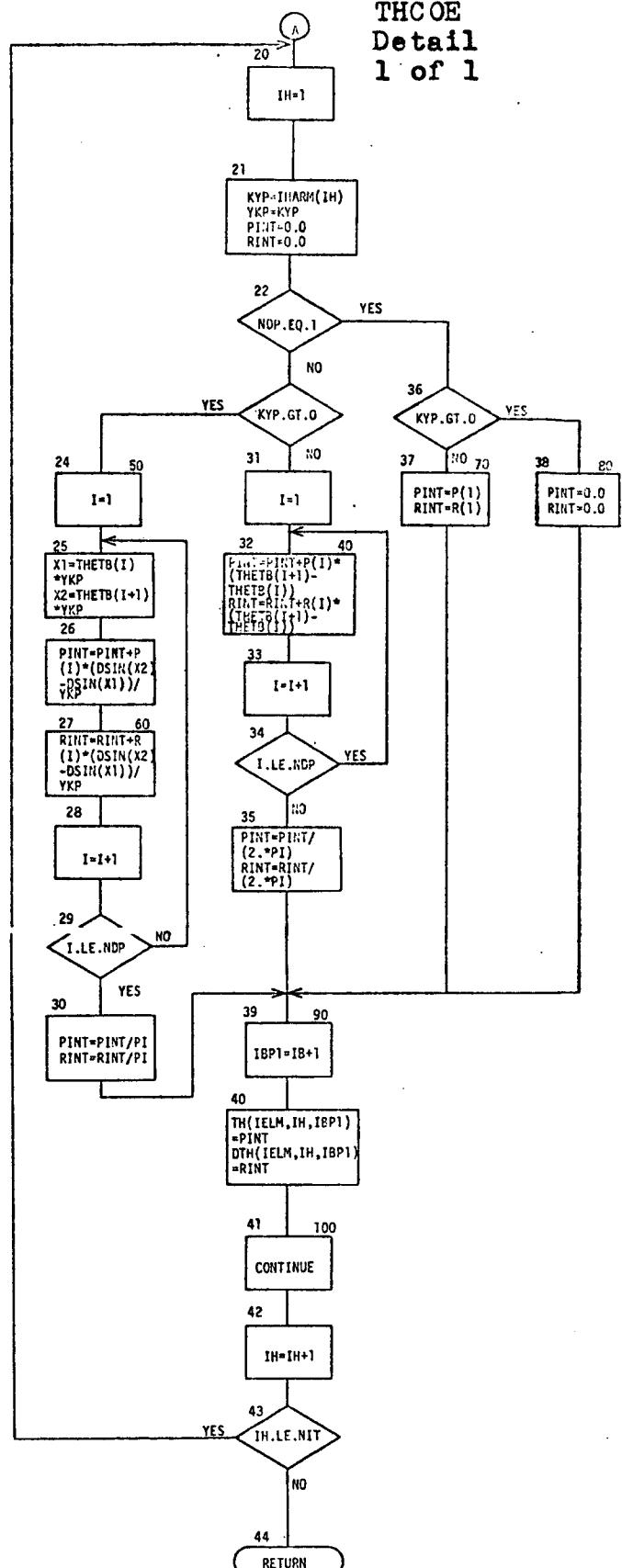
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0056      90      IBP1=IB+1          DYN16720
0057      THIELM,IH,IBP1)=PINT    DYN16730
0058      DTHIELM,IH,IBP1)=RINT    DYN16740
0059      100 CONTINUE
C
0060      RETURN
C
0061      110 FORMAT (1H1,31X,47HTEMPERATURES AND THERMAL GRADIENTS ON,
1           10H STRUCTURE///
1           27X,11HTEMPERATURE,10X,16HTHERMAL GRADIENT,10X,
2           29HFROM THETA TO THETA (DEGREES)//)
0062      120 FORMAT (3I5/(3F10.0))
0063      130 FORMAT (/,60X,11HELEMENT NO.,I3,1H-,I2,//
1           (28X,F9.3,15X,F10.3,16X,F7.2,2X,F7.2))
0064      END
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CE(TRI40R)
C
C      DESCRIPTION - TO CALCULATE THE VARIOUS TRIGONOMETRIC
C      INTEGRALS REQUIRED IN THE CALCULATIONS OF THE
C      GENERALIZED NONLINEAR LOADS.
C
C      INPUT ARGUMENTS.
C      IHARM = MATRIX OF HARMONIC NUMBERS FOR WHICH DISPLACEMENTS
C              AND/OR STRESSES WILL BE CALCULATED.
C      NH    = TOTAL NUMBER OF HARMONICS USED IN THE DYNAMIC ANALYSIS.
C
C      OUTPUT ARGUMENTS.
C      CCC   = MATRIX CONTAINING INTEGRALS FROM 0 TO 2*PI OF
C              COS(I*THETA) * COS(J*THETA) * COS(K*THETA) * DTHETA.
C      CCCC  = MATRIX CONTAINING INTEGRALS FROM 0 TO 2*PI OF
C              COS(I*THETA) * COS(J*THETA) * COS(K*THETA) *
C              COS(L*THETA) * DTHETA.
C      CSS   = MATRIX CONTAINING INTEGRALS FROM 0 TO 2*PI OF
C              COS(I*THETA) * SIN(J*THETA) * SIN(K*THETA) * DTHETA.
C      SSC   = MATRIX CONTAINING INTEGRALS FROM 0 TO 2*PI OF
C              SIN(I*THETA) * SIN(J*THETA) * COS(K*THETA) * DTHETA.
C      SSCC  = MATRIX CONTAINING INTEGRALS FROM 0 TO 2*PI OF
C              SIN(I*THETA) * SIN(J*THETA) * COS(K*THETA) *
C              COS(L*THETA) * DTHETA.
C      SSSS  = MATRIX CONTAINING INTEGRALS FROM 0 TO 2*PI OF
C              SIN(I*THETA) * SIN(J*THETA) * SIN(K*THETA) *
C              SIN(L*THETA) * DTHETA.
C
C      EXTERNALS.
C      CALLED BY
C          INPUT
C
0001      SUBROUTINE TRI40R                               DYN17646
0002      IMPLICIT REAL*8 (A-H,O-Z)                      DYN17648
0003      COMMON /CS/ CCC(125),SSC(125),CSS(125)        DYN17650
0004      COMMON /CS4/ CCCC(625),SSSS(625),SSCC(625),SCCS(625) DYN17652
0005      COMMON /CONST/ NH,NELEMS,NNODES,NSIZE,NPRNTQ,NEQ,NEQT,N,NN,NHNS, DYN17654
1          DT2,NPRNTL,NPRNTF,IDEFL,IDCOE                 DYN17656
0006      COMMON /HARM/ NHP,IHARM(5)                      DYN17658
0007      C1      CALCULATE TRIGONOMETRIC INTEGRALS       DYN17660
0008      PI02=1.570796                                  DYN17690
0009      ITH=0                                         DYN17700
0010      C
0009      DO 10 M=1,NH                                 DYN17710
0010          K=IHARM(M)                                DYN17720
0011      C
0011      DO 10 I=1,NH                                 DYN17728
0012          II=IHARM(I)                                DYN17730
0012

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C
0013      DO 10 J=1,NH                               DYN17748
0014          JJ=IHARM(J)                           DYN17750
0015          IPJ=II+JJ                            DYN17760
0016          IMJ=IABS(II-JJ)                         DYN17770
0017          IF (IPJ.NE.K.AND.IMJ.NE.K) GO TO 10    DYN17780
0018          ITH=ITH+1                            DYN17790
0019          IPM=II+K                            DYN17800
0020          IMM=IABS(II-K)                         DYN17810
0021          FONE=0.0                            DYN17820
0022          FTWO=0.0                            DYN17830
0023          FTHREE=0.0                           DYN17840
0024          FFOUR=0.0                           DYN17850
0025          IF (IPJ.EQ.K) FONE=1.0                 DYN17860
0026          IF (IPJ.FQ.K.AND.K.EQ.0) FONE=2.0       DYN17870
0027          IF (IMJ.EQ.K) FTWO=1.0                  DYN17880
0028          IF (IMJ.EQ.K.AND.K.EQ.0) FTWO=2.0       DYN17890
0029          IF (IPM.EQ.JJ) FTHREE=1.0                DYN17900
0030          IF (IPM.EQ.JJ.AND.JJ.EQ.0) FTHREE=2.0     DYN17910
0031          IF (IMM.EQ.JJ) FFOUR=1.0                 DYN17920
0032          IF (IMM.EQ.JJ.AND.JJ.EQ.0) FFOUR=2.0       DYN17930
0033          CCC(ITH)=PI02*(FONE+FTWO)              DYN17940
0034          SSC(ITH)=PI02*(-FONE+FTWO)              DYN17950
0035          CSS(ITH)=PI02*(-FTHREE+FFOUR)            DYN17960
0036          10 CONTINUE                           DYN17970
C
0037          PI04=0.785398                          DYN17980
0038          IFO=0.0                                DYN17983
C
0039          DO 20 L=1,NH                           DYN17990
0040              LL=IHARM(L)                         DYN18000
C
0041          DO 20 I=1,NH                           DYN18008
0042              II=IHARM(I)                         DYN18010
C
0043          DO 20 J=1,NH                           DYN18020
0044              JJ=IHARM(J)                         DYN18028
0045              IPJ=II+JJ                           DYN18030
0046              IMJ=IABS(II-JJ)                      DYN18040
C
0047          DO 20 K=1,NH                           DYN18048
0048              KK=IHARM(K)                         DYN18050
0049              KPL=KK+LL                           DYN18060
0050              KML=IABS(KK-LL)                      DYN18070
0051              IF (IPJ.NE.KPL.AND.IPJ.NE.KML.AND.IMJ. DYN18080
0052                  NE.KPL.AND.IMJ.NE.KML) GO TO 20    DYN18088
0053              IFO=IFO+1                           DYN18090
0054              FONE=0.0                            DYN18100

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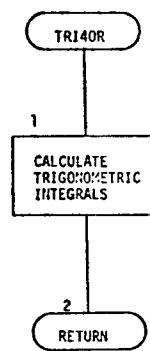
TRI40R

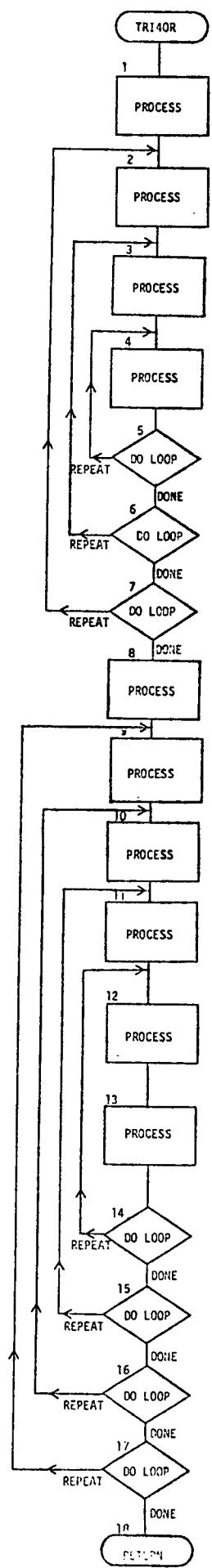
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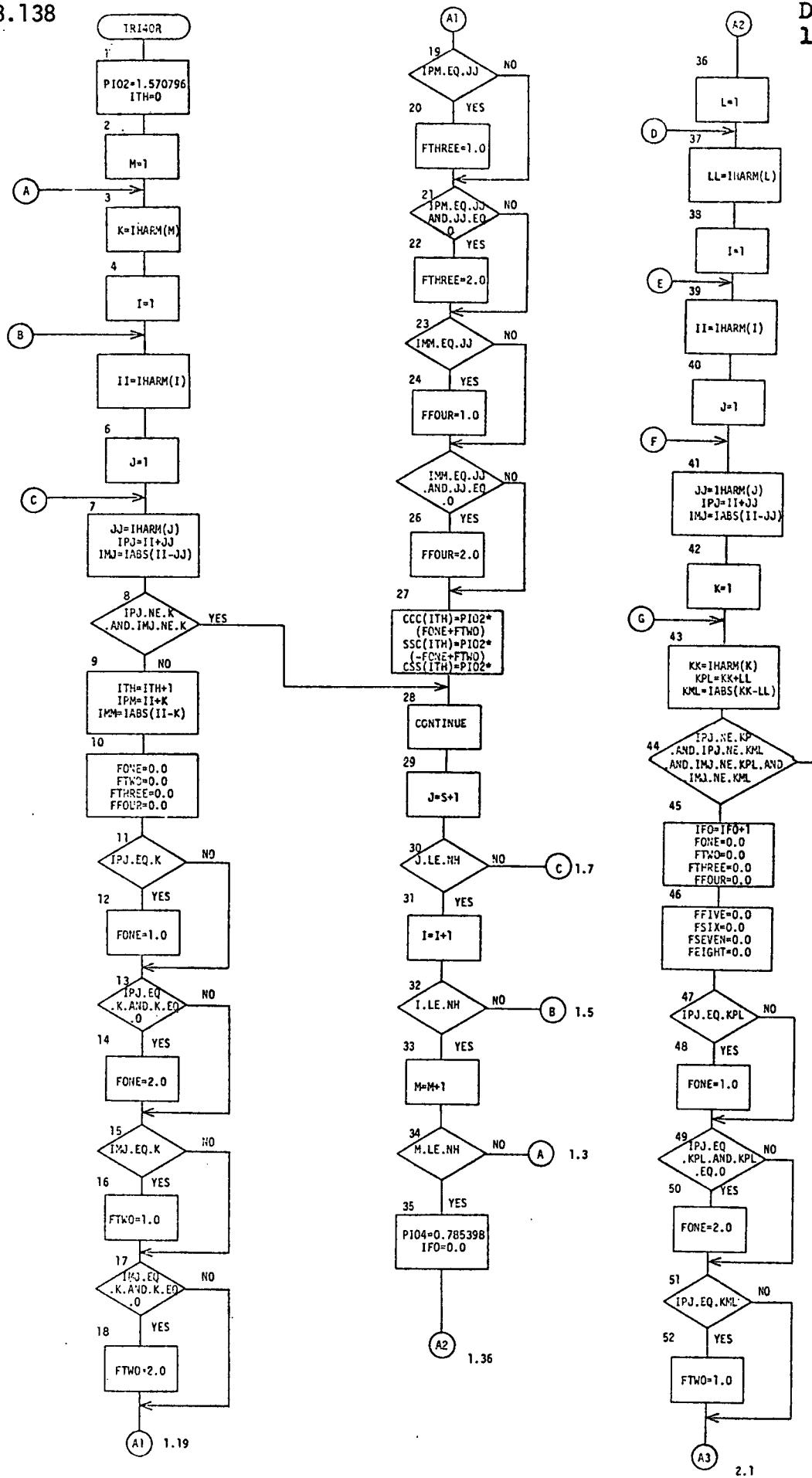
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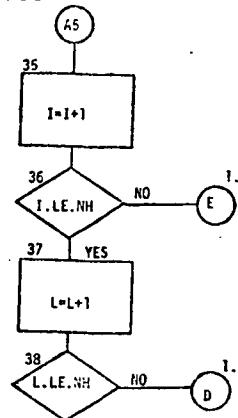
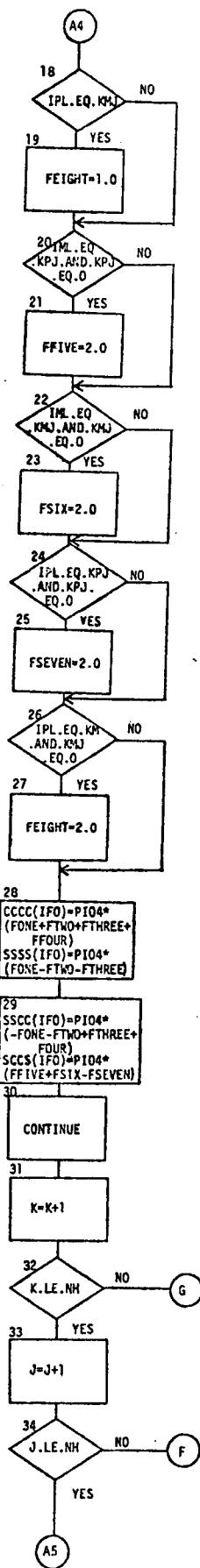
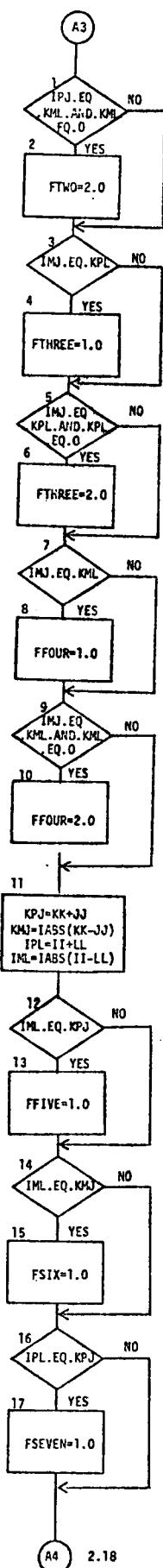
0054	FTWO=0.0	DYN18170
0055	FTHREE=0.0	DYN18180
0056	FFOUR=0.0	DYN18190
0057	FFIVE=0.0	DYN18200
0058	FSIX=0.0	DYN18210
0059	FSEVEN=0.0	DYN18220
0060	FEIGHT=0.0	DYN18230
0061	IF (IPJ.EQ.KPL) FONE=1.0	DYN18240
0062	IF (IPJ.EQ.KPL.AND.KPL.EQ.0) FONE=2.0	DYN18250
0063	IF (IPJ.EQ.KML) FTWO=1.0	DYN18260
0064	IF (IPJ.EQ.KML.AND.KML.EQ.0) FTWO=2.0	DYN18270
0065	IF (IMJ.EQ.KPL) FTHREE=1.0	DYN18280
0066	IF (IMJ.EQ.KPL.AND.KPL.EQ.0) FTHREE=2.0	DYN18290
0067	IF (IMJ.EQ.KML) FFOUR=1.0	DYN18300
0068	IF (IMJ.EQ.KML.AND.KML.EQ.0) FFOUR=2.0	DYN18310
0069	KPJ=KK+JJ	DYN18320
0070	KMJ=IABS(KK-JJ)	DYN18330
0071	IPL=II+LL	DYN18340
0072	IML=IABS(II-LL)	DYN18350
0073	IF (IML.EQ.KPJ) FFIVE=1.0	DYN18360
0074	IF (IML.EQ.KMJ) FSIX=1.0	DYN18370
0075	IF (IPL.EQ.KPJ) FSEVEN=1.0	DYN18380
0076	IF (IPL.EQ.KMJ) FEIGHT=1.0	DYN18390
0077	IF (IML.EQ.KPJ.AND.KPJ.EQ.0) FFIVE=2.0	DYN18400
0078	IF (IML.EQ.KMJ.AND.KMJ.EQ.0) FSIX=2.0	DYN18410
0079	IF (IPL.EQ.KPJ.AND.KPJ.EQ.0) FSEVEN=2.0	DYN18420
0080	IF (IPL.EQ.KMJ.AND.KMJ.EQ.0) FEIGHT=2.0	DYN18430
0081	CCCC(IF0)=PI04*(FONE+FTWO+FTHREE+FFOUR)	DYN18440
0082	SSSS(IF0)=PI04*(FONE-FTWO-FTHREE+FFOUR)	DYN18450
0083	SSCC(IF0)=PI04*(-FONE-FTWO+FTHREE+FFOUR)	DYN18460
0084	SCCS(IF0)=PI04*(FFIVE+FSIX-FSEVEN-FEIGHT)	DYN18470
0085	20 CONTINUE	DYN18480
C	RETURN	DYN18483
0086	END	DYN18490
0087		DYN18500





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VARIABLE CROSS REFERENCE

The variable cross reference listing gives an alphabetical listing of all variables from each routine along with the type of each variable, the dimension value for variable arrays, the statement number referencing the variable, and a corresponding letter value for each statement reference. The letter values for each reference are one of the following:

U - this indicates that the variable is simply being used in this particular statement reference. No values are being assigned to the variable in this particular reference.

D - a reference with a corresponding letter D indicates that the variable is defined in this statement reference. Examples of statements inwhich variables could be defined are COMMON, DIMENSION, all type statements, and subroutine definitions.

S - this indicates that the variable is set or given a value as in an assignment statement, input statement, etc...

P - the letter P stands for parameter
and indicates that the variable
appears in the argument list of
a subroutine CALL statement.

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
A	REAL*8		204	10850,U 10870,D 10950,S 11040,S 11040,S 11050,U 11050,S 11060,U 11060,S 11070,S 11070,U 11180,U 11180,S 11190,U 11190,S 11210,S 11210,U 11310,D 11410,S 11460,S 11460,U 11460,U 11470,U 11470,U 11470,S 11470,U 11470,U 11480,S 11480,U 11480,U 11480,U 11490,U 11490,U 11490,S 11490,U 11500,S 11500,U 11500,U 11510,U 11510,S 11510,U 11520,U 11520,S 11520,U 11520,U 11520,U 11520,U 11520,U 11520,U 11530,U 11530,U 11530,U 11530,U 11530,S 11530,U 11540,U 11540,S 11540,U 11550,S 11550,U 11550,U 11560,U 11560,S 11560,U 11570,S 11570,U 11570,U 11570,U 11570,U 11570,U 11570,U 11570,U 11570,U 11570,U 11580,U 11580,U 11590,U 11590,U 11590,U 11600,U 11600,U 11650,U 11660,U 11670,U 11680,U 11690,U 11700,U 11720,U 11730,U 11740,U 11750,U 11760,U 11770,U 11780,U 11790,U 11800,U 11810,U 11820,U 11830,U 11840,U 11850,U 11860,U 11870,U 11880,U 11890,U 11900,U 11910,U 11920,U 11930,U 11940,U 11950,U 11960,U 11970,U 11980,U 11990,U 12000,U 12010,U 12020,U 12030,U 12040,U 12050,U 12060,U 12070,U 12080,S 12090,S 12090,S 12090,S 12090,S 12090,S 12090,S 12090,S 12090,S 12710,S 12720,S 12730,S 12740,S 12750,S 12760,S 12770,S 12780,S 12790,S 12800,S 12810,S 12820,S 12830,S 12840,S 12850,S 12860,S 12870,S 12880,S 12890,S 12900,S 12910,S 12920,S 12930,S 12940,S 12950,S 12960,S 12970,S 12980,S 12990,S 13000,S 13010,S 13020,S 13030,S 13060,U 13070,U 13070,U 13080,U 13080,U 13080,U 13080,U 13120,U 13120,U 13120,U 13130,U 13130,U 13130,U 13130,U 13140,U 13150,U 13150,U 13160,U 13160,U 13160,U 13170,U 13170,U 13170,U 13180,U 13180,U 13180,U 13180,U 13240,U 13250,U 13250,U 13260,U 13260,U 13260,U 13270,U 13270,U 13270,U 13270,U 13320,U 13320,U 13320,U 13320,U 13330,U 13340,U 13340,U 13340,U 13340,U 13340,U 13350,U 13350,U 13360,U 13360,U 13360,U 13360,U 13360,U 13370,U 13370,U 13380,U 13380,U 13380,U 13380,U 13390,U 13390,U 13390,U 13390,U 13410,U 13410,U 13410,U 13420,U 13430,U 13430,U 13430,U 13430,U 13440,U 13440,U 13440,U 13450,U 13450,U 13450,U 13460,U 13460,U 13460,U 13460,U 13470,U 13470,U 13470,U 13470,U 13480,U 13480,U 13480,U 13480,U 13550,U
AAV	REAL*8			14590,S 14600,U 14620,U
AL	REAL*8		167	930,D 2650,S 2660,U 4310,S 4490,S 14900,D 15640,U 15650,U 15660,U 15670,U 15680,U 15690,U 15700,U 15710,U 15790,U 15800,U 15810,U 15820,U 15830,U 15840,U 15850,U 15860,U 16910,D 17280,U 17280,U 17290,U 17300,U 17300,U 17300,U 17310,U 17320,U 17320,U 17330,U 17330,U 17340,U 17340,U 17340,U 17350,U 17350,U 17350,U 17360,U 17360,U 17380,U 17380,U 17380,U 17380,U 17390,U 17390,U 17390,U 17400,U 17420,U 17420,U
ALPHK	REAL*8			4320,P 14870,U
ALS	REAL*8		50	1080,D 2890,S 2940,S 3020,U 7170,D 8820,U 8830,U 13710,D 14090,U 14150,U 16150,D 16890,D 17020,U 17050,U 17060,U 17090,U
ALSI1	REAL*8			2870,S 2890,U
ALT	REAL*8		50	1080,D 2900,S 2950,S 3020,U 7170,D 8820,U 8830,U 13710,D 14100,U 14180,U 16150,D 16890,D 17030,U 17040,U 17070,U 17080,U
ALTI1	REAL*8			2870,S 2900,U
AM1	REAL*8			11810,S 12230,U 12310,U 12330,U 12400,U 12430,U 12510,U 12550,U 12770,U
AM10	REAL*8			11650,S 11720,S 12200,U 12230,U 12280,U 12330,U 12370,U 12430,U 12480,U 12550,U 12600,U 12680,U
AM2	REAL*8			11800,S 12160,U 12170,U 12180,U 12190,U 12760,U

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED									
AM3	REAL*8			11790,S	12160,U	12170,U	12180,U	12190,U	12750,U				
AM4	REAL*8			11780,S	12160,U	12170,U	12180,U	12190,U	12740,U				
AM5	REAL*8			11790,S	11770,S	12220,U	12230,U	12300,U	12330,U	12390,U	12430,U	12500,U	12550,U
				12650,U	12730,U								
AM6	REAL*8			11690,S	11760,S	12120,U	12130,U	12140,U	12150,U	12640,U	12720,U		
AM7	REAL*8			11680,S	11750,S	12120,U	12130,U	12140,U	12150,U	12630,U	12710,U		
AM8	REAL*8			11670,S	11740,S	12210,U	12230,U	12290,U	12330,U	12380,U	12430,U	12490,U	12550,U
				12620,U	12700,U								
AM9	REAL*8			11660,S	11730,S	12080,U	12090,U	12100,U	12110,U	12610,U	12690,U		
ANG	REAL*8			15200,S	15220,U	16330,S	16350,U						
ARCL	REAL*8		50	1030,D	2720,S	2740,S	3030,U	6610,D	7140,D	13650,D	14140,U	14210,U	14210,U
				14590,U	14590,U	16880,D	17150,U	17150,U	17160,U	17160,U	17190,U	17190,U	17210,U
ARCLI	REAL*8			7380,S	7440,U	7450,U	7460,U	7470,U	7480,U	7490,U			
ARL	REAL*8			7330,S	7340,U	7350,U	7380,U	7900,U	8670,U				
AO	REAL*8			11820,S	12080,U	12120,U	12160,U	12200,S	12200,U	12230,U	12230,U	12240,U	12250,U
				12260,U	12270,U	12780,U							
A1	REAL*8			11830,S	12080,S	12080,U	12120,U	12160,U	12210,S	12210,S	12230,U	12230,U	12240,U
				12250,U	12260,U	12270,U	12790,U						
A10	REAL*8			11920,S	12330,U	12330,S	12420,U	12440,U	12530,U	12560,U	12880,U		
A11	REAL*8			11930,S	12100,U	12140,U	12180,U	12250,U	12340,U	12370,U	12370,S	12430,U	12430,U
				12450,U	12460,U	12890,U							
A12	REAL*8			11940,S	12100,U	12100,S	12140,U	12180,U	12250,U	12340,U	12380,S	12380,U	12430,U
				12430,U	12450,U	12460,U	12900,U						
A13	REAL*8			11950,S	12140,U	12140,S	12180,U	12250,U	12340,U	12390,S	12390,U	12430,U	12430,U
				12450,U	12460,U	12910,U							
A14	REAL*8			11960,S	12180,U	12180,S	12250,U	12340,U	12400,S	12400,U	12430,U	12430,U	12450,U
				12460,U	12920,U								
A15	REAL*8			11970,S	12250,U	12250,S	12340,U	12410,U	12410,S	12430,U	12430,U	12450,U	12460,U
				12930,U									
A16	REAL*8			11980,S	12340,U	12340,S	12420,S	12420,U	12440,U	12440,U	12450,U	12470,U	12540,U
A17	REAL*8			11990,S	12430,S	12430,U	12540,U	12560,U	12950,U				

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
A18	REAL*8		12000,S 12550,U	12110,U 12570,U 12960,U
A19	REAL*8		12010,S 12550,U	12110,S 12550,U 12570,U 12970,U
A2	REAL*8		11840,S 12260,U	12120,S 12270,U 12800,U
A20	REAL*8		12020,S 12550,U	12150,U 12570,U 12980,U
A21	REAL*8		12030,S 12570,U	12190,U 12990,U
A22	REAL*8		12040,S 13000,U	12260,U 12350,U 12450,U 12520,S 12520,U
A23	REAL*8		12050,S	12350,S 12450,U 12530,S 12530,U 12560,U 12560,U 12580,U 13010,U
A24	REAL*8		12060,S	12450,S 12540,U 12540,S 12560,U 12560,U 12580,U 13020,U
A25	REAL*8		12070,S	12550,S 12550,U 13030,U
A3	REAL*8		11850,S	12160,S 12160,U 12230,U 12230,U 12240,U 12250,U 12260,U 12270,U 12810,U
A4	REAL*8		11860,S	12230,U 12230,S 12320,U 12330,U 12410,U 12430,U 12520,U 12550,U 12820,U
A5	REAL*8		11870,S 12350,U	12090,U 12130,U 12170,U 12240,U 12280,S 12280,U 12330,U 12330,U 12340,U
A6	REAL*8		11880,S 12340,U	12090,U 12130,U 12170,U 12170,U 12240,U 12290,S 12290,U 12330,U 12330,U
A7	REAL*8		11890,S 12350,U	12130,U 12130,S 12170,U 12240,U 12300,U 12300,S 12330,U 12330,U 12340,U
A8	REAL*8		11900,S 12360,U	12170,S 12170,U 12240,U 12310,S 12310,U 12330,U 12330,U 12340,U 12350,U
A9	REAL*8		11910,S 12870,U	12240,S 12240,U 12320,S 12320,U 12330,U 12330,U 12340,U 12350,U 12360,U
BSL	REAL*8		14460,S	14550,U 14650,U
BSTL	REAL*8		14480,S	14550,U 14650,U
BSTMST	REAL*8	20	13720,S	14620,U 14630,U 14680,S
BSTRMS	REAL*8	20	13720,D	14600,U 14660,S

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED							
BSTRMT	REAL*8		20	13720,D	14610,U	14670,S					
BSTMNT	REAL*8		20	13720,D	14620,U	14700,S					
BSTU	REAL*8			14450,S	14550,U	14650,U					
BSU	REAL*8			14430,S	14540,U	14650,U					
BTL	REAL*8			14470,S	14550,U	14650,U					
BTTMST	REAL*8		20	13720,D	14600,U	14690,S					
BTU	REAL*8			14440,S	14540,U	14650,U					
CARD	REAL*8		20	130,D	140,S	300,S	310,U	330,U	330,U	390,U	400,U
CCC	REAL*8		125	7090,D	8100,U	8120,U	8150,U	8820,U	17600,D	17950,S	
CCCC	REAL*8		625	7100,D	8520,U	17610,D	18440,S				
CC1	REAL*8			5730,D	6640,D	6780,S	7150,D	8100,U	8120,U	8150,U	8170,U
				8820,U	13660,D	14340,U	14340,U			8510,U	8520,U
CC2	REAL*8			5730,D	6640,D	6790,S	7150,D	8120,U	8170,U	8540,U	8830,U
				14350,U						13660,D	14350,U
CES	REAL*8			7920,S	8100,S	8100,U	8210,U	8240,U	8260,U	8290,U	16970,D
				17060,S	17080,S	17280,U	17280,U	17280,U	17300,U	17300,U	17020,S
				17320,U	17330,U	17340,U	17340,U	17340,U	17350,U	17360,U	17320,U
				17380,U	17380,U	17390,U	17400,U	17400,U	17420,U	17420,U	17380,U
CEST	REAL*8			7940,S	8140,U	8140,S	8210,U	8230,U	8240,U	8260,U	8280,U
CET	REAL*8			7930,S	8120,S	8130,U	8230,U	8240,U	8280,U	8290,U	
CE13	REAL*8			7950,S	8150,S	8160,U	8210,U	8240,U	8260,U	8290,U	8690,S
				8860,U	8880,U	8890,U	8910,U				8820,U
CE23	REAL*8			7960,S	8170,S	8180,U	8210,U	8230,U	8240,U	8260,U	8280,U
				8830,U	8830,S	8860,U	8870,U	8880,U	8890,U	8900,U	8910,U
CE413	REAL*8			8340,S	8520,S	8520,S	8580,U	8600,U	8610,U	8630,U	
CE423	REAL*8			8350,S	8540,U	8540,S	8580,U	8590,U	8600,U	8610,U	8630,U
CHALS	REAL*8			930,D	14900,D	16910,D					
CHECK	REAL*8	8,8		930,D	2650,S	2660,U	4310,S	4490,S	14900,D	15910,U	16910,D
CHIS	REAL*8				13880,S	14160,U	14160,S	14370,U	14380,U		
CHIST	REAL*8				13900,S	14240,U	14240,S	14390,U			
CHIST1	REAL*8				14200,S	14240,U	14270,U				

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
CHIS1	REAL*8		14140,S	14160,U 14250,U
CHIS2	REAL*8		14150,S	14160,U 14250,U
CHIT	REAL*8		13890,S	14190,S 14190,U 14370,U 14380,U
CHIT1	REAL*8		14170,S	14190,U 14260,U
CHIT2	REAL*8		14180,S	14190,U 14260,U
CL2R	REAL*8		7570,S	7650,U
COMENT	REAL*8	20	1130,D	1150,S 1270,S 1280,U 1490,S 1510,U
CONST	REAL*8		50,D 14930,D	980,D 5710,D 6550,D 7070,D 9020,D 9830,D 10280,D 11270,D 13610,D 16120,D 16920,D 17620,D
CONSTF	REAL*8		1160,D	1200,S 3710,U 3980,S 4000,U 4060,U 4720,U
CONSTN	REAL*8	CONSTANT	1160,D	1170,S 3710,U 4000,U 4720,U
CCNST1	REAL*8	80 * S	1160,D	1170,S 1200,U
COPH	REAL*8		7350,S	7420,U 7450,U 7470,U 7550,U 7570,U
COSINE	REAL*8	51	1030,D	2720,S 2740,S 2740,S 6610,D 7140,D 13650,D 14120,U 14130,U 16880,D
COSM	REAL*8	50	1030,D	2790,S 6610,D 7140,D 13650,D 14210,U 14220,U 16880,D
CO2R	REAL*8		7550,S	7630,U
CS	REAL*8		6120,S 14190,U	6180,U 7090,D 13980,S 14040,U 14050,U 14070,U 14090,U 14100,U 14160,U 14270,U 17600,D
CSS	REAL*8	125	7090,D	8140,U 8170,U 8830,U 17600,D 17970,S
CS4	REAL*8		7100,D	17610,D
CTHIS	REAL*8		13910,S	14250,S 14250,U 14500,U
CTHIST	REAL*8		13930,S	14270,U 14270,S 14510,U
CTHIT	REAL*8		13920,S	14260,S 14260,U 14500,U
CYCLE	REAL*8		110,D	1100,D 1130,L,D
C1ST	REAL*8		14410,S	14430,U 14440,U 14450,U 14460,U 14470,U 14480,U
C12	REAL*8		15740,S	15750,S 15760,U 15770,U 15780,U
C2ST	REAL*8		14420,S	14430,U 14440,U 14450,U 14460,U 14470,U 14480,U
DABS	REAL*8		6330,U	

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
DATA	REAL*8	1170,S		
DCOS	REAL*8	279C,U	6120,U	1398C,U 1554C,U 1554C,U
DD1	REAL*8	5730,D	6640,D	6820,S 7150,D 13660,D 14370,U 14370,U
DD2	REAL*8	5730,D	6640,D	6830,S 7150,D 13660,D 14380,U 14380,U 14500,U 14500,U
DELTE	REAL*8	70,D 4910,U	580,U 4950,U	580,U 630,U 730,U 1010,D 1320,S 1780,U 2010,U 3430,U 6570,D 7190,D 9050,D 9150,U 9200,U 9860,D 13680,D 13790,U
DELTEP	REAL*8	100,D	1070,D	3280,S 3430,U 3510,U 5770,D 9060,D
DOUBLE	REAL*8	1160,D		
DRO	REAL*8	7310,S	7330,U	7340,U
DSIN	REAL*8	2800,U 16610,U	6110,U 16620,U	13990,U 14610,U 14630,U 15520,U 15520,U 15530,U 15530,U 16610,U
DSQRT	REAL*8	733C,U		
DTH	REAL*8	50,5,2	1080,D 4580,U 16740,S 17420,U	3310,S 3650,S 3660,S 3780,S 3780,U 3900,U 3900,S 3920,S 4450,S 4780,U 4780,S 4940,U 7170,D 13710,D 14020,U 14020,U 16150,D 16890,D 17270,U 17290,U 17310,U 17330,U 17350,U 17370,U 17390,U 17400,U
DTHT	REAL*8	14020,S	14150,U	14180,U
DTH1	REAL*8	5	1130,D	4420,S 4450,U
DT2	REAL*8		50,D 9350,U 16920,D	980,D 2010,S 5710,D 6550,D 7070,D 9020,D 9290,U 9330,U 9350,U 9400,U 9650,U 9830,D 10030,U 10280,D 11270,D 13610,D 14930,D 16120,D
DUM	REAL*8	1310	1140,D	1150,S 1590,S 1610,S 1640,S 1660,S 1690,S 1730,S
DZ	REAL*8		7320,S	7330,U 7330,U 7350,U
EES	REAL*8		6620,D	7110,D 13600,D
EPS	REAL*8		14300,S	14340,U 14350,U
EPST	REAL*8		14320,S	14360,U
EPT	REAL*8		14310,S	14340,U 14350,U
ES	REAL*8	5	6620,D	7110,D 7820,S 8150,U 8170,U 13600,D 14040,U
ESQ1	REAL*8		7500,S	7820,U 8210,U
ESQ3	REAL*8		7510,S	7820,U 8240,U

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
ESQ5	REAL*8			7520,S 7820,U 8260,U
ESQ7	REAL*8			7530,S 7820,U 8290,U
EST	REAL*8	5	6620,D	7110,D 7830,S 8160,U 8180,U 13600,D 14060,U
ESTQ1	REAL*8	5	7230,D	7660,S 7830,U 8210,U
ESTQ2	REAL*8		7480,S	7830,U 8230,U
ESTQ3	REAL*8	5	7230,D	7670,S 7830,U 8240,U
ESTQ5	REAL*8	5	7240,D	7680,S 7830,U 8260,U
ESTQ6	REAL*8		7490,S	7840,U 8260,U
ESTQ7	REAL*8	5	7240,D	7690,S 7840,U 8290,U
ESTU	REAL*8		13850,S	14060,U 14060,S 14320,U
ESU	REAL*8		13830,S	14040,S 14040,U 14300,U
ESUT	REAL*8		13940,S	14090,S 14090,U 14300,U
ET	REAL*8	5	6620,D	7110,D 7800,S 8150,U 8170,U 13600,D 14050,U
ETQ2	REAL*8	5	7240,D	7700,S 7710,U 7800,U 8230,U
ETQ3	REAL*8		7400,S	7800,U 8240,U
ETQ6	REAL*8	5	7240,D	7710,S 7800,U 8280,U
ETQ7	REAL*8		7410,S	7800,U 8290,U
ETU	REAL*8		13840,S	14050,S 14050,U 14310,U
ETUT	REAL*8		14100,U	14100,S 14310,U
E1	REAL*8	50	1020,D 17060,U	2680,S 3020,U 6600,D 6780,U 6820,U 7130,D 13640,D 16870,D 17020,U
E13	REAL*8	5	6620,D 8510,U 8520,U	7110,D 7850,S 8100,U 8100,U 8120,U 8120,U 8140,U 8150,U 8170,U
E13Q1	REAL*8		7440,S	7510,U 7850,U 8210,U 8580,U 8860,U
E13Q3	REAL*8		7450,S	7500,U 7850,U 8240,U 8600,U 8880,U
E13Q5	REAL*8		7460,S	7530,U 7850,U 8260,U 8610,U 8890,U
E13Q7	REAL*8		7470,S	7520,U 7850,U 8290,U 8630,U 8910,U
E13U	REAL*8		13860,S	14070,U 14070,S 14300,U 14320,U

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
FSEVEN	REAL*8		18220,S	18380,S 18420,S 18470,U
FSIX	REAL*8		18210,S	18370,S 18410,S 18470,U
FTHREE	REAL*8		17850,S	17910,S 17920,S 17970,U 18180,S 18280,S 18290,S 18440,U 18450,U 18460,U
FTWO	REAL*8		17840,S	17890,S 17900,S 17950,U 17960,U 18170,S 18260,S 18270,S 18440,U 18450,U 18460,U
F1	REAL*8		4160,S	4190,U 4230,U
F2	REAL*8		4160,S	4200,U 4230,U
F3	REAL*8		4160,S	4210,U 4230,U
F4	REAL*8		4160,S	4220,U 4230,U
G	REAL*8	50	1020,D	2690,S 3020,U 6600,D 6800,U 6810,U 7130,D 13640,D 16870,D
GCD	REAL*8		5730,D	6640,D 7150,D 13660,D
GEOM	REAL*8		1020,D	6600,D 7130,D 13640,D 16870,D
GG1	REAL*8		5730,D	6640,D 6800,S 7150,D 8140,U 8150,U 8170,U 8510,U 13660,D 14360,U
GG2	REAL*8		5730,D	6640,D 6810,S 7150,D 13660,D 14390,U 14510,U
HARM	REAL*8		90,D	1060,D 5760,D 7160,D 13670,D 14950,D 16160,D 16900,D 17640,D
HOUBQN	REAL*8		5870,U	9770,D
HOUBQ1	REAL*8		5860,U	8960,D

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED						
I	INTEGER	510,D 1610,U 1740,S 2040,U 2660,S 2690,S 2720,U 2740,U 2801,U 3030,U 3130,S 3281,U 3381,U 3570,S 3740,S 3870,S 4310,S 4740,U 4920,S 5310,U 6270,U 8120,U 8540,U 9240,U 9390,U 9650,U 10130,U 10480,U 10620,U 10940,S 11420,S 11720,U 11820,U 11920,U 12420,U 12640,U 12760,U 12860,U 12960,U 13510,U 14610,U 15780,U 16170,U 15310,U 15480,U 15890,U 16300,U 16540,U 17510,U	520,U 1640,U 1800,S 2140,U 2660,U 2690,U 2720,U 2750,U 3020,U 3030,U 3140,S 3290,U 3390,U 3580,U 3750,S 3890,U 4490,S 4750,S 4920,U 5000,S 6730,S 8140,U 8720,S 9300,S 9470,S 9670,S 10190,S 10480,U 10620,U 10950,U 11430,U 11730,U 11830,U 11930,U 12030,U 12650,U 12770,U 12790,U 12870,U 12970,U 13530,S 14620,U 15080,U 15170,U 15310,U 15480,U 15910,U 16390,U 16540,U 17510,U	1250,S 1640,S 1800,U 2180,U 2660,S 2690,S 2720,U 2750,S 3020,U 3030,S 3170,U 3290,S 3390,U 3590,U 3770,U 3890,U 4490,S 4770,U 4980,S 5000,S 6740,U 8150,U 8730,U 9310,U 9480,U 9680,U 10200,U 10540,S 10620,U 10920,S 11430,U 11730,U 11830,U 11930,U 12030,U 12650,U 12770,U 12790,U 12870,U 12970,U 13530,U 14620,U 15080,U 15170,U 15310,U 15480,U 15910,U 16390,U 16540,U 17510,U	1340,U 1660,U 1810,U 2550,S 2660,II 2690,U 2720,U 2770,S 3020,U 3030,U 3170,U 3320,U 3400,U 3610,S 3770,U 3890,U 4490,U 4770,U 4980,U 5000,U 6740,U 8160,U 8730,U 9330,U 9490,U 9680,S 10210,U 10550,U 10690,S 11040,U 11620,S 11750,U 11850,U 11950,U 12050,U 12690,U 12790,II 12800,U 12900,U 12990,U 13550,U 14630,U 15090,S 15170,U 15310,U 15480,U 15910,U 16390,U 16540,U 17520,S	1340,S 1660,S 1810,S 2560,U 2680,S 2690,U 2700,S 2740,U 2770,U 3020,U 3030,U 3170,S 3320,U 3410,U 3630,U 3780,U 3900,U 4490,S 4780,U 4990,U 5000,U 5970,U 7980,S 8170,U 8180,U 9180,S 9330,U 9500,U 9990,S 10420,S 10570,U 10700,U 11040,U 11650,U 11760,U 11860,U 11960,U 12050,U 12690,U 12790,U 12800,U 12900,U 13090,U 13820,S 14660,U 15090,U 15270,U 15320,U 15480,U 15910,U 16390,U 16540,S 17530,U	1370,S 1690,U 1930,S 2590,U 2680,S 2690,U 2700,S 2740,U 2770,U 3020,U 3080,S 3190,S 3320,S 3420,U 3640,U 3780,U 3910,U 4680,S 4780,U 4990,S 5000,U 5980,U 7990,U 8180,U 9190,U 9330,U 9500,U 10000,U 10440,U 10570,U 10700,U 11110,S 11660,U 11770,U 11870,U 11970,U 12070,U 12710,U 12810,U 12910,U 13010,U 13820,S 14670,U 15090,U 15270,U 15320,U 15490,U 15920,S 16400,S 16590,U 17530,U	1370,U 1690,S 1940,S 2650,U 2680,U 2700,U 2740,U 2780,S 2800,U 3080,S 3190,U 3320,U 3420,U 3660,U 3840,U 3920,U 4690,U 4900,U 5000,U 6070,U 8020,U 8370,S 9190,U 9350,U 9530,U 10030,U 10440,U 10570,U 10700,U 11120,U 11670,U 11780,U 11790,U 11890,U 11980,U 12660,U 12720,U 12820,U 12920,U 13030,U 14520,U 14680,U 14690,U 15090,U 15280,U 15430,U 15530,U 15940,U 16300,U 16530,U 16610,U 17480,S	1590,U 1730,S 1940,U 2650,S 2680,U 2710,U 2740,U 2780,S 2790,U 3020,U 3090,S 3270,U 3320,U 3430,U 3660,U 3840,U 4310,U 4730,S 4910,S 5000,U 6250,S 6260,U 8100,U 8510,U 9220,U 9350,U 9630,S 10030,U 10470,S 10610,S 10800,S 11400,U 11690,U 11800,U 11900,U 12000,U 12620,U 12740,U 12840,U 12940,U 13500,S 14600,U 14700,U 15170,U 15280,S 15430,U 15540,U 16300,S 16530,U 16620,U 17490,U	J-3.152
IABS	INTEGER	8670,U 8420,U 8460,U 8780,U 17780,U 17820,U 18080,U 18120,U 18330,U 18350,U								

VARIABLE	TYPE	INITIAL VALUF	DIMENSION	WHERE/HOW USED								
IB	INTEGER		3940,S 4720,U 17530,U	3950,S 4820,U 4820,S	3960,U 4830,U	4000,U 4870,U	4180,U 14870,U	4320,P 15930,U	4390,U 16100,U	4510,P 16720,U	4520,P 16850,U	4650,U 17230,U
IBP1	INTEGER		3300,U 4930,U 17290,U 17390,U	3300,S 4940,S 17300,U 17400,U	3310,S 4940,U 17310,U 17410,U	3310,U 16720,S 17320,U 17420,U	4390,S 16730,U 17330,U 17430,U	4450,U 16740,U 17340,U 17430,U	4460,U 17230,S 17350,U 17430,U	4580,U 17270,U 17360,U 17430,U	4580,U 17270,U 17370,U 17430,U	4930,S 17280,U 17380,U
IDCOE	INTEGER		60,D 13620,D	990,D 14940,D	3980,S 15050,U	5720,D 15390,U	6560,D 16130,D	7080,D 16930,D	9030,D 17630,D	9840,D 17630,D	10290,D 17630,D	11280,D
IDELF	INTEGER		60,D 11280,D	990,D 13620,D	3980,S 14940,D	4280,U 16130,D	5720,D 16930,D	6560,D 17630,D	7080,D 17630,D	9030,D 17630,D	9840,D 17630,D	10290,D
IDP	INTEGER		15330,S	15340,U	15340,U	16420,S	16430,U	16430,U				
IELM	INTEGER		2880,S 4300,S 4530,U 10590,U 15040,U 16730,U 17040,U 17060,U 17090,U 17160,U 17270,U 17370,U	2890,U 4320,P 4580,U 10600,U 15060,U 16740,U 17040,U 17070,U 17130,U 17190,U 17280,U 17380,U	2900,U 4430,S 4930,U 10620,U 15130,U 16850,U 17040,U 17070,U 17140,U 17190,U 17290,U 17390,U	2930,S 4450,U 4930,S 10640,U 15130,U 16850,U 17040,U 17070,U 17140,U 17190,U 17300,U 17400,U	2940,U 4460,U 4940,S 10660,U 15930,U 17120,U 17040,U 17070,U 17150,U 17190,U 17310,U 17400,U	2950,U 4480,S 4940,U 10670,U 16100,U 17020,U 17040,U 17070,U 17150,U 17190,U 17320,U 17420,U	3300,U 4510,P 10400,S 10670,U 16220,U 17020,U 17040,U 17070,U 17150,U 17210,U 17330,U 17420,U	3300,S 4520,P 10410,U 10540,U 16240,U 17030,U 17060,U 17080,U 17160,U 17210,U 17340,U 17530,U	3310,S 4570,S 10530,U 14870,U 16240,U 17030,U 17060,U 17090,U 17160,U 17210,U 17350,U 17530,U	3310,U 4580,U 10570,U 15030,U 16250,U 17030,U 17060,U 17090,U 17160,U 17270,U 17360,U 17530,U
IELM1	INTEGER		2870,S	2880,U	4420,S	4430,U	15080,S	15090,U	15170,S	15270,U	16300,S	16390,U
IELM2	INTEGER		2870,S 15170,S	2880,U 15270,U	2910,U 16220,S	4420,S 16240,U	4430,U 16300,S	4470,U 16390,U	15030,S	15040,U	15080,S	15090,U
IEQ	INTEGER		10130,S	10140,U								
IFLAG	INTEGER		2320,S 9130,S	2330,U 9460,U	2340,U 9590,S	2350,U	2360,U	2460,S	2470,U	2480,U	2490,U	2500,U
IFO	INTEGER		8320,S 18440,U	8490,S 18450,U	8490,U 18460,U	8520,U 18470,U	8520,U	8540,U	8540,U	18000,S	18150,S	18150,U

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED									
IH	INTEGER	2270,S 4080,S 4460,U 4940,U 7600,U 7680,U 7620,U 7861,U 10980,U 14020,U 14200,U 16740,U 17330,U 17430,U	2280,U 4090,U 4450,S 4940,S 7630,U 7690,U 7830,U 7870,U 10990,U 14120,U 15360,S 17240,U 17340,U 17430,U	2410,S 4140,U 4560,U 5830,S 5840,U 7640,U 7700,U 7830,U 8960,U 11240,U 14040,U 15370,U 17250,U 17350,U 17530,U	2420,U 4420,S 4580,U 5850,U 7650,U 7710,U 7830,U 9170,P 13960,S 14060,U 15760,U 17270,U 17360,U 17370,U	3040,S 4420,U 4640,S 5860,U 7660,U 7710,U 7840,U 9280,P 13970,U 14070,U 15770,U 17280,U 17380,U 17390,U	3060,U 4440,S 4650,U 5870,P 7660,U 7730,U 7850,U 9450,P 14010,U 14080,U 15930,U 17290,U 17390,U 17400,U	3300,U 4450,U 4660,U 5880,P 7670,U 7800,U 7860,U 9960,P 14010,U 14170,U 16450,S 17300,U 17400,U 17410,U	3310,S 4450,U 4660,U 5880,P 7670,U 7800,U 7860,U 9960,P 14010,U 14170,U 16450,S 17310,U 17420,U 17430,U	3310,C,U 4460,U 4930,U 7590,S 7680,U 7800,U 7860,U 10850,U 14020,U 14200,U 16730,U 17320,U 17420,U			
IHARM	INTEGER	5	90,D 4140,U 8120,U 13970,U 17760,U	10600,D 4560,U 8040,U 14950,D 18020,U	1370,U 4660,U 8360,U 15370,U 18040,U	1740,U 4900,U 8380,U 16160,D 18060,U	1800,U 5760,D 8400,U 16460,U 18100,U	2590,U 5840,U 8440,U 16960,D 18100,U	3060,U 6100,U 8710,U 17250,U 17640,D	3160,U 7160,D 8730,U 17640,D 17720,U	3180,U 7600,U 8750,U 17740,U 17740,U	3270,S 7970,U 13670,D 17740,U 17740,U	
IH1	INTEGER			4090,S	4180,U								
II	INTEGER			2570,S 8160,U 17810,U	2580,U 8380,S 17820,U	2590,U 8410,U 18040,S	2640,S 8420,U 18070,U	6950,S 8730,S 18080,U	6960,U 8760,U 18340,U	6990,U 8770,U 18350,U	7000,U 17740,S 17770,U	8020,S 17770,U 17780,U	8050,U
IID	INTEGER			10850,U	10940,U	10960,U	10990,U						
IMJ	INTEGER			8060,S 17900,U	8070,U 18080,S	8420,S 18130,U	8470,U 18130,U	8770,S 18280,U	8770,U 18290,U	8780,U 18300,U	17780,S 18310,U	17790,U	17890,U
IML	INTEGER			18350,S	18360,U	18370,U	18400,U	18410,U					
IMM	INTEGER			17820,S	17930,U	17940,U							
IN	INTEGER			4170,S	4180,U	4230,U							
INCRST	INTEGER			1320,S	1780,U	3350,U							
INODE	INTEGER			2310,S	2320,U	2450,S	2460,U						
INPUT	INTEGER			470,U	670,D	910,D	6400,U						
IN1	INTEGER			2340,S	2310,U	2440,S	2450,U	4160,S	4170,U				
IN2	INTEGER			2350,S	2310,U	2370,U	2440,S	2450,U	2510,U	4160,S	4170,U	4250,U	
IPJ	INTEGER			8050,S 17880,U	8070,U 18070,S	8410,S 18130,U	8470,U 18130,U	8760,S 18240,U	8760,U 18250,U	8780,U 18260,U	17770,S 18270,U	17790,U	17870,U
IPL	INTEGER			18340,S	18380,U	18390,U	18420,U	18430,U					
IPM	INTEGFR			17810,S	17910,U	17920,U							

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED									
IPRINT	INTEGER		80,D	1050,D	1320,S	1780,U	5750,D	5890,U	5890,U	6660,D	11290,D		
IQ	INTEGER		2560,S	2590,U	2590,U	2590,U	2590,U	2600,U	2600,U	2600,U	2600,U		
ION	INTEGER		2250,S	2260,U									
ION1	INTEGER		2250,S	2400,U									
IRSTRT	INTEGER		100,D 5770,D	500,U 9760,D	610,U 9210,U	1070,D 9320,U	1320,S	1370,U	1390,U	1780,U	2060,U	3220,U	
IT	INTEGER		5890,S	5910,U	6050,S	6110,U	6120,U	6230,U					
ITAM	INTEGER		110,D 5660,U 6220,U 11300,D	620,S 5820,U 6350,U 11440,U	630,U 5820,P 6390,U 13520,U	650,U 5870,U 6390,U 13580,U	690,P 5880,U 6530,U 13780,U	720,S 5890,U 6920,U	740,P 5890,U 6920,U	1100,D 5900,U 6920,U	4910,U 5910,U 6920,U	5020,U 5940,U 6930,P	
ITAM1	INTEGER		13780,S	13810,U									
ITCOE	INTEGER		1090,D	3980,S	4400,U	4500,U	7180,D						
ITELF	INTEGER		1090,D	1320,S	1790,U	2820,U	4340,U	7180,D	8650,U				
ITH	INTEGER		7890,S 8170,U 17960,U	8080,U 8660,S 17970,U	8080,S 8800,S	8100,U 8820,U	8100,U 8820,U	8120,U 8830,U	8120,U 17700,S	8140,U 17800,S	8150,U 17800,U	8150,U 17950,U	
ITP	INTEGER		100,D 9060,D	550,S	580,U	610,U	630,U	1070,D	3280,S	3350,U	3510,U	5770,D	
IT1	INTEGER		6390,S	6400,U									
IX	INTEGER		2590,S	2590,U	2590,U	2590,U	2600,U	2600,U	2600,U	2600,U	2600,U		
II	INTEGER		6130,S 6800,U 7050,U 8790,U 14000,U 14120,U 14210,U 14350,U 14580,U	6140,U 6810,U 7290,U 8790,U 14010,U 14130,U 14210,U 14370,U 14580,U	6760,S 6810,U 7300,U 8820,U 14010,U 14130,U 14210,U 14380,U 14590,U	6770,U 6820,U 7730,U 8820,U 14010,U 14140,U 14210,U 14410,U 14590,U	6770,U 6820,U 8100,U 8820,U 14020,U 14150,U 14220,U 14420,U 14600,U	6780,U 6830,U 8120,U 8830,U 14020,U 14170,U 14220,U 14500,U 14600,U	6780,U 6830,U 8120,U 8830,U 14020,U 14170,U 14220,U 14500,U 14600,U	6790,U 6870,P 8170,U 8830,U 14090,U 14180,U 14220,U 14530,U 14620,U	6790,U 6930,P 8510,U 8830,U 14100,U 14200,U 14220,U 14540,U 14640,U	6790,U 6930,P 8510,U 8830,U 14100,U 14200,U 14220,U 14570,U 14640,U	6800,U 6960,U 8790,U 13580,U 14120,U 14200,U 14220,U 14570,U 14640,U

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
J	INTEGER			1270,S 1270,U 1280,S 1280,U 1280,S 1490,S 1490,U 1510,U 1510,S 1600,U 1610,U 1680,S 1690,U 1700,S 1720,U 2650,U 2650,S 2660,S 2660,U 3620,S 3630,U 3640,U 3650,U 3660,U 3760,S 3770,U 3770,U 3780,U 3780,U 3880,S 3890,U 3890,U 3900,U 3900,U 3910,U 3920,U 4310,S 4310,U 4490,U 4490,S 4760,S 4770,U 4770,U 4780,U 4780,U 5980,S 5980,U 6160,S 6170,U 6180,U 6180,U 6180,U 6200,U 6200,U 6200,U 6270,U 6270,U 8030,S 8040,U 8100,U 8100,U 8100,U 8120,U 8120,U 8140,U 8150,U 8150,U 8160,U 8170,U 8170,U 8170,U 8390,S 8400,U 8520,U 8520,U 8540,U 8540,U 8740,S 8750,U 8750,U 8790,U 8790,U 8790,U 10430,S 10440,U 10460,S 10480,U 10560,S 10570,U 10590,S 10620,U 10640,U 10680,U 10680,S 10700,U 11010,S 11020,U 11040,U 11140,U 11150,U 11180,U 11190,U 11190,U 11210,U 11210,U 11210,U 11630,S 12270,U 12270,U 12270,U 12270,U 12270,U 12360,U 12360,U 12360,U 12360,U 12360,U 12360,U 12460,U 12460,U 12460,U 12460,U 12460,U 12460,U 12470,U 12470,U 12570,U 12570,U 12570,U 12570,U 12570,U 12570,U 12580,U 12580,U 15900,S 15910,U 15910,U 15930,S 15940,U 15940,U 17460,S 17470,U 17470,U 17500,S 17510,U 17510,U 17530,U 17540,U 17540,U
JH	INTEGER			3050,S 3060,U 3120,U 3160,U 3180,U 6080,S 6090,S 6100,U
JJ	INTEGER			6970,S 6980,U 6990,U 7000,U 8040,S 8050,U 8060,U 8400,S 8410,U 8420,U 8750,S 8760,U 8770,U 17760,S 17770,U 17780,U 17910,U 17920,U 17920,U 17930,U 17940,U 17940,U 18660,S 18670,U 18680,U 18320,U 18330,U
JM1	INTEGER			11150,S 11160,U
JUNK	INTEGER	20		1130,D 1450,S 1530,S 1740,S 3270,S 4900,U
J1	INTEGER			7290,S 7310,U 7320,U 7360,U
J11	INTEGER			7300,U 7310,U 7320,U 7360,U
K	INTEGER			1480,S 1580,S 1620,S 1630,U 1720,S 4180,S 4190,U 4200,U 4210,U 4220,U 4690,S 4700,U 4700,U 4700,U 4700,U 5970,S 5980,U 6140,S 6150,U 6180,U 6180,U 6200,U 6200,U 6260,S 6270,U 7600,S 7610,U 7970,S 8070,U 8070,U 8430,S 8440,U 8510,U 8520,U 8540,U 8710,S 8780,U 8780,U 10440,S 10450,U 10480,S 10490,U 10510,S 10510,U 10570,S 10580,U 10620,S 10630,U 10640,S 10650,U 10700,S 10710,U 10810,S 10820,U 11610,S 11620,U 11630,U 13090,S 13100,U 13110,U 13280,S 13290,U 13300,U 14000,S 14120,U 14120,U 14130,U 14130,U 14140,U 14140,U 14210,U 14210,U 14220,U 14220,U
KA	INTEGER			6960,S 6980,U
KEY	INTEGER			910,U 1180,U 3710,U 3950,U 11450,S 11640,U 12590,U 12660,S 15210,S 15220,U 15230,U 15240,U 15250,U 16340,S 16350,U 16360,U 16370,U
KEYRS	INTEGER			1380,S 1390,S 1500,U 1540,U 1750,S
KK	INTEGER			4650,S 4690,U 6980,S 6990,U 6990,U 7000,U 7730,S 7740,U 7750,U 7760,U 7770,U 7780,U 7790,U 8440,S 8450,U 8460,U 18100,S 18110,U 18120,U 18320,U 18330,U
KKP2	INTEGER			580,S 590,U 620,U 650,U 720,U
KK1	INTEGER			7740,U 7820,U 7830,U 7850,U 7860,U

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED								
KK2	INTEGER		7750,S	7800,U	7830,U	7860,U						
KK3	INTEGER		7760,S	7800,U	7820,U	7830,U	7850,U	7860,U				
KK5	INTEGER		7770,S	7820,U	7840,U	7850,U	7870,U					
KK6	INTEGER		7780,S	7800,U	7840,U	7870,U						
KK7	INTEGER		7790,S	7800,U	7820,U	7840,U	7850,U	7870,U				
KMJ	INTEGER		18330,S	18370,U	18390,U	18410,U	18410,U	18430,U	18430,U			
KML	INTEGER		18460,S 18310,U	8470,U 18310,U	8470,U	18120,S	18130,U	18130,U	18260,U	18270,U	18270,U	18300,U
KPJ	INTEGER		18320,S	18360,U	18380,U	18400,U	18400,U	18420,U	18420,U			
KPL	INTEGER		18450,S 18290,U	8470,U 18290,U	8470,U	18110,S	18130,U	18130,U	18240,U	18250,U	18250,U	18280,U
KY	INTEGER		5840,S 10360,U	5870,P 10780,U	5880,P	5950,U	8960,U	9430,P	9740,P	9770,U	10100,U	10250,U
KYP	INTEGER		4660,S 16660,U	4670,U 17250,S	15370,S 17260,U	15380,U 17440,U	15470,U	15560,U	15750,U	16460,S	16470,U	16510,U
L	INTEGER		8330,S 8610,U 11160,S 13130,S 13170,U 13320,U 13360,U 13380,U 13430,U 13460,U 13480,U	8360,U 8610,U 11180,U 13130,U 13170,U 13320,U 13360,U 13380,U 13430,U 13460,U 13480,U	8580,U 8610,U 11180,U 13130,U 13170,U 13320,U 13360,U 13380,U 13430,U 13460,U 13480,U	8580,U 8620,U 11190,U 13140,U 13180,U 13330,U 13360,U 13380,U 13430,U 13460,U 13480,U	8580,U 8620,U 13110,U 13150,U 13180,U 13340,U 13370,U 13390,U 13440,U 13470,U 13480,U	8590,U 8630,U 13120,U 13150,U 13180,U 13340,U 13370,U 13410,U 13440,U 13470,U 13480,U	8590,U 8630,U 13120,U 13150,U 13180,U 13340,U 13370,U 13410,U 13440,U 13470,U 13480,U	8600,U 8630,U 13120,U 13150,U 13180,U 13340,U 13370,U 13410,U 13440,U 13470,U 13480,U	8600,U 8630,U 13120,U 13150,U 13180,U 13340,U 13370,U 13410,U 13440,U 13470,U 13480,U	8600,U 8630,U 13120,U 13150,U 13180,U 13340,U 13370,U 13410,U 13440,U 13470,U 13480,U
LARGE	INTEGER		490,S	690,P	700,U	5660,U	6340,S					
LE	INTEGER		6330,U	15040,U	16240,U							
LK	INTEGER	204	970,D 1130,U	2180,S 10300,D	2190,S 10390,U	2200,S	3280,S	3330,S	3340,S	4910,U	9010,D	9820,D
LL	INTEGER		80,D 8360,S 18350,U	600,S 8450,U	610,S 8460,U	620,U 11290,D	1050,D 11440,U	5750,D 13520,U	5820,U 18620,S	5870,U 18110,U	5880,U 18120,U	6660,D 18340,U

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED								
M	INTEGER	7910,S 8240,U 8280,U 8870,U 9910,U 13260,U	7970,U 8240,U 8290,U 8870,U 8910,U 13260,U	7990,U 8250,U 8290,U 8880,U 8910,U 13260,U	8210,U 8260,U 8300,U 8880,U 10280,D 13230,S	8210,U 8260,U 8680,U 8890,U 13240,U 13270,S	8220,U 8260,U 8710,U 8890,U 13240,U 13270,U	8230,U 8270,U 8860,U 8890,U 13250,U 13270,U	8230,U 8280,U 8860,U 8900,U 13250,U 13270,U	8230,U 8280,U 8860,U 8900,U 13250,U 13270,U		
MATMUT	INTEGER		9170,U	9280,U	9960,U	10850,D						
MPRINT	INTEGER		290,S	340,U	370,S	380,S	380,U					
N	INTEGER	50,D 6150,U 9930,U 10640,U 13130,U 13150,U 13180,U 13270,U 13340,U 13360,U 13380,U 13430,U 13450,U 13470,U	980,D 6330,U 10000,U 13110,U 13130,U 13160,U 13180,U 13270,U 13340,U 13360,U 13380,U 13430,U 13450,U 13480,U	2280,S 6550,D 10550,S 10560,U 13120,U 13130,U 13160,U 13220,U 13300,S 13340,U 13370,U 13390,U 13430,U 13450,U 13480,U	2320,U 7070,D 10550,S 10660,S 13120,U 13130,U 13160,U 13240,U 13320,U 13340,U 13370,U 13390,U 13430,U 13450,U 13480,U	2460,U 9020,D 10560,U 10660,S 13120,U 13140,U 13170,U 13250,U 13320,U 13340,U 13370,U 13410,U 13430,U 13460,U 13610,D	5710,D 9190,U 10610,U 10640,U 13120,U 13150,U 13170,U 13260,U 13320,U 13350,U 13380,U 13410,U 13440,U 13470,U 14930,D	5860,S 9310,U 10640,U 10640,U 13120,U 13150,U 13170,U 13260,U 13320,U 13360,U 13380,U 13410,U 13450,U 13470,U 16120,D	5970,U 9480,U 10640,U 10640,U 13120,U 13150,U 13170,U 13260,U 13320,U 13360,U 13380,U 13410,U 13450,U 13470,U 16920,D	6090,S 9640,U 9830,D 10640,U 13130,U 13150,U 13180,U 13270,U 13330,U 13360,U 13380,U 13410,U 13450,U 13470,U 16580,U		
NA	INTEGER		11600,S	11630,S	11630,S	11640,U						
NCARD	INTEGER		270,S	310,U	320,U	320,S	410,U					
NCARDS	INTEGER		1230,S	1240,U	1250,U	1450,S	1460,U	1480,U				
NCASE	INTEGER		220,S 750,U	280,U —	280,S	350,U	420,S	420,U	430,U	460,S	480,S	480,U
NCASES	INTEGER		200,S	210,U	430,U	750,U						
NCF	INTEGER		3980,S	4070,U								
NCF1	INTEGER		4110,S	4120,U								
NCLCST	INTEGER		1040,D	1330,S	1790,U	5740,D	6650,D	6930,U	13630,D			
NCLOSE	INTEGER		970,D	1320,S	1790,U	9010,D	9820,D	10100,U	10300,D	10360,U		
ND	INTEGER		120,D 1370,U 4160,U	200,S 1790,U 4420,U	260,U 2110,U 14970,D	330,U 2160,U 15080,U	440,U 2250,U 15170,U	1110,D 2300,U 16170,D	1230,U 2440,U 16300,U	1270,U 2870,U 16300,U	1320,U 3980,U 4110,U	1340,U
NDIRCT	INTEGER		2160,S	2170,U	2160,U							
NDP	INTEGER		15170,U 16300,S	15170,S 16300,U	15180,U 16310,U	15190,U 16320,U	15280,U 16330,U	15290,U 16400,U	15300,U 16410,U	15310,U 16500,U	15420,U 16520,U	15440,U 16580,U

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED							
NDPP2	INTEGER	15300,S	15320,U								
NDP1	INTEGER	15420,S	15430,U								
NDP2	INTEGER	15180,S	15210,U	16310,S 16340,U							
ND2	INTEGER	15290,S	15320,U	15330,U 16410,S 16420,U							
NELEMS	INTEGER	50,D 1960,U 2710,U 43,0,U 7075,D 13280,U	980,D 1990,U 2640,U 2780,U 4470,U 9020,D 13290,U	1530,S 2640,U 2910,U 4480,U 9830,D 10280,U	1580,U 2680,U 2930,U 4570,U 10660,D 10280,U	1600,U 2680,U 3030,U 4750,U 10660,D 10280,U	1620,U 2680,U 3300,U 4930,U 11270,D 16120,U	1630,U 2690,U 3310,U 4940,U 11610,U 16920,D	1680,U 2690,U 3610,U 4940,U 13090,U 17140,U	1710,U 2690,U 3750,U 5710,D 13220,U 17620,D	1790,U 2700,U 3870,U 6760,U 13230,U
NEQ	INTEGER	50,D 5860,U 9280,P 10400,U 10590,U 16120,D	980,D 6060,U 9300,P 10470,U 10670,U 16020,D	1970,S 6000,U 9470,U 10430,U 10720,D 17530,U	1980,U 6550,D 9630,D 10460,U 11270,D 17620,D	2280,U 6960,U 9830,D 10470,U 11420,U 17620,D	2420,U 7070,D 9920,U 10500,U 10500,U 10500,U	2560,U 7730,U 9960,P 10500,U 10500,U 10500,U	4180,U 9020,D 9990,U 10500,U 10500,U 14000,U	4650,U 9170,P 10190,U 10500,U 10540,U 14930,D	5710,D 9180,U 10390,U 10540,U 10590,U 15930,U
NEQT	INTEGER	50,D 3570,U 4740,U 9020,D 16120,D	510,U 3590,U 4890,U 9240,U 16920,D	980,D 3730,U 4980,U 9360,U 17530,U	1980,S 3740,U 5000,U 9830,D 17620,D	2020,U 3930,U 5000,U 10010,U 17620,D	3260,U 3840,U 5000,U 10280,D 17620,D	3320,U 3850,U 5710,D 11270,D 17730,U	3320,U 4180,U 6550,D 13610,D 17750,U	3320,U 4650,U 6730,U 14930,D 15930,U	3370,U 4730,U 7070,D 15930,U
NF	INTEGER	10990,S	11040,U	11050,U 11060,U 11060,U							
NFF	INTEGER	11130,S	11180,U	11190,U 11210,U							
NH	INTEGER	50,D 2270,U 3880,U 4940,U 7910,U 9120,D 16120,D 18650,U	980,D 2410,U 4080,U 5710,D 8010,U 8930,D 16450,U 18090,U	1370,U 2550,U 4420,U 5930,U 8030,U 8330,U 10280,D 16920,D	1370,S 3050,U 4440,U 6100,U 8370,U 8390,U 11270,D 17240,U	1740,U 3270,U 4550,U 6010,U 8370,U 8390,U 13610,D 17620,D	1740,S 3270,S 4640,U 6080,U 8390,U 13960,U 14930,D 17710,U	1800,U 3300,U 4760,U 6550,D 8430,U 14930,D 15080,U 17730,U	1800,U 3310,U 4900,U 6950,U 8680,U 14930,D 15090,U 17750,U	1980,U 3620,U 4910,U 7070,D 8720,U 15090,U 15360,U 18010,U	2000,U 3760,U 4930,U 7540,U 8740,U 15360,U 18630,U
NHNS	INTEGER	50,D 13610,D	980,D 14930,D	2000,S 15120,D							
NHP	INTEGER	90,D 16900,D	1060,D 17640,D	1530,S 1700,U							
NI	INTEGER	11120,S	11130,U	11180,U 11190,U							
NIX	INTEGER	10280,D									
NK	INTEGER	10980,S	11000,U	11050,U 11060,U							
NKK	INTEGER	11090,S	11170,U	11170,S 11180,U 11190,U							
				11200,S 11200,S 11210,U							

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED								
NLTERM	INTEGER		740,U	3360,U	5820,U	6530,D						
NLTRMS	INTEGER		6630,D	7120,D								
NM1	INTEGER		11100,S	11110,U								
NN	INTEGER		50,D 7070,D 10570,U 13610,D	980,D 9020,D 10620,U 14930,D	3120,S 9390,U 10640,U 16120,D	3130,U 9530,U 10700,U 16920,D	3140,U 9680,U 10960,S 17620,D	3170,U 9830,D 10970,U 16920,D	3190,U 10280,D 11100,U 17620,D	5710,D 10440,U 11270,D 16920,D	5850,S 10480,U 11400,U 17620,D	6550,D 10500,U 13540,U
NNODES	INTEGER		50,D 4680,U 11800,D	980,D 5710,D 11270,D	1960,S 5960,U 13610,D	1970,U 6130,U 14930,D	2370,U 6250,U 16120,D	2510,U 6550,D 16920,D	2570,U 7070,D 17620,D	2770,U 9020,D 17620,D	2770,U 9830,D 17620,D	4250,U 10280,U
NNPI	INTEGER		9390,S 9690,U	9400,U 9700,U	9400,U 9700,U	9400,U 9700,U	9530,S 9710,U	9540,U 11400,S	9550,U 11410,U	9550,U 13540,S	9560,U 13550,S	9680,S
NODRE	INTEGER		10690,S	10100,S	10100,U	10110,U	10120,U	10350,S	10360,S	10360,U	10370,U	10380,U
NODRES	INTEGER		970,D 3340,U	2110,S 4910,U	2120,U 4910,U	2130,U 9710,D	2140,U 9820,D	2190,U 10090,U	2200,U 10300,U	3280,U 10350,D	3280,S 10350,D	3330,U
NOIT	INTEGER		80,D	590,S	1050,D	1350,S	5750,D	5900,U	6660,D	6930,U	11290,D	
NP	INTEGER		2160,S	2170,U	2180,U							
NPI	INTEGER		9190,S 9330,U 9650,U 10010,U	9200,U 9350,U 9930,S 10010,U	9200,U 9350,U 9940,U 10040,U	9220,U 9360,U 9940,U 10040,U	9240,U 9480,S 9940,U 10050,U	9240,U 9490,U 9940,U 10050,U	9240,U 9640,S 10000,S 10060,U	9250,U 9650,U 10010,U 10060,U	9310,S 9650,U 10010,U 10200,S	9650,U 10010,U 10010,U 10210,U
NPK	INTEGER		6150,S	6180,U	6200,U							
NPRNIT	INTEGER		100,D	1070,D	1330,S	1780,U	5770,D	6390,U	6390,U	9060,D		
NPRNMS	INTEGER		1330,S	1800,U	3150,U							
NPRNT	INTEGER		100,D	1070,D	1330,S	1780,U	5770,D	6380,U	6400,U	9060,D		
NPRNTF	INTEGER		60,D 9840,D	990,D 10290,D	1330,S 11280,D	1790,U 13620,D	4010,U 14940,D	4600,U 16130,D	5720,D 16930,D	6560,D 17630,D	7080,D	9030,D
NPRNTH	INTEGER		1090,D	1330,S	1790,U	4540,U	7180,D					
NPRNTL	INTEGER		60,D 9030,D 15310,U	990,D 9840,D 16130,D	1330,S 10290,D 16250,U	1790,U 11280,D 16390,U	4010,U 13620,D 16930,D	4130,U 14940,D 17630,D	4230,U 15060,U 17630,D	5720,D 15090,U 15130,U	6560,D 15130,U 15270,U	7080,D
NPRNTQ	INTEGER		50,D 10280,D	990,D 11270,D	1320,S 13610,D	1780,U 14930,D	5710,D 16120,D	5920,U 16920,D	6550,D 17620,D	7070,D	9020,D	9830,D

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
NPESTR	INTEGER	9430,U	9740,U	10250,D
NS	INTEGER	120,D 14970,D	200,S 16170,D	1110,D 1790,U 2630,U 2660,U 4290,U 4310,U 4380,U 4490,U
NSIZE	INTEGER	50,D 3140,U 9670,U 17620,D	980,D 3170,U 9830,D	1710,S 3190,U 10280,D 1730,U 5710,D 11270,D 1990,S 5850,U 11390,U 2000,U 6550,D 13530,U 3080,U 7070,D 13610,D 3090,U 9020,D 14930,D 3120,U 9380,U 16120,D 3130,U 9520,U 16920,D
NSTRSS	INTEGER	1040,D	1330,S	1790,U 5740,D 6650,D 6910,U 6920,U 6920,U 6930,U 13630,D
NT	INTEGER	120,D 1660,U 3080,U 4930,U	1110,D 1690,U 3190,U 5000,U	1230,S 1730,U 3130,U 10970,S 1440,U 1740,U 3140,U 10980,U 1450,U 1790,U 3270,U 14970,D 1490,U 2650,U 3280,U 16170,D 1530,U 2680,U 3300,U 3320,U 1590,U 2720,U 3300,U 4900,U 1610,U 2740,U 4910,U 1640,U 2770,U 4910,U
NTF	INTEGER	3260,S	3290,U	4890,S 4920,U
NTHETA	INTEGER	1040,D 12820,U	1340,S	1340,U 1810,U 1810,U 1930,U 5740,D 6050,U 6650,D 13630,D
NW	INTEGER	11270,D		
P	REAL*8	74	14890,D 15570,U	15080,S 15760,U 15170,S 16140,D 16300,S 16360,U 16360,S 16390,U 15230,U 16360,U 15230,U 16390,U 15270,U 16390,U 15310,U 16530,U 15480,U 16610,U 15520,U 16670,U
PAV	REAL*8		14580,S	14610,U 14630,U
PH	REAL*8	50	1030,D 14580,U	2720,S 16880,D 2740,S 2790,U 2800,U 3030,U 6610,D 7140,D 13650,D 7140,D 13650,D 14580,U
PHP	REAL*8	50	1030,D 17150,U	2720,S 17160,U 2740,S 17160,U 3030,U 17190,U 6610,D 17190,U 7140,D 17210,U 13650,D 17210,U 14220,U 17210,U 16880,D 17150,U
PHPP	REAL*8		17170,S	17190,S 17210,S 17360,U 17390,U
PHPP1	REAL*8		17150,S	17170,U
PHPP2	REAL*8		17160,S	17170,U
PI	REAL*8		1910,S 16560,U	1920,U 16630,U 15020,S 16640,U 15570,U 1710,S 1720,U 1740,U 15580,U 17060,U 15760,U 17080,U 15770,U 17060,U 15780,U 17080,U 16230,S 16550,U
PINT	REAL*8		15480,S 16530,S 16730,U	15520,S 16530,U 16550,U 15570,S 16550,S 15610,S 16610,U 15680,U 16610,S 15690,U 16630,S 15830,U 16630,U 15840,U 16670,S 16700,U
PI02	REAL*8		17690,S	17950,U 17960,U 17970,U
PI04	REAL*8		17990,S	18440,U 18450,U 18460,U 18470,U

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
PRINT	REAL*8		80,D	1050,D 5750,D 6660,D 11290,D
PS	PEAL*8		1000,D	9040,D 9850,D
Q	REAL*8	8	14960,D 15410,S 15640,U 15640,S 15650,S 15650,U 15660,S 15660,U 15670,S 15670,U 15680,S 15680,U 15690,S 15690,U 15700,U 15700,S 15710,S 15710,U 15790,S 15790,U 15810,S 15820,S 15830,S 15840,S 15850,S 15860,S 15910,U 16960,D 17280,S 17300,S 17320,S 17340,S 17360,S 17380,S 17400,S 17420,S 17470,S 17510,U	
QB3	REAL*8		14120,S	14200,U 14210,U
QR7	RFAL*8		14130,S	14200,U 14210,U
QDC1	REAL*8		4970,S	4990,U
QDC2	REAL*8		4960,S	4990,U
QDC3	REAL*8		4950,S	4960,U 4970,U 4990,U
QLLOAD	REAL*8	204	940,D 5680,D 6070,S 6180,U 6180,S 6200,S 6200,U 6270,U 8980,D 9280,P 9330,U 9330,S 9350,S 9350,U 9490,U 9500,S 9650,U 9790,D 9960,P 10030,S 10030,U 10140,S 10210,U	
QLLOAD1	REAL*8	1020	9070,D	9170,P 9220,U 9220,S 9240,S 9240,U 9330,S 9350,S 9500,S
QN	REAL*8	1020	30,D 140,S 950,D 2030,S 2330,S 2340,S 2350,S 2360,S 2590,U 2590,U 2590,U 2590,U 3320,S 3380,U 3390,U 4990,U 5000,U 5690,D 5690,D 5980,U 6180,U 6200,U 6330,U 6580,D 7200,D 7800,U 7800,U 7800,U 7800,U 7820,U 7820,U 7820,U 7820,U 7830,U 7830,U 7830,U 7840,U 7840,U 7840,U 7840,U 7850,U 7850,U 7850,U 7850,U 7860,U 7860,U 7860,U 7870,U 7870,U 7870,U 7870,U 8990,D 9200,U 9200,S 9280,P 9490,S 9650,U 9800,D 9940,U 10050,U 10210,S 13690,D 14120,U 14120,U 14130,U 14140,U 14140,U 14210,U 14210,U 14220,U 14220,U 14910,D 16940,D	
QN1	REAL*8	1020	30,D 950,D 2040,S 2470,S 2480,S 2490,S 2500,S 2600,U 2600,U 2600,U 2600,U 3320,S 3390,U 3400,S 4990,U 5690,D 6580,D 6580,D 7200,D 8990,D 9650,S 9200,U 9650,U 9800,D 10040,S 13690,D 14910,D 16940,D 10050,S 13690,D 14910,D 16940,D	
QN2	REAL*8	1020	30,D 950,D 4990,U 5690,D 6580,D 7200,D 8990,D 9650,S 9800,D 9940,U	
QP	REAL*8	1020	30,D 950,D 3420,U 3430,S 3430,U 3430,U 4990,S 5000,U 5690,D 6580,D 6740,S 6990,S 6990,U 7000,S 7200,D 8990,D 9350,U 9800,D 10010,U 10060,U 13690,D 14910,D 16940,D	
QPR	REAL*8	8,5	6630,D 6990,U 7000,U 7120,D 7990,S 8210,S 8210,U 8230,S 8230,U 8240,S 8250,U 8260,S 8260,U 8280,U 8280,S 8290,S 8300,U 8580,U 8580,S 8590,U 8590,S 8610,S 8610,U 8610,S 8620,U 8620,S 8630,S 8630,U 8860,U 8860,S 8870,U 8870,S 8880,S 8880,U 8890,S 8890,U 8900,U 8900,S 8910,U	
QPRIME	REAL*8		6870,U	7050,D

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED					
QP1	REAL*8	1020	30,D 8990,D	520,S 9240,U 9800,D 10010,U 10060,S 13690,D 14910,D 16940,D 5000,U 5690,D 6580,D 7200,D					
QQ	RFAL*8	8	14960,D	15890,S 15910,S 15910,U 15940,U 16960,D 17490,S 17510,S 17510,U 17540,U					
QS	RFAL*8		30,D 950,D	5690,D 6580,D 7200,D 8990,D 9800,D 13690,D 14910,D 16940,D					
QSS	REAL*8		10010,S	10030,U					
QUES	RFAL*8		14960,D	16960,D					
Q1	REAL*8		2300,S	2330,U 2440,S 2470,U					
Q2	REAL*8		2300,S	2340,U 2440,S 2480,U					
Q3	REAL*8		2300,S	2350,U 2440,S 2490,U					
Q4	REAL*8		2300,S	2360,U 2440,S 2500,U					
R	REAL*8	50	1030,D 11580,U 12270,U 12360,U 12470,U 13060,U 13080,U 13130,U 13150,U 13180,U 13260,S 13270,U 13320,U 13360,U 13380,S 13410,U 13450,U 13470,U 14220,U 15090,U 16140,D	2720,S 2740,S 3020,U 6610,D 11590,U 12270,S 12360,S 12470,S 13060,S 13080,U 13130,S 13150,U 13180,U 13240,U 13270,U 13320,U 13360,U 13380,U 13410,U 13430,S 13450,U 13470,U 14570,U 15240,S 16300,S	11310,D 11590,S 12270,U 12460,U 12570,U 13070,S 13120,U 13140,U 13170,U 13240,S 13270,S 13340,S 13360,U 13380,U 13410,S 13430,U 13450,U 13480,U 14600,U 15270,U 16370,U	7140,D 11600,U 12270,U 12460,U 12570,U 13070,U 13120,U 13150,U 13170,U 13250,U 13270,U 13340,U 13370,U 13390,U 13430,U 13460,U 13480,U 14620,U 15310,U 16390,U	11430,S 11600,S 12360,U 12460,S 12570,U 13080,S 13080,U 13120,S 13150,U 13170,U 13260,U 13320,S 13320,U 13380,U 13410,U 13430,U 13470,S 13470,U 14170,U 14890,D 15530,U 16620,U	11580,S 11600,U 12360,U 12460,U 12580,U 13080,U 13080,C 13120,U 13150,U 13170,U 13260,U 13320,U 13350,U 13380,U 13410,U 13430,U 13470,U 14210,U 14890,D 15580,U 16680,U	11580,U 11600,U 12360,U 12460,U 12580,U 13080,U 13080,C 13120,U 13150,U 13170,U 13260,U 13320,U 13360,S 13380,U 13410,U 13430,U 13470,U 14210,U 14890,D 15580,U 16680,D
RAD	REAL*8		1920,S	1940,U					
RAV	REAL*8		14570,S	14600,U 14620,U					
RESTART	REAL*8		100,D	1070,D 5770,D 9060,D					
RINT	REAL*8		15490,S 15810,U 16640,S	15530,S 15820,U 16680,S 15580,S 15820,S 16710,S	15620,S 16490,S 16710,U 15640,U 16540,U 16740,U	15640,U 16540,U 16740,U 15660,U 16560,U 16680,U	15660,U 16560,U 16680,U 15670,U 16560,S 16620,S	15670,U 16560,S 16620,S 15770,S 16620,U	15790,S 16620,U
RL	REAL*8		8670,S	8860,U 8870,U 8880,U 8890,U 8900,U 8910,U					

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
RM	REAL*8		7360,S	7370,U 7900,U 8670,U
RSL	REAL*8		7900,S 8610,U	8210,U 8620,U 8230,U 8630,U 8250,U 8260,U 8280,U 8300,U 8580,U 8590,U 8600,U
RSTRNT	REAL*8		970,D	9910,D 9820,D 10300,D
RZ	REAL*8		1120,D	7220,D
RO	REAL*8	51	1120,D	2770,S 7220,D 7310,U 7310,U 7360,U 7360,U
R2I	REAL*8		7370,S 7770,U	7400,U 7410,U 7420,U 7480,U 7490,U 7550,U 7560,U 7570,U 7580,U
S	REAL*8	74	14890,D 16140,D	15080,S 15090,U 15170,S 15250,U 15250,S 15270,U 15310,U 15540,U 15780,U
SCCS	REAL*8	625	7100,D	8540,U 17610,D 18470,U
SETUP	REAL*8		690,U	5660,D
SHRS	REAL*8		14610,S	14640,U
SHRT	REAL*8		14620,S	14650,U
SINE	REAL*8	51	1020,D	2720,S 2740,S 2740,S 6600,D 7130,D 13640,D 14120,U 14130,U 16870,D
SINM	REAL*8	50	1030,D	2800,S 6610,D 7140,D 13650,D 14170,U 14200,U 14200,U 14220,U 16880,D
SINT	REAL*8		15500,S	15540,S 15590,S 15630,S 15700,U 15710,U 15780,S 15850,U 15860,U
SIPH	REAL*8		7340,S	7440,U 7460,U 7480,U 7490,U 7560,U 7580,U
SLVEEQ	REAL*8		940,D	5680,D 8980,D 9790,D 10270,D 11260,D
SL2R	REAL*8		7560,S	7640,U
SN	REAL*8		6110,S	6200,U 13990,S 14060,U 14080,U 14240,U 14250,U 14260,U
SOLVEQ	REAL*8		9450,U	10180,U 11240,D
SC2R	REAL*8		7580,S	7620,U
SPA	REAL*8	6550	11260,D	11410,U 13550,S
SPR	REAL*8	204	11260,D	11430,U 13510,S
SSC	REAL*8	125	7090,D	8100,U 8120,U 8150,U 17600,D 17960,S
SSCC	REAL*8	625	7100,D	8520,U 17610,D 18460,S
SSSS	REAL*8	625	7100,D	8540,U 17610,D 18450,S

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
STIFM	REAL*8		6550	10270,D 10450,S 10490,S 10510,S 10580,S 10630,S 10650,S 10710,S 10790,S 10820,S 10850,U 10870,D 11040,U 11050,U 11060,U 11060,U 11070,U 11070,U 11070,U 11180,U 11190,U 11210,U
STRESS	REAL*8			6930,U 13580,D
STRMS	REAL*8			14370,S 14430,U 14460,U 14540,U 14600,U 14640,U 14660,U
STRMST	REAL*8			14390,S 14450,U 14480,U 14540,U 14620,U 14630,U 14640,U 14680,U
STRMT	REAL*8			14380,S 14440,U 14470,U 14540,U 14610,U 14640,U 14670,U
STRNS	REAL*8			14340,S 14430,U 14460,U 14540,U 14640,U
STRNST	REAL*8			14300,S 14450,U 14490,U 14540,U 14640,U
STRNT	REAL*8			14350,S 14440,U 14470,U 14540,U 14640,U
STTMST	REAL*8			14510,S 14600,U 14690,U
STTRMT	REAL*8			14500,S 14620,U 14700,U
T	REAL*8	50		1020,D 2690,S 3030,U 6600,D 6780,U 6790,U 6800,U 6810,U 6820,U 6830,U 7130,D 13640,D 14410,U 14420,U 16870,D 17020,U 17040,U 17060,U 17080,U
TAPES	REAL*8			120,D 1110,D 14970,D 16170,D
TDT2	REAL*8			9290,S 9330,U 9350,U
TEST	REAL*8	END		150,S 310,U 330,U 400,U
TFORCE	REAL*8			4520,U 16850,D
TH	REAL*8	50,5,2		1080,D 3300,S 3630,S 3640,S 3770,U 3770,S 3890,U 3890,S 3910,S 4460,S 4500,U 4770,S 4770,U 4930,U 7170,D 8790,U 8790,U 8790,U 13710,D 14010,U 14010,U 14100,U 16150,D 16730,S 16890,D 17270,U 17280,U 17300,U 17320,U 17340,U 17360,U 17380,U 17400,U 17420,U
THCDE	REAL*8			4510,U 16100,D
THCON	REAL*8			1020,D 7180,D
ATHER	REAL*8			1080,D 7170,D 13710,D 16150,D 16890,D
THETA	REAL*8			1040,D 1340,D 1810,S 1940,S 1940,U 5740,D 6110,U 6120,U 6230,U 6650,D 13630,D 13980,U 13990,U 14520,U
THETAS	REAL*8			1040,U 5740,D 6650,D 13630,D
THETAI	REAL*8			6230,S 6240,U 14520,S 14540,U 14640,U

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
THETB	REAL*8		74	14890,D 15170,S 15210,U 15220,S 15270,U 15280,U 15310,U 15320,U 15340,U 15340,S 15450,U 15460,U 15480,U 15480,U 15490,U 15490,U 15490,U 16140,D 16300,S 16330,U 16350,S 15300,U 16390,U 16430,U 16430,S 16530,U 16530,U 16540,U 16540,U 16590,U 16600,U
THT	REAL*8			8790,S 8820,I 8830,U 14010,S 14090,U 14100,U
TH1	REAL*8		5	1130,D 4420,S 4460,U
TIM	REAL*8			3990,S 4050,U
TIME	REAL*8			70,D 630,S 640,U 690,P 730,U 730,S 1010,D 4910,U 5010,U 5660,U 5930,U 6350,U 6570,D 7190,D 8790,U 9050,D 9140,U 9150,U 9860,D 9980,U 13680,D 13790,U 14010,U 14020,U
TIMEP	REAL*8			100,D 560,S 580,U 630,U 1070,D 3280,S 3500,U 5770,D 9060,D
TMFT	REAL*8			70,D 1010,D 6570,D 7190,D 9050,D 9860,D 13680,D
TM1	REAL*8			13790,S 13810,U
TOTIME	REAL*8			70,D 580,U 1010,D 1320,S 1780,U 3800,U 4000,U 6570,D 7190,D 9050,D 9860,D 13680,D
TPRINT	REAL*8			13800,S 13810,U
TPRNT	REAL*8			3500,S 3510,U 4050,S 4060,U 5010,S 5020,U 5930,S 5940,U 6220,U
TRI40R	REAL*8			3210,U 17580,D
T0	REAL*8			70,D 570,S 660,S 1010,D 3280,S 3790,S 3960,S 4910,U 6570,D 7190,D 8790,U 8790,U 9050,D 9140,U 9140,U 9150,U 9860,D 9980,U 9980,U 13680,D 14010,U 14010,U 14020,U 14020,U
T1	REAL*8			70,D 640,U 660,U 1010,D 3280,S 3790,U 3800,S 3960,U 3980,S 3990,U 4000,S 4910,U 6570,D 7190,D 8790,U 9050,D 9140,U 9150,U 9860,D 9980,U 13680,D 14010,U 14020,U 14020,U
T3	REAL*8			9140,S 9350,U 9980,S 10010,U
T3M1	REAL*8			9150,S 9240,U
XIH1	REAL*8			6100,S 6110,U 6120,U 13970,S 13980,U 13990,U 14170,U 14200,U 14200,U 14210,U 14250,U 14260,U 14270,U
XK	REAL*8			7610,S 7620,U 7630,U 7640,U 7650,U 7700,U
XKEEP	REAL*8			3380,S 3400,U 3410,S 3430,U 9540,S 9560,U 9690,S 9710,U
XN	REAL*8	6550	940,U 9540,U	1150,S 1150,S 9690,U 9700,U 9700,S 9790,D 5680,D 8980,D 9170,P 9400,U 9400,S
XP	REAL*8	6550	100,D 9850,D	3140,S 3140,U 3190,U 9040,D 9280,P 9400,U 9550,U 9560,S 9700,U 9710,S

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
X1	REAL*8			15450,S 15520,U 15530,U 15540,U 16590,S 16610,U 16620,U
X2	REAL*8			15460,S 15520,U 15530,U 15540,U 16600,S 16610,S 16620,S
YKP	REAL*8			15380,S 15450,U 15460,U 15520,U 15530,U 15540,U 16470,S 16590,U 16600,U 16610,U 16620,U 17260,S 17280,U 17300,U 17330,U 17350,U 17400,U 17400,U 17420,U 17420,U
Z	REAL*8	51	1120,D	2770,S 7220,D 7320,U 7320,U

FRCFS

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
AI	REAL*8		167	14970,0 15640,U 15650,U 15660,U 15670,U 15680,U 15690,U 15700,U 15710,U 15790,U 15870,U 15810,U 15820,U 15830,U 15840,U 15850,U 15860,U
ALPHK	REAL*8			14970,U
ANG	REAL*8			15200,S 15220,U
CHALS	REAL*8			14970,0
CHECK	REAL*8		8,8	14970,0 15010,U
CONST	REAL*8			14930,0
C12	REAL*8			15740,S 15750,S 15760,U 15770,U 15780,U
DCOS	REAL*8			15540,U 15540,U
DSIN	REAL*8			15520,U 15520,U 15530,U 15530,U
DT2	REAL*8			14930,0
ENRCE	REAL*8		2040	14910,0 15940,S 15940,U
FRCF	REAL*8			14990,0
FRCFS	REAL*8			14970,0
HARM	REAL*8			14950,0
I	INTEGER			15080,U 15080,U 15080,U 15080,S 15090,U 15090,U 15090,U 15090,U 15090,U 15090,S 15170,U 15170,U 15170,U 15170,S 15270,U 15270,U 15270,U 15270,U 15270,U 15280,U 15280,S 15310,U 15310,U 15320,U 15320,U 15320,S 15400,S 15410,U 15430,U 15450,U 15460,U 15480,U 15480,U 15480,U 15490,U 15490,U 15520,U 15530,U 15540,U 15880,S 15890,U 15890,U 15910,U 15910,U 15920,S 15930,U 15940,U
IR	INTEGER			14870,U 15930,U
IDCNE	INTEGER			14940,0 15050,U 15390,U
IDELF	INTEGER			14940,0
IDP	INTEGER			15230,S 15240,U 15340,U
IFLM	INTEGER			14870,U 15030,U 15040,U 15040,U 15060,U 15130,U 15930,U
IFLM1	INTEGER			15080,S 15090,U 15170,S 15270,U
IFLM2	INTEGER			15030,S 15040,U 15080,S 15190,U 15170,S 15270,U
IH	INTEGER			15360,S 15370,U 15760,U 15770,U 15780,U 15930,U
THARM	INTEGER			14950,0 15370,U

FRCFS

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
J	INTEGER		15920,S	15910,U 15910,U 15920,S 15940,U 15940,U
KFY	INTEGER		15210,S	15220,U 15230,U 15240,U 15250,U
KYP	INTEGER		15370,S	15380,U 15470,U 15560,U 15750,U
LF	INTEGER		15040,U	
N	INTEGER		14930,D	
ND	INTEGER		14970,D	15080,U 15170,U
NDP	INTEGER		15170,S	15170,U 15180,U 15190,U 15280,U 15290,U 15300,U 15310,U 15420,U 15440,U
NDPP2	INTEGER		15300,S	15320,U
NDP1	INTEGER		15420,S	15430,U
NDP2	INTEGER		15180,S	15210,U
ND2	INTEGER		15200,S	15320,U 15330,U
NELMS	INTEGER		14930,D	
NFO	INTEGER		14930,D	15930,U
NFOT	INTEGER		14930,D	15930,U
NH	INTEGER		14930,D	15080,U 15090,U 15360,U
NHNS	INTEGER		14930,D	
NHP	INTEGER		14950,D	
NN	INTEGER		14930,D	
NNODES	INTEGER		14920,D	
NPRNTF	INTEGER		14940,D	
NRNTI	INTEGER		14940,D	15060,U 15090,U 15130,U 15270,U 15310,U
NPRNTO	INTEGER		14930,D	
NS	INTEGER		14970,D	
NTZFE	INTEGER		14930,D	
NT	INTEGER		14970,D	

ERFCS

VARIABLE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
R	REAL*8	74	14890,0 15080,S 15090,U 15170,S 15230,S 15230,U 15270,U 15310,U 15480,U 15520,U 15570,U 15760,U
PT	REAL*8		15020,S 15570,U 15580,U 15760,U 15770,U 15780,U
PINT	REAL*8		15480,S 15520,S 15570,S 15610,S 15680,U 15690,U 15760,S 15830,U 15840,U
Q	REAL*8	8	14960,0 15410,S 15640,S 15640,U 15650,S 15650,U 15660,S 15660,U 15670,S 15670,U 15680,S 15690,U 15690,S 15690,U 15700,S 15700,U 15710,S 15710,U 15790,S 15830,S 15810,S 15820,S 15830,S 15840,S 15850,S 15860,S 15910,U
QN	REAL*8	1020	14910,0
QN1	REAL*8	1020	14910,0
QN2	REAL*8	1020	14910,0
QP	REAL*8	1020	14910,0
QP1	REAL*8	1020	14910,0
QQ	REAL*8	8	14960,0 15820,S 15910,S 15910,U 15940,U
QS	REAL*8		14910,0
QUES	REAL*8		14960,0
R	REAL*8	74	14890,0 15080,S 15090,U 15170,S 15240,S 15240,U 15270,U 15310,U 15490,U 15530,U 15580,U 15770,U
QTNT	REAL*8		15400,S 15520,S 15580,S 15620,S 15640,U 15650,U 15660,U 15670,U 15770,S 15790,S 15820,U 15810,U 15820,U
S	REAL*8	74	14890,0 15080,S 15090,U 15170,S 15250,S 15250,U 15270,U 15310,U 15540,U 15780,U
SINT	REAL*8		15520,S 15540,S 15590,S 15630,S 15700,U 15710,U 15780,S 15850,U 15860,U
TAPES	REAL*8		14970,0
THETB	REAL*8	74	14890,0 15170,S 15220,U 15220,S 15270,U 15280,U 15310,U 15320,U 15340,S 15340,U 15450,U 15460,U 15480,U 15480,U 15490,U 15490,U
X1	REAL*8		15450,S 15520,U 15530,U 15540,U
X2	REAL*8		15460,S 15520,U 15530,U 15540,U
YKP	REAL*8		15380,S 15450,U 15460,U 15520,U 15570,U 15540,U

HOURON

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
CONST	REAL*8			9830,0
DFLTG	REAL*8			9860,0
DT2	REAL*8			9830,0 10030,U
FORCE	REAL*8	2040	9820,0 10010,II 10010,U 10010,U	
HOURON	REAL*8			9770,0
I	INTEGER		9920,S 9930,U 9990,S 10000,U 10030,U 10030,U 10120,S 10130,U 10190,S 10200,U 10210,U	
IDONE	INTEGER			9840,0
IDELF	INTEGER			9840,0
IEQ	INTEGER			10130,S 10140,II
TH	INTEGER			9770,II 9960,P 10190,P
KY	INTEGER			9770,II 10100,U
LK	INTEGER	204	9820,0 10130,U	
MATMUT	INTEGER			9960,II
N	INTEGER			9930,0 9930,U 10000,U 10200,U
NCLOSE	INTEGER			9920,0 10100,U
NFLFMS	INTEGER			9830,0
NEQ	INTEGER			9830,0 9920,II 9960,P 9990,U 10190,U
NEQT	INTEGER			9830,0 10010,U
NH	INTEGER			9930,0
NHNS	INTEGER			9830,0
NN	INTEGER			9920,0
NNODES	INTEGER			9820,0
NNODE	INTEGER		10090,S 10100,S 10100,U 10110,U 10120,II	
NOORE	INTEGER			9820,0 10090,U
NOORES	INTEGER			9930,S 9940,II 9940,U 9940,II 9940,U 10000,S 10010,U 10010,U 10010,U 10010,U 10010,U 10040,U 10040,U 10050,U 10050,U 10060,U 10060,U 10060,S 10210,U
NPT	INTEGER			

HOURON

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
NPRNTF	INTEGER			9840,D
NDRNTI	INTEGER			9840,D
NPRNTO	INTEGER			9830,D
NSIZE	INTEGER			9830,D
PS	REAL**8			9850,D
OLNAD	REAL**8	204	9790,D	9960,P 10030,S 10030,U 10140,S 10210,U
DN	REAL**8	1020	9800,D	9940,U 10050,U 10210,S
DN1	REAL**8	1020	9800,D	9940,U 10040,U 10050,S
DN2	REAL**8	1020	9800,D	9940,S 9940,U 9960,P 10040,S
DP	REAL**8	1020	9800,D	10010,U 10060,U
DP1	REAL**8	1020	9800,D	10010,U 10060,S
QS	REAL**8			9800,D
QSS	REAL**8			10010,S 10030,U
RSTRNT	REAL**8			9820,D
SLVFFO	REAL**8			9790,D
SOLVED	REAL**8			10110,U
TIME	REAL**8		9860,D	9990,U
TMFT	REAL**8			9860,D
TOTIME	REAL**8			9860,D
TA	REAL**8		9860,D	9980,U 9990,U
T1	REAL**8		9860,D	9980,U
T3	REAL**8		9980,S	10010,U
XN	REAL**8	6550	9790,D	
XP	REAL**8	6550	9850,D	9960,D

HOUJ801

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
CONST	REAL*8			9020,0
DEFTE	REAL*8			9050,0 9150,I 9200,U
DELTED	REAL*8			9060,0
DT2	REAL*8			9020,0 9290,U 9320,U 9350,I 9350,U 9400,I 9650,U
FORCE	REAL*8	2047	8990,0	9220,I 9240,U 9240,U 9240,U 9330,U 9350,U 9360,U 9360,U
HOUR01	REAL*8			8960,0
I	INTEGER			9180,S 9190,I 9220,I 9220,U 9240,I 9240,U 9300,S 9310,U 9330,U 9330,I 9330,U 9350,I 9350,U 9350,U 9380,S 9390,U 9470,S 9480,U 9490,U 9500,U 9500,I 9520,S 9520,U 9630,S 9640,I 9650,U 9670,S 9680,U
IDCDE	INTEGER			9030,0
IDELF	INTEGER			9030,0
IFLAG	INTEGER			9130,S 9460,I 9590,S
TH	INTEGER			8960,I 9170,P 9280,P 9450,P
IPSTRT	INTEGER			9060,0 9210,I 9320,U
ITP	INTEGER			9060,0
KV	INTEGER			8960,U 9430,P 9740,P
LK	INTEGER	204	9010,0	
MATM1T	INTEGER			9170,I 9280,I
M	INTEGER			9020,0 9190,I 9310,I 9480,I 9640,I
NCLOSE	INTEGER			9010,0
NFLMS	INTEGER			9020,0
NFQ	INTEGER			9020,0 9170,P 9180,I 9280,P 9300,U 9470,U 9630,U
NFQT	INTEGER			9020,0 9240,I 9360,I
NH	INTEGER			9020,0
NHNS	INTEGER			9020,0
NN	INTEGER			9020,0 9390,U 9520,U 9680,I
NNODES	INTEGER			9020,0

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HOUR01

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
TIMEP	REAL*8		9060,0	
TMET	REAL*8		9050,0	
TOTIME	REAL*8		9050,0	
T1	REAL*8		9050,0	9140,U 9140,U 9150,U 9150,U
T1	REAL*8		9050,0	9140,U 9150,U
T2	REAL*8		9140,S	9350,U
TRM1	REAL*8		9150,S	9240,II
XKEFP	REAL*8		9540,S	9560,II 9600,S 9710,U
XV	REAL*8	6550	8980,0	9170,P 9400,S 9400,U 9540,II 9550,S 9600,U 9700,S 9700,U
XP	REAL*8	6550	9040,0	9280,P 9400,U 9550,U 9560,S 9700,U 9710,S

INPUT

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
AI	REAL*8		167	930,0 2650,S 2660,U 4310,S 4490,S
ALPHK	REAL*8			4320,0
ALS	REAL*8		50	1080,0 2890,S 2940,S 3020,U
ALSTI	REAL*8			2870,S 2890,U
ALT	REAL*8		50	1080,0 2900,S 2950,S 3020,U
ALTTI	REAL*8			2870,S 2900,U
ARCI	REAL*8		50	1030,0 2720,S 2740,S 3030,U
CHALS	REAL*8			930,0
CHECK	REAL*8		8,8	930,0 2650,S 2660,U 4310,S 4490,S
COMMENT	REAL*8		20	1130,0 1150,S 1270,S 1280,U 1490,S 1510,U
CONST	REAL*8			980,0
CONSTF	REAL*8			1160,0 1200,S 3710,U 3980,S 4000,U 4060,U 4720,U
CONSTN	REAL*8	CONSTANT		1160,0 1170,S 3710,U 4000,U 4720,U
CONSTI	REAL*8	R1 + S		1160,0 1170,S 1200,U
COSTNF	REAL*8		51	1030,0 2720,S 2740,S 2740,S
COSM	REAL*8		50	1030,0 2790,S
CYCLE	REAL*8			1100,0
DATA	REAL*8			1170,S
DCDS	REAL*8			2790,U
DELTE	REAL*8			1010,0
DELTED	REAL*8			1070,0 3280,S 3430,U 3510,U
DELTU	REAL*8			1320,S 1780,U 2010,U 3430,U 4910,U 4950,U
DOUBLF	REAL*8			1160,0
DSTN	REAL*8			2800,U
DTH	REAL*8	50,5,2	1080,0 4580,U	3310,S 3650,S 3660,S 3780,S 3780,U 3900,S 3900,U 3920,S 4450,S 4780,S 4780,U
DTHL	REAL*8	5	1130,0	4420,S 4450,U

INPUT

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHEN/HOW USED	INPUT									
DT2	REAL*8			980,0	2010,S									
DJM	REAL*8		1310	1140,0	1150,S	1500,S	1610,S	1640,S	1660,S	1690,S	1730,S			
F1	REAL*8		57	1020,0	2680,S	3020,U								
F2	REAL*8		57	1020,0	2680,S	3020,U								
FNU1	REAL*8		50	1020,0	2680,S	3020,U								
FNU2	REAL*8		50	1020,0	2680,S	3020,U								
FORCE	REAL*8		2040	950,0 2850,S 4740,U	3080,S 4100,S 4910,U	3080,S 4200,S 4210,S	3280,S 4220,S 4220,U	3580,S 4220,S 4700,U	3590,S 4700,U 4700,U	3740,S 4700,U 4700,U	3740,U 4700,U 4740,S	3840,S 4700,U 4740,S	3840,U 4700,U 4740,S	
FRCES	REAL*8			4220,U										
F1	REAL*8			4160,S	4190,U	4220,U								
F2	REAL*8			4160,S	4200,U	4230,U								
F3	REAL*8			4160,S	4210,U	4230,U								
F4	REAL*8			4160,S	4220,U	4230,U								
G	REAL*8		50	1020,0	2680,S	3020,U								
GFM	REAL*8			1020,0										
HARM	REAL*8			1060,0										
I	INTEGER			1250,S 1640,S 1660,U 1660,S 1810,U 1810,S 2180,U 2550,S 2660,S 2660,U 2690,U 2690,S 2720,U 2720,U 2770,U 3020,U 3030,U 3140,S 3170,U 3200,S 3200,U 3220,U 3610,S 3620,U 3770,U 3900,U 4400,S 4770,U 4980,S 5000,S	1340,U 1660,U 1660,S 1660,U 1810,S 1810,U 2550,U 2660,U 2660,S 2690,U 2690,S 2720,U 2720,U 2770,S 3020,U 3030,U 3140,S 3170,S 3200,S 3200,U 3220,U 3610,S 3620,U 3770,U 3900,U 4400,U 4770,U 4980,U 5000,U	1340,S 1660,S 1660,U 1660,U 1810,S 1810,S 2550,S 2660,S 2660,U 2690,S 2690,U 2720,U 2720,U 2770,U 3020,U 3030,U 3140,S 3170,S 3200,S 3200,U 3220,U 3610,S 3620,U 3770,U 3900,U 4400,U 4770,U 4980,U 5000,U	1370,U 1660,U 1660,S 1660,U 1810,S 1810,U 2550,U 2660,U 2660,S 2690,U 2690,S 2720,U 2720,U 2770,U 3020,U 3030,U 3140,S 3170,S 3200,S 3200,U 3220,U 3610,S 3620,U 3770,U 3900,U 4400,U 4770,U 4980,U 5000,U	1370,S 1660,S 1660,U 1660,U 1810,S 1810,U 2550,S 2660,S 2660,U 2690,U 2690,S 2720,U 2720,U 2770,U 3020,U 3030,U 3140,S 3170,S 3200,S 3200,U 3220,U 3610,S 3620,U 3770,U 3900,U 4400,U 4770,U 4980,U 5000,U	1590,U 1660,U 1660,S 1660,U 1810,S 1810,U 2550,U 2660,U 2660,S 2690,U 2690,S 2720,U 2720,U 2770,U 3020,U 3030,U 3140,S 3170,S 3200,S 3200,U 3220,U 3610,S 3620,U 3770,U 3900,U 4400,U 4770,U 4980,U 5000,U	1590,S 1660,S 1660,U 1660,U 1810,S 1810,U 2550,S 2660,S 2660,U 2690,U 2690,S 2720,U 2720,U 2770,U 3020,U 3030,U 3140,S 3170,S 3200,S 3200,U 3220,U 3610,S 3620,U 3770,U 3900,U 4400,U 4770,U 4980,U 5000,U	1610,U 1660,U 1660,S 1660,U 1810,S 1810,U 2550,U 2660,U 2660,S 2690,U 2690,S 2720,U 2720,U 2770,U 3020,U 3030,U 3140,S 3170,S 3200,S 3200,U 3220,U 3610,S 3620,U 3770,U 3900,U 4400,U 4770,U 4980,U 5000,U	1610,S 1660,S 1660,U 1660,U 1810,S 1810,U 2550,S 2660,S 2660,U 2690,U 2690,S 2720,U 2720,U 2770,U 3020,U 3030,U 3140,S 3170,S 3200,S 3200,U 3220,U 3610,S 3620,U 3770,U 3900,U 4400,U 4770,U 4980,U 5000,U	1640,U 1660,U 1660,S 1660,U 1810,S 1810,U 2550,U 2660,U 2660,S 2690,U 2690,S 2720,U 2720,U 2770,U 3020,U 3030,U 3140,S 3170,S 3200,S 3200,U 3220,U 3610,S 3620,U 3770,U 3900,U 4400,U 4770,U 4980,U 5000,U	

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INPUT

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INPUT

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED							
TP\$TRT	INTEGER	1070,0	1320,S	1370,U 1390,U 1780,U 2060,U 3220,U							
TTAM	INTEGER	1100,0	4910,U	5020,U							
ITCDE	INTEGER	1000,0	3980,S	4400,U 4500,U							
ITELF	INTEGER	1000,0	1320,S	1700,U 2820,U 4340,U							
ITD	INTEGER	1070,0	3280,S	3350,U 3510,U							
IX	INTEGER	2580,S	2500,U	2590,U 2600,U 2600,U 2600,U 2600,U							
J	INTEGER	1270,U 1680,S 3640,U 3800,U 4770,U	1270,S 1690,U 3650,U 3900,U 4770,U	1280,U 1700,S 3660,U 3910,U 4780,U	1280,S 1720,U 3760,S 3920,U 4780,U	1490,U 2650,U 3770,U 3920,U 4780,U	1490,S 2650,S 3770,U 4310,U 4490,U	1510,U 2660,U 3780,U 4310,S 4490,S	1510,S 2660,S 3780,U 4490,S 4760,S	1600,U 3620,S 3880,S 3890,U 4760,S	1610,U 3630,U 3890,U 4760,S
JH	INTEGER	3050,S	3260,U	3120,U 3160,U 3180,U							
JUNK	INTEGER	27	1130,0	1450,S 1530,S 1740,S 3270,S 4900,U							
K	INTEGER	1480,S 4690,S	1580,S 4700,U	1620,S 4700,U	1630,U 4700,U	1720,S 4700,U	4180,S 4700,U	4190,U 4700,U	4200,U 4700,U	4210,U 4700,U	4220,U
KFY	INTEGER	910,U	1180,U	3710,U 3950,U							
KEYRS	INTEGER	1380,S	1390,S	1500,U 1540,U 1750,S							
KK	INTEGER	4650,S	4690,U								
KYD	INTEGER	4660,S	4670,U								
LK	INTEGER	204	970,0	2180,S 2190,S 2200,S 3280,S 3330,S 3340,S 4910,U							
LL	INTEGER	1050,0									
N	INTEGER	980,0	2280,S	2320,U 2420,S 2460,U							
NCARDS	INTEGER	1230,S	1240,U	1250,U 1450,S 1460,U 1480,U							
NCF	INTEGER	3990,S	4070,U								
NCF1	INTEGER	4110,S	4120,U								
NCLOST	INTEGER	1040,0	1330,S	1790,U							
NCLOSE	INTEGER	970,0	1320,S	1790,U							
ND	INTEGER	1110,0 2300,U	1230,U 2440,U	1270,U 2870,U	1320,U 3980,U	1340,U 4110,U	1370,U 4160,U	1790,U 4420,U	2110,U 4420,U	2160,U 4420,U	2250,U

INPUT

VARIABLE TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED	INPUT								
NODREC	INTEGER		2160,S	2170,U	2180,U							
NELFMS	INTEGER		980,D	1530,S	1580,U	1600,U	1620,U	1630,U	1680,U	1710,U	1790,U	1960,U
			1000,U	2640,U	2680,U	2680,U	2680,U	2690,U	2690,U	2690,U	2700,U	2710,U
			2780,U	2910,U	2920,U	3220,U	3220,U	3310,U	3610,U	3750,U	3870,U	4300,U
			4470,U	4480,U	4570,U	4750,U	4930,U	4940,U				
NFO	INTEGER		980,D	1970,S	1980,U	2280,U	2420,U	2560,U	4180,U	4650,U		
NFOT	INTEGER		980,D	1980,S	2020,U	3260,U	3320,U	3320,U	3320,U	3370,U	3570,U	3590,U
			3730,U	3740,U	3830,U	3840,U	3850,U	4180,U	4650,U	4730,U	4740,U	4890,U
NH	INTEGER		980,D	1370,S	1370,U	1740,S	1740,U	1800,U	1800,U	1980,U	2000,U	2270,U
			2410,U	2550,U	3050,U	3270,S	3270,U	3320,U	3310,U	3620,U	3760,U	3880,U
			4080,U	4420,U	4440,U	4550,U	4640,U	4760,U	4900,U	4900,U	4930,U	4940,U
NHNS	INTEGER		980,D	2000,S								
NHP	INTEGER		1060,D	1530,S	1700,U	3040,U						
NLTERM	INTEGER		3360,U									
NN	INTEGER		980,D	3120,S	3130,U	3140,U	3170,U	3190,U				
NNODES	INTEGER		980,D	1960,S	1970,U	2370,U	2510,U	2570,U	2770,U	2770,U	4250,U	4680,U
NOORES	INTEGER		970,D	2110,S	2120,U	2130,U	2140,U	2190,U	2200,U	3280,S	3280,U	3330,U
NOTT	INTEGER		1050,D	1250,S								
ND	INTEGER		2160,S	2170,U	2180,U							
NPRNIT	INTEGER		1070,D	1330,S	1780,U							
NPRNMS	INTEGER		1330,S	1800,U	3150,U							
NPRNT	INTEGER		1070,D	1330,S	1780,U							
NPRNTF	INTEGER		990,D	1330,S	1790,U	4010,U	4600,U					
NPRNTH	INTEGER		1000,D	1330,S	1790,U	4540,U						
NPRNTI	INTEGER		990,D	1330,S	1790,U	4010,U	4170,U	4230,U				
NPRNTQ	INTEGER		980,D	1320,S	1780,U							
NS	INTEGER		1110,D	1790,U	2620,U	2660,U	4290,U	4310,U	4380,U	4490,U		

INPUT

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED								
NSIZE	INTEGER			980,0 1710,S 1730,U 1990,S 2000,U 3080,U 3090,U 3120,U 3130,U 3140,U 3170,U 3190,U								
NSTRESS	INTEGER			1040,0 1330,S 1700,U								
NT	INTEGER			1110,0 1230,S 1440,U 1450,U 1490,U 1530,U 1590,U 1610,U 1640,U 1660,U 1690,U 1730,U 1740,U 1790,U 2650,U 2680,U 2720,U 2740,U 2770,U 3080,U 3090,U 3130,U 3140,U 3270,U 3280,U 3300,U 3320,U 4900,U 4910,U 4930,U								
NTF	INTEGER			3260,S 3290,U 4990,S 4920,U								
NTHETA	INTEGER			1040,0 1340,S 1340,U 1810,U 1810,U 1930,U								
PH	REAL*8	50		1030,0 2720,S 2740,S 2790,U 2800,U 3030,U								
PHD	REAL*8	50		1030,0 2720,S 2740,S 3030,U								
P1	REAL*8			1910,S 1920,U								
PRINT	REAL*8			1050,0								
PS	REAL*8			1000,0								
QDC1	REAL*8			4970,S 4990,U								
QDC2	REAL*8			4960,S 4990,U								
QDC3	REAL*8			4950,S 4960,U 4970,U 4990,U								
QLNAD	REAL*8	204		940,0								
QN	REAL*8	1020		950,0 2030,S 2320,S 2380,U 2290,U 4990,U 2350,S 2360,S 2590,U 2590,U 2590,U 2590,U 2320,S 2380,U 2290,U 4990,U								
QN1	REAL*8	1020		950,0 2040,S 2470,S 2480,S 2490,S 2500,S 2600,U 2600,U 2600,U 2600,U 2320,S 2390,U 2400,S 4990,U								
QN2	REAL*8	1020		950,0 4990,U								
QP	REAL*8	1020		950,0 3420,U 3430,U 3430,S 3430,U 4990,S 5020,U								
QP1	REAL*8	1020		950,0 3320,S 3410,U 3420,S 5000,U								
QS	REAL*8			950,0								
Q1	REAL*8			2300,S 2320,U 2440,S 2470,U								
Q2	REAL*8			2310,S 2340,U 2440,S 2480,U								
Q3	REAL*8			2300,S 2350,U 2440,S 2490,U								

INPUT

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
Q4	REAL*8			2300,S 2360,U 2440,S 2500,U
R	REAL*8	50	1030,D	2720,S 2740,S 3020,U
RAD	REAL*8		1020,S	1040,U
PESTRT	REAL*8		1070,D	
RETRNT	REAL*8		970,D	
R7	REAL*8		1120,D	
DN	REAL*8	51	1120,D	2770,S
SINF	REAL*8	51	1020,D	2720,S 2740,S 2740,S
SINH	REAL*8	50	1030,D	2800,S
SIVFFQ	REAL*8		940,D	
T	REAL*8	50	1020,D	2690,S 3030,U
TAPES	REAL*8		1310,D	
TFORCE	REAL*8		4520,U	
TH	REAL*8	50,5,2	1080,D 4580,U	3300,S 3630,S 3640,S 3770,S 3770,U 3890,S 3890,U 3910,S 4460,S 4770,S 4770,U 4930,U
THCOF	REAL*8		4510,U	
THCON	REAL*8		1000,D	
THFR	REAL*8		1080,D	
THETA	REAL*8		1040,D	1340,D 1810,S 1940,U 1940,S
THETAS	REAL*8		1040,U	
THI	REAL*8	5	1130,D	4420,S 4460,U
TM	REAL*8		3990,S	4050,U
TIME	REAL*8		1010,D	4010,U 5010,U
TIMEP	REAL*8		1070,D	3280,S 3500,U
TMET	REAL*8		1010,D	
TOTTIME	REAL*8		1010,D	1320,S 1780,U 3800,U 4000,U
TPRNT	REAL*8		3500,S	3510,U 4050,S 4060,U 5010,S 5020,U

INPUT

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
TP140P	REAL*8			3210,U
T0	REAL*8		1010,D	3280,S 3700,S 3960,S 4910,U
T1	REAL*8		1010,D	3280,S 3790,U 3800,S 3960,U 3980,S 3990,U 4000,S 4910,U
XKFP	REAL*8		3280,S	3400,II 3410,S 3430,II
XN	REAL*9	6550	940,D	1150,S 2130,S 3170,U
XP	REAL*9	6550	1000,D	3140,S 2190,U
Z	REAL*8	51	1120,D	2770,S

MAIN

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
CARD	REAL*8		20	130,0 140,S 300,S 210,U 330,U 330,U 390,U 400,U
CONST	REAL*8			50,0
CYCLE	REAL*8			110,0
DELTF	REAL*8			70,0 580,U 580,U 530,U 730,U
DELTF0	REAL*8			100,0
DT2	REAL*8			50,0
FORCE	REAL*8		2040	30,0
HARM	REAL*8			90,0
I	INTEGER			510,0 520,U
INCOE	INTEGER			60,0
INELF	INTEGER			60,0
THADM	INTEGER	5		90,0
INDIJT	INTEGER			470,U 670,0
IPRINT	INTEGER			80,0
IPSTRT	INTEGER			100,0 500,U 610,U
ITAM	INTEGER			110,0 620,S 630,U 650,U 690,P 720,S 740,P
ITD	INTEGER			100,0 550,S 580,U 610,U 630,U
KKP2	INTEGER			580,S 590,U 620,U 650,U 720,U
LARGE	INTEGER			400,S 600,0 700,U
LL	INTEGER			80,0 600,S 610,S 620,U
MPRINT	INTEGER			290,S 340,U 370,S 380,S 380,U
N	INTEGER			50,0
NCARD	INTEGER			270,S 310,U 320,S 320,U 410,U
NCASE	INTEGER			220,S 280,S 280,U 350,U 420,S 420,U 430,U 460,S 480,S 480,U 750,U
NCASES	INTEGER			200,S 210,U 430,U 750,U
ND	INTEGER			120,0 200,S 260,U 330,U 440,U

MAIN

VARIABLE	INITIAL TYPE	VALUE	DIMENSION	WHERE/HOW USED
NLEMS	INTEGER		50,0	
NFO	INTEGER		50,0	
NEOT	INTEGER		50,0	510,0
NH	INTEGER		50,0	
NHNS	INTEGER		50,0	
NHD	INTEGER		90,0	
NLTERM	INTEGER		740,0	
NN	INTEGER		50,0	
NNODES	INTEGER		50,0	
NOTT	INTEGER		80,0	590,5
NPRNTT	INTEGER		100,0	
NPRNT	INTEGER		100,0	
NPRNTF	INTEGER		60,0	
NPRNTL	INTEGER		60,0	
NPRNTO	INTEGER		50,0	
NS	INTEGER		120,0	200,S
NSIZE	INTEGER		50,0	
NT	INTEGER		120,0	
PRINT	REAL*8		80,0	
QV	REAL*8	1020	30,0	140,S
QV1	REAL*8	1020	30,0	
QV2	REAL*8	1020	30,0	
QP	REAL*8	1020	30,0	
QP1	REAL*8	1020	30,0	520,S
QS	REAL*8		30,0	
RFSTRT	REAL*8		100,0	

MAIN

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
SETUP	REAL**8			690,U
TAPES	REAL**8			120,D
TEST	REAL**8	END	150,S	310,U 230,U 400,U
TIME	REAL**8		70,D	630,S 640,U 690,P 730,S 730,U
TIMEP	REAL**8		100,D	560,S 580,U 630,U
TMET	REAL**8		70,D	
TOTIME	REAL**8		70,D	580,II
T0	REAL**8		70,D	570,S 660,S
T1	REAL**8		70,D	640,U 660,II

MATMUT

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
A	REAL*8	204	10850,0 10870,0 10950,S 11040,S 11040,S 11050,S 11050,U 11060,S 11060,U 11070,S 11070,U 11190,S 11180,U 11190,S 11190,U 11210,S 11210,U	
FORCE	REAL*8	1020	10950,U 10870,D 10940,U 11050,II 11060,U 11060,U 11070,U 11070,U 11080,U 11180,U 11190,U 11210,U	
I	INTEGER		10940,S 10950,U 11020,S 11040,U 11040,U 11110,S 11120,U	
TH	INTEGER		10850,U 10980,U 10997,U	
TID	INTEGER		10850,II 10940,U 10960,U 10990,U	
J	INTEGER		11010,S 11020,II 11040,U 11140,U 11150,U 11180,U 11190,U 11190,U 11210,U 11210,U 11210,U	
JM1	INTEGER		11150,S 11160,U	
L	INTEGER		11160,S 11180,U 11180,U 11190,U	
MATMUT	INTEGER		10850,0	
NA	INTEGER		11030,S 11030,S 11030,S 11040,U	
NF	INTEGER		10990,S 11040,U 11050,U 11060,U 11060,U 11070,U 11070,U 11080,U 11130,U	
NFF	INTEGER		11130,S 11180,U 11190,U 11210,U	
NT	INTEGER		11120,S 11130,II 11180,U 11180,U 11190,U 11190,U 11210,U 11210,U	
NK	INTEGER		10990,S 11000,U 11050,U 11060,U 11060,U 11070,U 11070,U 11070,U 11090,U	
NKK	INTEGER		11000,S 11170,S 11170,U 11180,U 11190,U 11200,S 11200,S 11210,U	
NM1	INTEGER		11100,S 11110,U	
NN	INTEGER		10960,S 10970,U 11100,U	
NT	INTEGER		10970,S 10980,U	
STFM	REAL*8	6550	10850,U 10870,D 11040,U 11050,U 11060,U 11060,U 11070,U 11070,U 11070,U 11180,U 11190,U 11210,II	

NLTERM

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHICH/HOW USED
APCL	REAL*8		50	6610,0
CF1	REAL*8			6640,0 6780,S
CF2	REAL*8			6640,0 6790,S
CONST	REAL*8			6550,0
COSINE	REAL*8		51	6610,0
COSH	REAL*8		50	6610,0
DD1	REAL*8			6640,0 6820,S
DD2	REAL*8			6640,0 6830,S
DELT	REAL*8			6570,0
DT2	REAL*8			6550,0
DFS	REAL*8			6620,0
ES	REAL*8	5		6620,0
FCT	REAL*8	5		6620,0
ST	REAL*8	5		6620,0
F1	REAL*8	50	6600,0	6780,II 6820,II
F13	REAL*8	5	6620,0	
F2	REAL*8	50	6600,0	6790,II 6830,II
F23	REAL*8	5	6620,0	
FV	REAL*8		6770,S	6780,II 6790,II 6820,II 6830,II
FAU1	REAL*8	50	6600,0	6770,II
FAU2	REAL*8	50	6600,0	6770,II
FORCE	REAL*8	2040	6580,0	
G	REAL*8	50	6600,0	6800,II 6910,II
GD0	REAL*8		6640,0	
GFOM	REAL*8		6600,0	
GG1	REAL*8		6640,0	6800,S

NLTERM

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
GG2	REAL*8		6640,0	6810,S
I	INTEGER		6730,S	6740,U
IDCNE	INTEGER		6560,0	
IDELF	INTEGER		6560,0	
IT	INTEGER		6950,S	6960,U 6990,U 7000,U
IPRINT	INTEGER		6660,0	
ITAM	INTEGER		6530,U	6920,U 6920,U 6920,U 6920,U 6930,P
T1	INTEGER		6720,S 6810,U	6770,U 6770,U 6780,U 6780,U 6790,U 6820,U 6820,U 6830,U 6830,U 6870,P
JJ	INTEGER		6970,S	6980,U 6990,U 7000,U
KA	INTEGER		6960,S	6980,U
KK	INTEGER		6980,S	6990,U 6990,U 7000,U
LL	INTEGER		6650,0	
N	INTEGER		6550,0	
NCLST	INTEGER		6650,0	6930,U
NFLMS	INTEGER		6550,0	6760,U
NEQ	INTEGER		6550,0	6960,U
NEQT	INTEGER		6550,0	6730,U
NH	INTEGER		6550,0	6950,U
NHNS	INTEGER		6550,0	
NLTERM	INTEGER		6530,0	
NLTRMS	INTEGER		6620,0	
NN	INTEGER		6550,0	
NNODES	INTEGER		6550,0	
NOIT	INTEGER		6660,0	6930,U
NPRTF	INTEGER		6560,0	
NPRTL	INTEGER		6560,0	

NLTERM

VARTABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
NPRNTQ	INTEGER			6550,0
NSTEF	INTEGER			6550,0
NSTRSS	INTEGER			6650,0 6910,U 6920,U 6920,U 6930,U
NTHETA	INTEGER			6650,0
PH	REAL#8	50		6610,0
DHD	REAL#8	50		6610,0
PRINT	REAL#8			6660,0
QV	REAL#8	1020		6580,0
QV1	REAL#8	1020		6580,0
QV2	REAL#8	1020		6580,0
QP	REAL#8	1020	6590,0	6740,S 6990,S 6990,U 7000,S
QPR	REAL#8	8,5	6630,0	6990,U 7000,U
QPRIME	REAL#8			6870,U
QPT	REAL#8	1020		6580,0
QS	REAL#8			6580,0
R	REAL#8	50		6610,0
STNF	REAL#8	51		6670,0
STMN	REAL#8	50		6610,0
STRESS	REAL#8			6930,U
T	REAL#8	50	6600,0	6780,U 6790,U 6800,U 6910,U 6820,U 6830,U
THETA	REAL#8	20		6650,0
THETAS	REAL#8			6650,0
TIME	REAL#8			6570,0
TMFT	REAL#8			6570,0
TOTIME	REAL#8			6570,0
TA	REAL#8			6570,0

NLTFRM

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHFRF/HOW USED
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T1	REAL*8		6570,0	
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VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
CONST	REAL*8	10280,0		
DT2	REAL*8	10280,0		
FORCE	REAL*8	204	10270,0 10720,S	
I	INTEGER		10420,S 10440,U 10440,U 10440,U 10470,S 10480,U 10480,U 10480,U 10540,S 10550,U 10570,U 10570,U 10570,U 10570,U 10610,S 10620,U 10620,U 10620,U 10620,U 10690,S 10700,U 10700,U 10700,U 10700,U 10800,S 10810,U	
IDCINF	INTEGER	10280,0		
IDELF	INTEGER	10280,0		
IELM	INTEGER		10400,S 10410,U 10540,U 10570,U 10590,U 10620,U 10620,U 10640,U 10660,U 10670,S 10670,U 10700,U	
J	INTEGER		10430,S 10440,U 10460,S 10480,U 10560,S 10570,U 10590,S 10620,U 10640,U 10680,S 10680,U 10700,U	
K	INTEGER		10440,S 10450,U 10480,S 10490,U 10500,S 10510,U 10570,S 10580,U 10620,S 10630,U 10640,S 10650,U 10700,S 10710,U 10810,S 10820,U	
KY	INTEGER	10250,U 10360,U 10780,U		
L	INTEGER	10380,S 10390,U		
LK	INTEGER	204	10300,0 10300,U	
M	INTEGER	10280,0		
N	INTEGER		10550,S 10560,U 10600,S 10610,U 10640,U 10640,U 10640,U 10640,U	
NCLOSE	INTEGER	10300,0	10350,U	
NELEMS	INTEGER	10280,0	10660,U	
NEQ	INTEGER		10300,U 10400,U 10420,U 10430,U 10460,U 10470,U 10500,U 10500,U 10500,U 10500,U 10540,U 10590,U 10600,U 10720,U	
NEQT	INTEGER	10280,0		
NH	INTEGER	10280,0		
NHNS	INTEGER	10280,0		
NTX	INTEGER	10280,0		
NN	INTEGER		10280,0 10440,U 10480,U 10500,U 10570,U 10620,U 10640,U 10700,U	
NNODES	INTEGER	10280,0	10800,U	

NREFSTR

VARIABLE	INITIAL	TYPE	VAL IF	DIMENSION	WHERE/HOW USED
NODRE		INTEGER			10350,S 10360,S 10360,U 10370,U 10380,U
NODRES		INTEGER			10370,D 10350,U
NPRNTF		INTEGER			10290,D
NPRNTL		INTEGER			10290,D
NPRNTD		INTEGER			10280,D
NREFSTR		INTEGER			10250,D
NSIZE		INTEGER			10280,D
RSTRNT		REAL*			10370,D
SIVFF0		REAL**			10270,D
STITEM		REAL**		6550	10270,D 10450,S 10490,S 10510,S 10580,S 10630,S 10650,S 10710,S 10790,S 10820,S

OPP TIME

VARTABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
ALS	REAL*8	50	7170,0	8820,U 8830,U
ALT	REAL*8	50	7170,0	8820,U 8830,U
APCL	REAL*8	50	7140,0	
ARCLT	REAL*8		7380,S	7440,U 7450,U 7460,U 7470,U 7480,U 7490,U
APL	REAL*8		7330,S	7340,U 7350,II 7380,U 7900,U 8670,U
CCC	REAL*8	125	7090,0	8100,U 8120,U 9150,U 8820,U
CCCC	REAL*8	625	7100,0	9520,U
CC1	REAL*8		7150,0	8100,U 8120,II 8150,U 8170,U 8510,U 8520,U 8820,U
CC2	REAL*8		7150,0	8120,U 8170,U 9540,U 8830,U
CES	REAL*8		7920,S	8100,S 8100,II 8210,U 8240,U 8260,U 8290,U
CFST	REAL*8		7940,S	8140,S 8140,U 8210,U 8230,U 8240,U 8260,U 8280,U 8290,U
CET	REAL*8		7930,S	9120,S 8130,II 8230,II 8240,U 8280,U 8290,U
CF13	REAL*8		7950,S 8850,U	8150,S 8160,U 8210,U 8240,U 8260,U 8290,U 9690,S 8820,S 8820,U
CF23	REAL*8		7960,S 8820,S	8170,S 8180,U 8210,U 8230,U 8240,U 8260,U 8280,U 8290,U 8700,S
CF413	REAL*8		8340,S	8520,S 8520,S 8580,U 8600,U 8610,U 8630,U
CF423	REAL*8		8350,S	8540,S 8540,U 8580,U 8590,U 8600,U 8610,U 8620,U 8630,U
FL29	REAL*8		7570,S	7650,U
CONST	REAL*8		7070,0	
COPH	REAL*8		7350,S	7420,U 7450,U 7470,U 7550,U 7570,U
COSTNE	REAL*8	51	7140,0	
COSM	REAL*8	50	7140,0	
CO2R	REAL*8		7550,S	7630,U
CS	REAL*8		7090,0	
CS5	REAL*8	125	7090,0	8140,U 8170,U 8830,II
CS4	REAL*8		7100,0	

OPRTM

VARIABLE	TYPE	INITIAL VALIF	DIMENSION	WHERE/HOW USED
DD1	REAL*8			7150,0
DD2	REAL*8			7150,0
DELT	REAL*8			7190,0
DR0	REAL*8			7310,S 7330,U 7330,U 7340,U
DSORT	REAL*8			7230,II
DTH	REAL*8	50,5,2		7170,0
D*2	REAL*8			7070,0
DZ	REAL*8			7320,S 7330,U 7330,U 7350,U
EFS	REAL*8			7110,0
ES	REAL*8	5		7110,0 7820,S 8150,II 8170,II
ES01	REAL*8			7500,S 7820,U 8210,U
ES03	REAL*8			7510,S 7820,II 8240,U
ES05	REAL*8			7520,S 7820,U 8260,U
ES07	REAL*8			7530,S 7820,II 8290,U
FST	REAL*8	5		7110,0 7830,S 8160,U 8180,II
FST01	REAL*8	5		7230,0 7660,S 7830,II 8210,II
FST02	REAL*8			7480,S 7830,U 8230,U
FST03	REAL*8	5		7230,0 7670,S 7830,II 8240,U
FST05	REAL*8	5		7240,0 7680,S 7830,II 8260,U
FST06	REAL*8			7490,S 7840,II 8290,U
FST07	REAL*8	5		7240,0 7690,S 7840,II 8290,II
FT	REAL*8	5		7110,0 7800,S 8150,II 8170,II
FT02	REAL*8	5		7240,0 7700,S 7710,II 7800,U 8230,U
FT03	REAL*8			7400,S 7800,II 8240,II
FT06	REAL*8	5		7240,0 7710,S 7800,II 8280,U
FT07	REAL*8			7410,S 7800,II 8290,U

OPPTIME

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
E1	REAL*8		50	7130,0
F13	REAL*8		5	7110,0 7850,S 8100,U 8170,U 8120,U 8120,U 8140,U 8150,U 8170,U 8510,U 8520,U 8520,U 8520,U 8540,U 8540,U 8820,U
F1301	REAL*8		7440,S	7510,U 7850,U 8210,U 8580,U 8860,U
F1303	REAL*8		7450,S	7500,U 7850,U 8240,U 8600,U 8880,U
F1305	REAL*8		7460,S	7530,U 7850,U 8260,U 8610,U 8890,U
F1307	REAL*8		7470,S	7520,U 7850,U 8290,U 8630,U 8910,U
F2	REAL*8		50	7130,0
F23	REAL*8		5	7110,0 7860,S 8100,U 8170,U 8120,U 8120,U 8140,U 8160,U 8170,U 8510,U 8520,U 8540,U 8540,U 8540,U 8830,U
F2301	REAL*8		5	7230,0 7620,S 7670,U 7860,U 8210,U 8580,U 8860,U
F2302	REAL*8		7420,S	7430,U 7860,U 8230,U 8590,U 8870,U
F2303	REAL*8		5	7230,0 7630,S 7660,U 7860,U 8240,U 8600,U 8880,U
F2305	REAL*8		5	7230,0 7640,S 7690,U 7860,U 8260,U 8610,U 8890,U
F2306	REAL*8		7430,S	7870,U 8280,U 8620,U 8900,U
F2307	REAL*8		5	7230,0 7650,S 7680,U 7870,U 8290,U 8630,U 8910,U
ENIJ1	REAL*8		50	7130,0 8100,U 8120,U 8150,U 8170,U 8510,U 8820,U
ENIJ2	REAL*8		50	7130,0 8830,U
FOR	REAL*8		8510,S	8520,U 8540,U
FORCE	REAL*8	2040	7200,0	
G	REAL*8	50	7130,0	
GCD	REAL*8		7150,0	
GEOM	REAL*8		7130,0	
GG1	REAL*8		7150,0	8140,U 8150,U 8170,U 8510,U
GG2	REAL*8		7150,0	
HARM	REAL*8		7160,0	

OPTION

VARIABLE TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
T	INTEGER		7980,S 8150,U 8820,II 8830,U 7990,U 8170,II 8180,U 8370,S 8380,U 8510,U 8120,U 8120,U 8140,U 8150,U 8730,U
TABS	INTEGER		8070,U 8420,II 8460,U 9780,II
TDCOF	INTEGER		7080,D
TELF	INTEGER		7080,D
TFO	INTEGER		8320,S 8400,S 8400,U 8520,U 8520,U 8540,II 8540,U
TH	INTEGER		7500,S 7600,U 7680,II 7700,II 7800,U 7820,II 7830,U 7860,U 7620,II 7630,II 7640,U 7650,U 7660,U 7660,U 7710,U 7730,U 7800,U 7860,U 7870,U 7870,U
THARM	INTEGER	5	7160,D 8730,II 8750,U 7600,II 7970,U 9020,U 8040,U 8360,U 8380,U 8400,U 8440,U 8710,U
TI	INTEGER		8020,S 8050,II 8060,U 8380,S 8410,U 8420,U 8730,S 8760,U 8770,U
TMJ	INTEGER		8060,S 8070,U 8420,S 8470,U 8470,U 8770,S 8780,U
TPJ	INTEGER		8050,S 8070,U 8410,S 9470,U 8470,U 8760,S 8780,U
TCDF	INTEGER		7180,D
TELF	INTEGER		7180,D 8650,II
TH	INTEGER		7800,S 8080,S 8170,II 8660,S 8800,S 8820,U 8830,U 8120,U 8120,U 8140,U 8150,U 8150,U
II	INTEGER		7050,II 8700,U 7290,II 8700,II 7300,U 7730,U 8120,U 8120,U 8150,U 8170,U 8510,U 8790,U
J	INTEGER		8030,S 8170,II 8170,U 8750,U 8790,U 8100,II 8170,II 8300,S 8470,U 8120,U 8120,U 8140,U 8150,U 8150,U 8160,U 8740,S
JJ	INTEGER		8040,S 8050,U 8260,U 9470,S 8610,U 8420,U 8750,S 8760,U 8770,U
J1	INTEGER		7290,S 7310,U 7320,U 7360,U
J11	INTEGER		7380,II 7310,II 7320,U 7360,II
K	INTEGER		7600,S 8710,S 8780,II 7610,II 7970,S 8370,II 8370,U 8430,S 8440,U 8510,U 8520,U 8540,U
KK	INTEGER		7730,S 7740,II 7750,U 7760,U 7770,U 7780,U 7790,U 8440,S 8450,U 8460,U

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OPTIMF

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VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
KK1	INTEGER	7740,U	7820,U	7830,U 7850,U 7860,U
KK2	INTEGER	7750,S	7800,U	7830,U 7860,U
KK3	INTEGER	7760,S	7800,U	7820,U 7830,U 7850,U 7860,U
KK5	INTEGER	7770,S	7820,U	7840,U 7850,U 7870,U
KK6	INTEGER	7780,S	7800,U	7840,U 7870,U
KK7	INTEGER	7790,S	7800,U	7820,U 7840,U 7850,U 7870,U
KML	INTEGER	8460,S	8470,U	9470,U
KPI	INTEGER	8450,S	8470,U	8470,U
L	INTEGER	8330,S 8610,U	8360,U 8610,U	8580,U 8580,U 8590,U 8590,U 8600,U 8600,U 8600,U
LL	INTEGER	8360,S	8450,U	8460,U
M	INTEGER	7910,S 8240,U 8280,U 8870,U 8910,U	7970,U 8240,U 8290,U 8870,U 8910,U	7990,U 8210,U 8210,U 8220,U 8230,U 8230,U 8230,U 8240,U 8250,U 8260,U 8260,U 8270,U 8280,U 8280,U 8290,U 8290,U 8300,U 8680,U 8710,U 8860,U 8860,U 8870,U 8880,U 8880,U 8890,U 8890,U 8890,U 8890,U 8910,U 8910,U 8910,U 8910,U 8910,U 8910,U 8910,U
N	INTEGER	7070,D		
NFLEMS	INTEGER	7070,D		
NFO	INTEGER	7070,D	7730,U	
NFOT	INTEGER	7070,D		
NH	INTEGER	7070,D 8720,U	7590,U 8740,U	8010,U 8030,U 8330,U 8370,U 8390,U 8430,U 8680,U
NHNS	INTEGER	7070,D		
NHD	INTEGER	7160,D		
NLTRMS	INTEGER	7120,D		
NN	INTEGER	7070,D		
NNODES	INTEGER	7070,D		
NPRNTF	INTEGER	7080,D		
NPRNTH	INTEGER	7190,D		

QPRIME

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
NPRNTL	INTEGER		7080,0	
NPRNTO	INTEGER		7070,0	
NSIZE	INTEGER		7070,0	
PH	REAL*8	50	7140,0	
PHP	REAL*8	50	7140,0	
QN	REAL*8	1020	7200,0 7830,0 7860,0	7800,U 7830,U 7860,U 7800,U 7830,U 7860,U 7800,U 7830,U 7860,U 7800,U 7830,U 7860,U 7800,U 7830,U 7860,U
QN1	REAL*8	1020	7200,0	
QN2	REAL*8	1020	7200,0	
QP	REAL*8	1020	7200,0	
QPO	REAL*8	8,5	7120,0 8280,S 9610,S 9890,S	7900,S 8290,U 8610,U 9890,U 8210,S 8290,S 8620,S 9890,S 8210,U 8290,U 8620,U 9890,U 8230,S 8580,U 8630,S 8900,S 8230,U 8590,S 8630,U 8900,U 8240,S 8590,U 8630,S 8910,S 8250,U 8590,U 8630,U 8910,U
QPRIME	REAL*8		7050,0	
QPI	REAL*8	1020	7200,0	
QS	REAL*8		7200,0	
R	REAL*8	50	7140,0	
RL	REAL*8		8670,S	8860,U 8870,U 8880,U 8890,U 8900,U 8910,U
RM	REAL*8		7360,S	7370,U 7900,U 8670,U
RC	REAL*8	51	7220,0	7310,U 7360,U 7360,U
RCL	REAL*8		7900,S 8610,U	8210,U 8620,U 8230,U 9630,U 8250,U 8260,U 8280,U 8300,U 8580,U 8590,U 8600,U
R7	REAL*8		7220,0	
R21	REAL*8		7370,S 7770,U	7400,U 7410,U 7420,U 7480,U 7490,U 7550,U 7560,U 7570,U 7580,U
SCCS	REAL*8	625	7100,0	8540,U
STNF	REAL*8	51	7130,0	
STNM	REAL*8	50	7140,0	

OPTIME

VARIABLE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
SIPH	REAL#8		7340,S 7440,U 7460,II 7480,U 7490,U 7560,U 7580,U
SL2R	REAL#8		7560,S 7640,II
SO2R	REAL#8		7580,S 7620,II
SSC	REAL#8	125	7090,D 8100,II 8120,U 8150,U
SSCC	REAL#8	625	7100,D 8520,U
SSSS	REAL#8	625	7100,D 8540,U
T	REAL#8	50	7130,D
TH	REAL#P	50,5,2	7170,D 8790,II 8790,II 8790,U
T4CON	REAL#8		7180,D
THFR	REAL#8		7170,D
THT	REAL#8		8700,S 8820,II 8830,U
TIME	REAL#8		7190,D 8790,U
THFT	REAL#8		7190,D
TOTIME	REAL#8		7190,D
TT	REAL#8		7190,D 8790,II 8790,II
T1	REAL#8		7190,D 8790,U
XX	REAL#8		7610,S 7620,U 7630,U 7640,U 7650,U 7700,U
Z	REAL#8	51	7220,D 7320,II 7320,II

SETUP

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
C01	REAL*8		5730,D	
C02	REAL*8		5730,D	
CONST	REAL*8		5710,D	
CS	REAL*8		6120,S 6180,U	
DABS	REAL*8		6330,U	
DCOS	REAL*8		6120,U	
DD1	REAL*8		5730,D	
DD2	REAL*8		5730,D	
DFLTDP	REAL*8		5770,D	
DETN	REAL*8		6110,U	
DT2	REAL*8		5710,D	
FORCE	REAL*8	2040	5690,D	
GCD	REAL*8		5730,D	
GG1	REAL*8		5730,D	
GG2	REAL*8		5730,D	
HARM	REAL*8		5760,D	
HOUJBO1	REAL*8		5980,U	
HOUJBO2	REAL*8		5870,U	
I	INTEGER		5960,S 5970,U 5980,U 6060,S 6070,U 6250,S 6260,U 6270,U	
IDCODE	INTEGER		5720,D	
IDFLF	INTEGER		5720,D	
TH	INTEGER		5830,S 5840,U 5950,U 5860,U 5870,P 5880,P 6000,U	
THARM	INTEGER	5	5760,D 5840,U 6100,U	
INPJT	INTEGER		6400,U	
IPRINT	INTEGER		5750,D 5890,U 5890,U	
FRSTRT	INTEGER		5770,D	

SETUP

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED																
IT	INTEGER	5890,S	5910,U	6050,S	6110,U	6120,U	6230,U													
ITAM	INTEGER		5660,U	5820,U	5820,P	5970,U	5880,U	5890,U	5890,U	5900,U	5910,U	5940,U								
ITD	INTEGER		5220,U	6350,U	6350,U	6390,U														
ITI	INTEGER		5770,D																	
ITJ	INTEGER		6390,S	6400,U																
II	INTEGER		6130,S	6140,U																
J	INTEGER		5980,U	5990,S	6160,S	6170,U	6180,U	6180,U	6180,U	6200,U	6200,U	6200,U								
JH	INTEGER		5270,U	6270,U																
K	INTEGER		6080,S	6090,S	6100,U															
KY	INTEGER		5970,S	5980,U	6140,S	6150,U	6180,U	6180,U	6200,U	6200,U	6260,S	6270,U								
LARGE	INTEGER		5660,U	6340,S																
LF	INTEGER		6330,U																	
LL	INTEGER		5750,D	5820,U	5870,U	5880,U														
N	INTEGER		5710,D	5860,S	5970,U	6000,S	6150,U	6330,U												
NFCST	INTEGER		5740,D																	
NFLEMS	INTEGER		5710,D																	
NEQ	INTEGER		5710,D	5860,U	6060,U	6090,U														
NEQT	INTEGER		5710,D																	
NH	INTEGER		5710,D	5830,U	6000,U	6010,U	6080,U													
MHNS	INTEGER		5710,D																	
NHD	INTEGER		5760,D																	
NLTERM	INTEGER		5820,U																	
NN	INTEGER		5710,D	5850,S																
NNODES	INTEGER		5710,D	5960,U	6130,U	6250,U														
NOIT	INTEGER		5750,D	5900,U																
NDK	INTEGER		6150,S	6180,U	6200,U															

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SETUP

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
NPRNTT	INTEGER		5770,D	6390,U 6390,U
NPRNT	INTEGER		5770,D	6390,U 6400,U
NPRNTF	INTEGER		5720,D	
NPRNTL	INTEGER		5720,D	
NPRNTQ	INTEGER		5710,D	5920,U
NCIZE	INTEGER		5710,D	5850,U
NSTRSS	INTEGER		5740,D	
NTHETA	INTEGER		5740,D	6050,U
PRINT	REAL*8		5750,D	
Q1Q2D	REAL*8	204	5680,D	6070,S 6180,S 6180,U 6200,S 6200,U 6270,U
Q1	REAL*8	1020	5680,D	5980,U 6180,U 6200,U 6330,U
Q11	REAL*8	1020	5680,D	
Q12	REAL*8	1020	5680,D	
QP	REAL*8	1020	5680,D	
QPI	REAL*8	1020	5680,D	
QS	REAL*8		5680,D	
RESTRT	REAL*8		5770,D	
SETUP	REAL*8		5680,D	
SOLVE0	REAL*8		5680,D	
SN	REAL*8		6110,S	6200,U
THETA	REAL*8	20	5740,D	6110,U 6120,U 6230,U
THETAS	REAL*8		5740,D	
THETAI	REAL*8		6230,S	6240,U
TIME	REAL*8		5660,U	5930,U 6350,U
TMFP	REAL*8		5770,D	
TPRNT	REAL*8		5930,S	5940,U 6220,U

SETUP

VARIABLE	TYPE	INITIAL VALUE	DIMENSTON	WHERE/HOW USED
XTH1	REAL*8		6100,S	6110,U 6120,U
XV	REAL*8		6550	5680,D

SOLVED

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
A	REAL*8		1310	11310,0 11410,S 11460,S 11460,U 11460,U 11470,S 11470,U 11470,U 11470,U 11470,U 11480,S 11490,U 11480,U 11480,U 11490,S 11490,U 11490,U 11490,U 11490,U 11490,U 11500,U 11510,S 11510,U 11510,U 11520,S 11520,U 11520,U 11520,U 11520,U 11520,U 11520,U 11530,S 11530,U 11530,U 11530,U 11530,U 11530,U 11530,U 11530,U 11530,U 11540,U 11550,S 11550,U 11550,U 11560,S 11560,U 11560,U 11560,U 11560,U 11560,U 11570,U 11570,U 11570,U 11570,U 11570,U 11570,U 11570,U 11570,U 11570,U 11570,U 11580,U 11590,U 11600,U 11600,U 11600,U 11650,U 11650,U 11650,U 11650,U 11650,U 11660,U 11670,U 11680,U 11690,U 11700,U 11710,U 11720,U 11730,U 11740,U 11750,U 11760,U 11770,U 11780,U 11790,U 11800,U 11810,U 11820,U 11830,U 11840,U 11850,U 11860,U 11870,U 11880,U 11890,U 11900,U 11910,U 11920,U 11930,U 11940,U 11950,U 11960,U 11970,U 11980,U 11990,U 12000,U 12010,U 12020,U 12030,U 12040,U 12050,U 12060,U 12070,U 12080,U 12090,U 12100,U 12110,U 12120,U 12130,U 12140,U 12150,U 12160,U 12170,U 12180,U 12190,U 12200,U 12210,U 12220,U 12230,U 12240,U 12250,U 12260,U 12270,U 12280,U 12290,U 12300,U 12310,U 12320,U 12330,U 12340,U 12350,U 12360,U 12370,U 12380,U 12390,U 12400,U 12410,U 12420,U 12430,U 12440,U 12450,U 12460,U 12470,U 12480,U 12490,U 12500,U 12510,U 12520,U 12530,U 12540,U 12550,U AM1 REAL*8 11910,U 12230,U 12310,U 12330,U 12400,U 12430,U 12510,U 12550,U 12770,U AM10 REAL*8 11650,S 11720,S 12200,U 12230,U 12280,U 12330,U 12370,U 12430,U 12480,U 12550,U 12600,U 12680,U AM2 REAL*8 11800,S 12160,U 12170,U 12180,U 12190,U 12760,U AM3 REAL*8 11790,S 12160,U 12170,U 12180,U 12190,U 12750,U AM4 REAL*8 11780,S 12160,U 12170,U 12180,U 12190,U 12740,U AM5 REAL*8 11720,S 11770,S 12220,U 12230,U 12300,U 12330,U 12390,U 12430,U 12500,U 12550,U 12650,U 12730,U AM6 REAL*8 11690,S 11760,S 12120,U 12130,U 12140,U 12150,U 12640,U 12720,U AM7 REAL*8 11680,S 11750,S 12120,U 12130,U 12140,U 12150,U 12630,U 12710,U AM8 REAL*8 11670,S 11740,S 12210,U 12230,U 12290,U 12330,U 12380,U 12430,U 12490,U 12550,U 12620,U 12710,U AM9 REAL*8 11660,S 11730,S 12080,U 12090,U 12100,U 12110,U 12610,U 12690,U AT REAL*8 11820,S 12090,U 12120,U 12160,U 12220,S 12230,U 12230,U 12240,U 12250,U 12260,U 12270,U 12780,U

SOLVED

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
A1	REAL*8			11830,S 12080,S 12080,U 12120,U 12160,U 12210,S 12210,S 12230,U 12230,U 12240,U 12250,U 12260,U 12270,U 12270,U
A10	REAL*8			11920,S 12330,S 12330,U 12420,U 12440,U 12530,U 12560,U 12880,U
A11	REAL*8			11930,S 12120,U 12140,U 12180,U 12250,U 12340,U 12370,S 12370,U 12430,U 12430,U 12450,U 12460,U 12490,U
A12	REAL*8			11940,S 12100,S 12100,U 12140,U 12180,U 12250,U 12340,U 12380,S 12380,U 12430,U 12430,U 12450,U 12460,U 12490,U
A13	REAL*8			11950,S 12140,S 12140,U 12180,U 12250,U 12340,U 12390,S 12390,U 12430,U 12430,U 12450,U 12460,U 12490,U
A14	REAL*8			11960,S 12180,S 12180,U 12250,U 12340,U 12400,S 12400,U 12430,U 12430,U 12450,U 12460,U 12490,U
A15	REAL*8			11970,S 12250,S 12250,U 12240,U 12410,S 12410,U 12430,U 12430,U 12450,U 12460,U 12490,U
A16	REAL*8			11990,S 12340,S 12340,U 12420,S 12420,U 12440,U 12440,U 12450,U 12470,U 12940,U
A17	REAL*8			11990,S 12430,S 12430,U 12540,U 12560,U 12950,U
A18	REAL*8			12000,S 12110,U 12150,U 12190,U 12260,U 12350,U 12450,U 12480,S 12480,U 12550,U 12550,U 12570,U 12960,U
A19	REAL*8			12010,S 12110,S 12110,U 12150,U 12190,U 12260,U 12350,U 12450,U 12490,S 12490,U 12550,U 12550,U 12570,U 12970,U
A2	REAL*8			11840,S 12120,S 12120,U 12160,U 12220,S 12220,U 12230,U 12230,U 12240,U 12250,U 12260,U 12270,U 12880,U
A20	REAL*8			12020,S 12150,S 12150,U 12190,U 12260,U 12350,U 12450,U 12500,S 12500,U 12550,U 12550,U 12570,U 12980,U
A21	REAL*8			12030,S 12190,S 12190,U 12260,U 12350,U 12450,U 12510,S 12510,U 12550,U 12550,U 12570,U 12990,U
A22	REAL*8			12040,S 12260,S 12260,U 12350,U 12450,U 12520,S 12520,U 12550,U 12550,U 12570,U 13000,U
A23	REAL*8			12050,S 12350,S 12350,U 12450,U 12530,S 12530,U 12560,U 12560,U 12580,U 13010,U
A24	REAL*8			12060,S 12450,S 12450,U 12540,S 12540,U 12560,U 12560,U 12580,U 13020,U
A25	REAL*8			12070,S 12550,S 12550,U 13130,U
A3	REAL*8			11850,S 12160,S 12160,U 12230,U 12230,U 12240,U 12250,U 12260,U 12270,U 12810,U

SOLVEQ

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
A4	REAL*8		11860,S	12230,S 12230,U 12320,U 12330,U 12410,U 12430,U 12520,U 12550,U 12820,U
A5	REAL*8		11870,S 12350,U	12090,U 12130,II 12170,U 12240,U 12280,S 12280,U 12330,U 12330,U 12340,U 12360,II 12830,U
A6	REAL*8		11890,S 12340,U	12090,S 12130,II 12170,U 12240,U 12290,S 12290,U 12330,U 12330,U 12350,II 12840,U
A7	REAL*8		11890,S 12350,U	12130,S 12170,U 12240,U 12300,S 12300,U 12330,U 12330,U 12340,U 12360,II 12850,U
A8	REAL*8		11900,S 12360,U	12170,S 12240,II 12310,S 12310,U 12330,U 12330,U 12340,U 12350,U 12860,II
A9	REAL*8		11910,S 12870,U	12240,S 12240,II 12320,S 12320,U 12330,U 12330,U 12340,U 12350,U 12870,U
CONST	REAL*8		11270,D	
CYCLE	REAL*8		11300,D	
DT2	REAL*8		11270,D	
I	INTEGER		11390,S 11690,II 11790,U 11890,II 11900,II 12000,U 12610,II 12730,U 12830,U 12930,U 13030,II	11400,U 11410,U 11420,S 11430,U 11430,U 11620,S 11650,U 11660,U 11670,U 11690,U 11700,U 11720,U 11730,U 11740,U 11750,U 11760,U 11770,U 11780,U 11790,U 11800,II 11810,U 11820,U 11830,U 11840,U 11850,U 11860,U 11870,U 11880,U 11890,II 11900,II 11910,U 11920,U 11930,U 11940,U 11950,U 11960,U 11970,U 11980,U 11990,II 12000,U 12010,II 12020,U 12030,U 12040,U 12050,II 12060,U 12070,U 12080,U 12620,II 12630,U 12640,II 12650,U 12660,U 12670,U 12680,U 12690,U 12700,U 12710,U 12720,U 12750,U 12760,U 12770,U 12780,U 12790,U 12790,U 12800,U 12810,U 12820,U 12850,II 12860,U 12870,U 12880,U 12890,U 12890,U 12900,U 12910,U 12920,U 12950,U 12960,U 12970,U 12980,U 12990,U 12990,U 13000,U 13010,U 13020,U 13500,S 13510,II 13510,U 13520,S 13540,U 13550,U
IDCNE	INTEGER		11280,D	
IDEF	INTEGER		11280,D	
TH	INTEGER		11240,D	
TPRINT	INTEGER		11290,D	
TTAM	INTEGER		11300,D	11440,II 13520,U
J	INTEGER		11630,S 12360,II 12460,II 12560,II	12270,II 12270,II 12270,II 12270,II 12270,U 12270,U 12270,U 12270,U 12360,U 12360,II 12360,U 12360,U 12460,U 12460,U 12460,U 12460,U 12460,II 12470,U 12570,U 12570,U 12570,U 12570,U 12570,U 12570,U 12570,U
K	INTEGER		11610,S	11620,U 11630,U 13090,S 13100,U 13110,U 13280,S 13290,U 13300,U

SOLVED

VARIABLE TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED						
KFY	INTEGER	11450,S	11640,U 12590,U 12660,S						
L	INTEGER	13110,U 13150,U 13180,U 13240,U 13370,U 13390,U 13440,U 13470,U	13120,U 13150,U 13180,U 13340,U 13370,U 13410,U 13440,U 13470,U	13120,U 13160,U 13290,S 13340,U 13370,U 13410,U 13450,U 13470,U	13130,S 13160,U 13300,U 13350,U 13380,U 13410,U 13450,U 13480,U	13130,U 13170,U 13320,U 13360,U 13380,U 13420,U 13460,U 13480,U	13130,U 13170,U 13320,U 13360,U 13390,U 13430,U 13460,U 13470,U	13140,U 13180,U 13180,U 13330,U 13360,U 13390,U 13430,U 13470,U	
LL	INTEGER	11290,S	11440,U 13520,U						
M	INTEGER	13230,S 13270,U	13240,U 13270,U	13250,U 13270,S	13250,U 13270,U	13260,U	13260,U	13260,U	13260,U
N	INTEGER	13100,U 13130,U 13160,U 13180,U 13270,U 13340,U 13360,U 13390,U 13430,U 13450,U 13480,U	13120,U 13130,U 13160,U 13220,S 13270,U 13340,U 13370,U 13390,U 13430,U 13450,U 13480,U	13120,U 13140,U 13170,U 13240,U 13320,U 13340,U 13370,U 13390,U 13410,U 13460,U 13480,U	13120,U 13150,U 13170,U 13250,U 13320,U 13350,U 13380,U 13410,U 13470,U 13480,U	13130,U 13150,U 13170,U 13260,U 13320,U 13360,U 13380,U 13410,U 13470,U 13480,U	13130,U 13150,U 13180,U 13270,U 13330,U 13360,U 13380,U 13420,U 13470,U 13470,U	13130,U 13150,U 13180,U 13270,U 13330,U 13360,U 13380,U 13420,U 13470,U 13470,U	13140,U 13150,U 13180,U 13270,U 13330,U 13360,U 13380,U 13430,U 13470,U 13470,U
NELEMS	INTEGER	11270,U	11610,U 13090,U 13220,U 13230,U 13280,U 13290,U 13300,U						
NEO	INTEGER	11270,D	11420,U 13520,U						
NEOT	INTEGER	11270,D							
NH	INTEGER	11270,D							
NHNS	INTEGER	11270,D							
NN	INTEGER	11270,D	11400,U 13540,U						
NNODES	INTEGER	11270,D							
NNPT	INTEGER	11400,S 11410,U	13540,S 13550,S						
NOIT	INTEGER	11290,D							
NPRNTF	INTEGER	11280,D							
NPRNTL	INTEGER	11290,D							
NPRNTO	INTEGER	11270,D							

SQ1VRQ

STRESS

J-3-210

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
AAV	REAL*8			14590,S 14600,U 14620,U
ALS	REAL*8	50		13710,D 14000,U 14150,U
ALT	REAL*8	50		13710,D 14100,U 14180,U
ARCI	REAL*8	50		13650,D 14140,U 14210,U 14590,U 14590,U
RSL	REAL*8			14460,S 14550,U 14650,U
RSTL	REAL*8			14480,S 14550,II 14650,II
RSTMET	REAL*8	20		13720,S 14620,II 14630,II 14680,S
RSTRMS	REAL*8	20		13720,D 14600,II 14660,S
RSTRMT	REAL*8	20		13720,D 14610,II 14670,S
RSTMUT	REAL*8	20		13720,D 14620,II 14700,S
RSTU	REAL*8			14450,S 14550,U 14650,U
RCIJ	REAL*8			14430,S 14540,U 14650,U
RTL	REAL*8			14470,S 14550,U 14650,U
RTMNET	REAL*8	20		13720,D 14600,II 14690,S
RTIJ	REAL*8			14440,S 14540,U 14650,U
CC1	REAL*8			13660,D 14340,U 14340,U
CC2	REAL*8			13660,D 14350,II 14350,U
CHIS	REAL*8			13890,S 14160,S 14160,U 14370,U 14380,U
CHIST	REAL*8			13920,S 14240,S 14240,U 14390,U
CHIST1	REAL*8			14270,S 14240,II 14270,U
CHIS1	REAL*8			14140,S 14160,U 14250,U
CHIS2	REAL*8			14150,S 14160,II 14250,U
CHIT	REAL*8			13890,S 14190,S 14190,U 14370,U 14380,U
CHIT1	REAL*8			14170,S 14190,II 14260,U
CHIT2	REAL*8			14190,S 14190,II 14260,U
CONST	REAL*8			13610,D

STRESS

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
COSINE	REAL*8		51	13650,D 14120,U 14130,U
COS4	REAL*8		50	13650,D 14210,U 14220,U
CS	REAL*8			13980,S 14040,U 14050,U 14070,U 14090,U 14100,U 14160,U 14190,U 14270,U
CTHIS	REAL*8			13910,S 14250,S 14250,U 14500,U
CTHIST	REAL*8			13920,S 14270,S 14270,U 14510,U
CTHIT	REAL*8			13920,S 14260,S 14260,U 14500,U
CIST	REAL*8			14410,S 14430,U 14440,U 14450,U 14460,U 14470,U 14480,U
CPST	REAL*8			14420,S 14430,U 14440,U 14450,U 14460,U 14470,U 14480,U
DCDS	REAL*8			13080,U
DD1	REAL*8			13660,D 14370,U 14370,U
DD2	REAL*8			13660,D 14380,U 14380,U 14500,U 14500,U
DELTF	REAL*8			13680,D 13790,U
DNIN	REAL*8			13900,U 14610,U 14630,U
DTH	REAL*8	50,5,2	13710,D 14020,U 14020,U 14120,U	
DTHT	REAL*8			14020,S 14150,U 14180,U
DT2	REAL*8			13610,D
EPS	REAL*8			13600,D
EPS	REAL*8			14300,S 14340,U 14350,U
EPST	REAL*8			14320,S 14360,U
EDT	REAL*8			14310,S 14340,U 14350,U
ES	REAL*8	5	13600,D 14040,U	
EST	REAL*8	5	13600,D 14060,U	
ESTIJ	REAL*8			13850,S 14060,S 14060,U 14120,U
ESIJ	REAL*8			13830,S 14040,S 14040,U 14300,U
ESIJT	REAL*8			13940,S 14090,S 14090,U 14300,U
ET	REAL*8	5	12670,D 14050,U	

STRESS

.. VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
ETU	REAL*8		13840,S	14050,S 14050,U 14310,U
ETUT	REAL*8		14170,S	14170,U 14310,U
F1	REAL*8	50	13640,D	
F13	REAL*8	5	13670,D	14070,U 14170,U 14200,U
F13U	REAL*8		13860,S	14070,S 14070,U 14300,U 14320,U
F2	REAL*8	50	13640,D	
F23	REAL*8	5	13670,D	14080,U 14170,U 14200,U
F23U	REAL*8		13870,S	14080,S 14080,U 14310,U 14320,U
FNU1	REAL*8	50	13640,D	14340,U 14370,U
FNU2	REAL*8	50	13640,D	14350,U 14380,U 14500,U
FORCE	REAL*8	2040	13680,D	
G	REAL*8	50	13640,D	
GCD	REAL*8		13660,D	
GFM	REAL*8		13640,D	
GG1	REAL*8		13660,D	14360,U
GG2	REAL*8		13660,D	14390,U 14510,U
HARM	REAL*8		13670,D	
I	INTEGER		13820,S 13980,U 13990,U 14520,U 14600,U 14600,U 14610,U 14620,U 14620,U 14630,U 14660,U 14670,U 14680,U 14690,U 14700,U	
IDCOF	INTEGER		13620,U	
IDELF	INTEGER		13620,D	
IH	INTEGER		13960,S 13970,U 14000,U 14010,U 14010,U 14010,U 14020,U 14020,U 14020,U 14040,U 14050,U 14060,U 14070,U 14080,U 14170,U 14170,U 14200,U 14200,U	
THARM	INTEGER	5	13670,D	13970,U
ITAM	INTEGER		13580,U	13780,U
ITAM1	INTEGER		13780,S	13810,U

STRESS

VARIABLE	INITIAL TYPE	VALUE	DIMENSION	WHERE/HOW USED
I1	INTEGER			13580,0 13810,0 14000,0 14010,0 14010,0 14020,0 14020,0 14020,0 14020,0 14020,0 14020,0 14020,0 14020,0 14020,0 14100,0 14120,0 14120,0 14130,0 14130,0 14140,0 14140,0 14150,0 14150,0 14170,0 14170,0 14170,0 14170,0 14180,0 14200,0 14200,0 14210,0 14210,0 14210,0 14210,0 14220,0 14220,0 14220,0 14220,0 14220,0 14220,0 14220,0 14220,0 14220,0 14340,0 14350,0 14370,0 14380,0 14410,0 14420,0 14500,0 14530,0 14540,0 14540,0 14540,0 14540,0 14540,0 14570,0 14570,0 14580,0 14580,0 14590,0 14590,0 14600,0 14600,0 14600,0 14600,0 14600,0 14600,0 14600,0 14600,0 14640,0
K	INTEGER			14070,0 14120,0 14120,0 14130,0 14130,0 14140,0 14140,0 14140,0 14140,0 14210,0 14210,0 14210,0 14210,0 14220,0
N	INTEGER			13610,0
NCLCST	INTEGER			13630,0
NELMS	INTEGER			13610,0
NEQ	INTEGER			13610,0 14000,0
NEOT	INTEGER			13610,0
NH	INTEGER			13610,0 13960,0
NHNS	INTEGER			13610,0
NHD	INTEGER			13670,0
NM	INTEGER			13610,0
NNODES	INTEGER			13610,0
NPRNTF	INTEGER			13620,0
NPRNTL	INTEGER			13620,0
NPRNTO	INTEGER			13610,0
NSTZF	INTEGER			13610,0
NSTRSS	INTEGER			13670,0
NTHETA	INTEGER			13630,0 13820,0
PAV	REAL*8			14580,0 14610,0 14630,0
PH	REAL*8	50		13650,0 14580,0 14580,0
PHD	REAL*8	50		13650,0 14220,0
QR3	REAL*8			14120,0 14200,0 14210,0
QR7	REAL*8			14130,0 14200,0 14210,0

STRESS

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
Q4	REAL**	1020	13600,0	14120,U 14120,II 14130,U 14130,II 14140,U 14140,II 14210,U 14210,II 14220,U 14220,II
QN1	REAL**	1020	13690,0	
QN2	REAL**	1020	13600,0	
QP	REAL**	1020	13600,0	
QP1	REAL**	1020	13600,0	
QS	REAL**		13690,0	
R	REAL**	50	13650,0	14170,U 14210,U 14220,II 14220,U 14570,U 14570,II 14600,U 14600,II 14620,U 14620,II
RAV	REAL**		14570,U	14600,U 14620,U
SHRS	REAL**		14600,S	14640,II
SHRT	REAL**		14620,S	14650,II
STNF	REAL**	51	13640,0	14120,II 14130,II
STNM	REAL**	50	13650,0	14170,II 14200,II 14200,U 14220,U
SM	REAL**		13900,S	14060,II 14080,U 14240,II 14250,U 14260,U
STRESS	REAL**		13580,0	
STRMS	REAL**		14370,S	14430,U 14460,II 14540,II 14600,II 14640,II 14660,U
STRUST	REAL**		14380,S	14450,U 14480,U 14540,II 14620,U 14630,U 14640,U 14680,U
STRUT	REAL**		14380,S	14440,U 14470,U 14540,II 14610,U 14640,U 14670,U
STRNC	REAL**		14340,S	14430,U 14460,U 14540,U 14640,U
STRNCT	REAL**		14360,S	14450,U 14480,U 14540,U 14640,U
STRNT	REAL**		14350,S	14440,U 14470,II 14540,II 14640,U
STMST	REAL**		14510,S	14600,II 14690,U
STTRMT	REAL**		14500,S	14620,II 14700,U
T	REAL**	50	13640,0	14410,II 14420,U
TH	REAL**	50,5,2	13710,0	14010,U 14010,II 14010,II
THFR	REAL**		13710,0	

STRESS

VARIABLE	INITIAL TYPE	VALUE	DIMENSION	WHERE/HOW USED
THETA	REAL*8		2^	13630,D 13980,U 13900,U 14520,U
THETAS	REAL*8			13630,D
THETAI	REAL*8			14520,S 14540,U 14640,U
TWT	REAL*8			14010,S 14000,U 14100,U
TIME	REAL*8			13680,D 13790,U 14010,U 14220,U
TMFT	REAL*8			13680,D
TM1	REAL*8			13790,S 13800,U
TOTIME	REAL*8			13680,D
TOPINT	REAL*8			13800,S 13910,U
T0	REAL*8			13680,D 14010,U 14010,U 14020,U 14020,U
T1	REAL*8			13680,D 14010,U 14020,U
XTHI	REAL*8			13970,S 13980,U 13990,U 14170,U 14200,U 14200,U 14210,U 14250,U 14260,U 14270,U

TENPCF

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
AL	REAL*8	167	16910,0 17290,U 17280,U 17290,U 17300,U 17300,U 17300,U 17310,U 17320,U 17320,U	17320,U 17330,U 17330,U 17340,U 17340,U 17340,U 17350,U 17350,U 17360,U 17360,U
			17360,U 17380,U 17380,U 17380,U 17380,U 17380,U 17390,U 17390,U 17400,U 17400,U	17380,U 17400,U 17420,U 17420,U
ALS	REAL*8	50	16890,U 17020,II 17050,U 17060,U 17090,U	
ALT	REAL*8	50	16890,D 17030,U 17040,II 17070,II 17080,U	
ARCL	REAL*8	50	16980,D 17150,U 17150,U 17160,U 17160,U 17160,U 17190,U 17190,U 17210,U 17210,U	
CFS	REAL*8	4	16070,D 17020,S 17040,S 17060,S 17080,S 17280,U 17280,U 17280,U 17300,U 17300,U	17300,U 17320,U 17320,U 17330,U 17330,U 17340,U 17340,U 17350,U 17360,U 17360,U
CHALS	REAL*8		16910,0	
CHECK	REAL*8	8,8	16910,0 17510,U	
CONST	REAL*8		16920,D	
COSTNE	REAL*8	51	16890,D	
COSM	REAL*8	50	16880,D	
DTH	REAL*8	50,5,2	16890,D 17270,II 17290,U 17310,U 17330,U 17350,U 17370,U 17390,U 17400,U 17420,U	
DT2	REAL*8		16920,D	
F1	REAL*8	50	16870,D 17020,U 17060,U	
F2	REAL*8	50	16870,D 17040,II 17080,U	
ENU1	REAL*8	50	16870,D 17020,II 17020,U 17040,U 17060,U 17070,U 17080,U	
ENU2	REAL*8	50	16870,D 17020,II 17040,U 17040,U 17060,U 17080,U 17090,U	
FORCE	REAL*8	2040	16940,D 17540,S 17540,U	
G	REAL*8	50	16970,D	
GFM	REAL*8		16870,D	
HARM	REAL*8		16900,D	
T	INTEGER		17480,S 17490,II 17510,U 17510,U 17520,S 17530,U 17540,U	
TR	INTEGER		16850,II 17230,U 17530,U	

TDFCFC

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
IPPI	INTEGER			17230,S 17270,U 17270,I 17280,I 17290,I 17300,U 17310,U 17320,U 17330,U 17340,U 17350,I 17360,U 17370,I 17380,U 17390,U 17400,U 17410,U 17420,U 17430,U
ICDF	INTEGER			16920,D
IDELF	INTEGER			16930,D
TELM	INTEGER			16850,I 17020,I 17020,U 17020,U 17020,U 17020,U 17020,U 17020,U 17020,U 17020,U 17040,U 17040,I 17040,U 17050,U 17050,U 17050,U 17050,U 17050,U 17050,U 17050,U 17070,I 17070,U 17080,U 17080,U 17080,U 17080,U 17080,U 17080,U 17080,U 17080,U 17140,U 17150,I 17150,U 17150,U 17150,U 17150,U 17150,U 17150,U 17150,U 17150,U 17160,U 17160,U 17160,U 17160,U 17160,U 17160,U 17160,U 17160,U 17160,U 17160,U 17180,U 17190,U 17190,U 17210,I 17210,U 17210,U 17210,U 17210,U 17210,U 17210,U 17220,U 17300,U 17310,U 17320,U 17330,U 17340,U 17350,U 17360,U 17370,U 17380,U 17390,U 17400,I 17400,U 17420,U 17420,U 17530,U
TH	INTEGER			17240,U 17250,U 17270,U 17270,U 17280,U 17290,U 17300,U 17310,U 17320,U 17330,U 17340,I 17350,I 17360,U 17370,U 17380,U 17390,U 17400,U 17410,U 17420,U 17430,U 17530,U
THAM	INTEGER	S	16900,D 17250,U	
J	INTEGER		17460,S 17470,I 17470,U 17500,S 17510,U 17510,U 17530,U 17540,U 17540,U	
KVP	INTEGER		17250,S 17260,U 17440,I	
N	INTEGER		16920,D	
NELMS	INTEGER		16920,D 17140,I	
NFO	INTEGER		16920,D 17530,U	
NFQT	INTEGER		16920,D 17530,U	
NH	INTEGER		16920,D 17240,U	
NHNC	INTEGER		16920,D	
NHO	INTEGER		16920,D	
NN	INTEGER		16920,D	
NNODES	INTEGER		16920,D	
NPRNTE	INTEGER		16920,D	
NPRNTL	INTEGER		16920,D	
NPRNTO	INTEGER		16920,D	
NSTZE	INTEGER		16920,D	
PH	REAL*	50	16980,D	

TENPCF

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
PND	REAL*R	50	16880,D	17150,U 17150,U 17160,U 17160,U 17190,U 17190,U 17210,U 17210,U
PHDD	REAL*R		17170,S	17190,S 17210,S 17360,U 17390,U
PHPP1	REAL*R		17150,S	17170,U
PHDD2	REAL*R		17160,S	17170,U
PT	REAL*R		17010,S	17020,U 17040,U 17060,U 17080,U
Q	REAL*R	R	16960,D	17200,S 17300,S 17320,S 17340,S 17360,S 17380,S 17400,S 17420,S 17470,S
QN	REAL*R	1020	16940,D	
QV1	REAL*R	1020	16940,D	
QN2	REAL*R	1020	16940,D	
QP	REAL*R	1020	16940,D	
QP1	REAL*R	1020	16940,D	
QQ	REAL*R	R	16960,D	17400,S 17510,S 17510,U 17540,U
QS	REAL*R		16940,D	
QUES	REAL*R		16960,D	
Q	REAL*R	50	16880,D	
SINF	REAL*R	51	16870,D	
SINM	REAL*R	50	16880,D	
T	REAL*R	50	16870,D	17020,U 17040,U 17060,U 17080,U
TENPCF	REAL*R		16850,D	
TH	REAL*R	50,5,2	16890,D	17270,U 17280,U 17300,U 17320,U 17340,U 17360,U 17380,U 17400,U 17420,U
THFR	REAL*R		16890,D	
YKD	REAL*R		17260,S	17280,U 17300,U 17320,U 17350,U 17400,U 17400,U 17420,U 17420,U

THCOF

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
ALS	REAL*8		50	16150,D
ALT	REAL*8		50	16150,D
ANG	REAL*8			16330,S 16350,U
CONST	REAL*8			16120,D
DSTN	REAL*8			16610,U 16610,U 16620,U 16620,U
DTH	REAL*8	50,5,2		16150,D 16740,S
DT2	REAL*8			16120,D
FRCE	REAL*8			16140,D
HARM	REAL*8			16160,D
I	INTEGER			16320,U 16320,U 16320,II 16320,S 16320,U 16320,U 16320,U 16320,U 16400,U 16400,S 16520,S 16520,II 16520,U 16530,U 16540,U 16540,U 16540,U 16580,S 16590,U 16600,U 16610,U 16620,II
IR	INTEGER			16100,U 16720,U
TRD1	INTEGER			16720,S 16730,U 16740,U
TDCOF	INTEGER			16130,D
TDCFL	INTEGER			16130,D
TOP	INTEGER			16420,S 16430,U 16430,U
TELM	INTEGER			16100,II 16220,II 16240,U 16240,U 16250,U 16730,U 16740,U
TELM1	INTEGER			16320,S 16390,U
IFLM2	INTEGER			16220,S 16240,U 16320,S 16390,U
TH	INTEGER			16450,S 16460,II 16730,U 16740,U
THARM	INTEGER	5		16160,D 16460,U
KEY	INTEGER			16340,S 16350,U 16360,U 16370,U
KYP	INTEGER			16460,S 16470,II 16510,II 16660,U
LE	INTEGER			16240,U
N	INTEGER			16120,D
NO	INTEGER			16170,D 16300,U

THCOF

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
NOP	INTEGER			16300,S 16300,U 16310,U 16320,U 16330,U 16400,U 16410,U 16500,U 16520,U 16580,U
NOP2	INTEGER			16310,S 16340,U
ND2	INTEGER			16410,S 16420,U
NELEMS	INTEGER			16120,D
NEQ	INTEGER			16120,D
NEQT	INTEGER			16120,D
NH	INTEGER			16120,D 16450,U
NHNS	INTEGER			16120,D
NHP	INTEGER			16160,D
NN	INTEGER			16120,D
NNODES	INTEGER			16120,D
NPRNTF	INTEGER			16130,D
NPRNTL	INTEGER			16130,D 16250,U 16290,U
NPRNTO	INTEGER			16120,D
NS	INTEGER			16170,D
NSIZE	INTEGER			16120,D
NT	INTEGER			16170,D
D	REAL**8	74	16140,D	16300,S 16360,S 16360,U 16390,U 16530,U 16610,U 16670,U
PJ	REAL**8		16230,S	16550,U 16560,U 16630,U 16640,U
PINT	REAL**8		16480,S 16530,S 16530,U 16550,S 16550,U 16610,S 16610,U 16630,S 16630,U 16670,S	
			16700,U 16730,U	
R	REAL**8	74	16140,D	16300,S 16370,S 16370,U 16390,U 16540,U 16620,U 16680,U
RINT	REAL**8		16400,S 16540,S 16540,U 16560,S 16560,U 16620,S 16620,U 16640,S 16640,U 16680,S	
S	REAL**8	74	16140,D	
TAPES	REAL**8		16170,D	
TH	REAL**8	50,5,2	16150,D	16730,S

THCNE

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
THCNE	REAL*8			16100,D
THFR	REAL*8			16150,D
THETR	REAL*8	74	16140,D 16300,S 16330,U 16350,S 16390,U 16390,U 16430,S 16430,U 16530,U 16530,U 16540,U 16540,U 16590,U 16600,U	
X1	REAL*8			16590,S 16610,U 16620,U
X2	REAL*8			16600,S 16610,S 16620,S
YKO	REAL*8			16470,S 16590,U 16600,U 16610,U 16620,U

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
CCC	REAL*8		125	17600,D 17950,S
CCCC	REAL*8		625	17610,D 18440,S
CONST	REAL*8			17620,D
CS	REAL*8			17600,D
CSS	REAL*8		125	17600,D 17970,S
CS4	REAL*8			17610,D
DT2	REAL*8			17620,D
FFIGHT	REAL*8			18230,S 18390,S 18430,S 18470,U
FFTYF	REAL*8			18200,S 18260,S 18400,S 18470,U
FFDUR	REAL*8			17860,S 17930,S 17940,S 17970,U 18190,S 18300,S 18310,S 18440,U 18450,U 18460,U
FONE	REAL*8			17830,S 17870,S 17880,S 17950,U 17960,U 18160,S 18240,S 18250,S 18440,U 18450,U
FSEVEN	REAL*8			18220,S 18390,S 18420,S 18470,U
FCIX	REAL*8			18210,S 18370,S 18410,S 18470,U
FTHREE	REAL*8			17850,S 17910,S 17920,S 17970,U 18180,S 18280,S 18290,S 18440,U 18450,U 18460,U
FTWO	REAL*8			17840,S 17890,S 17900,S 17950,U 17960,U 18170,S 18260,S 18270,S 18440,U 18450,U
HARM	REAL*8			17640,D
TARS	INTEGER			17790,U 17820,U 18080,U 18120,U 18330,U 18350,U
TOOLF	INTEGER			17630,D
TOOLF	INTEGER			17630,D
TEO	INTEGER			18000,S 18150,S 18150,U 18440,U 18450,U 18460,U 18470,U
IHARM	INTEGER	5		17640,D 17720,U 17740,U 17760,U 18020,U 18040,U 18060,U 18100,U
II	INTEGER			17740,S 17770,U 17780,U 17810,U 17820,U 18040,S 18070,U 18080,U 18340,U 18350,U
IMJ	INTEGER			17780,S 17790,U 17890,U 17930,U 18080,S 18130,U 18130,U 18280,U 18290,U 18300,U
				18310,U

TRT40R

VARIABLE	TYPE	INITIAL VALUE	DIMENSION	WHERE/HOW USED
TML	INTEGER	18350,S	18360,U	18370,U 18400,U 18410,U
TMM	INTEGER	17820,S	17930,U	17940,U
TPJ	INTEGER	17770,S	17790,U	17870,U 17880,U 18070,S 18130,U 18130,U 18240,U 18250,U 18260,U 18270,U
TPL	INTEGER	18340,S	18380,U	18390,U 18420,U 18430,U
TPM	INTEGER	17810,S	17910,U	17920,U
ITH	INTEGER	17770,S	17800,S	17800,U 17950,U 17960,U 17970,U
IJ	INTEGER	17760,S	17770,U	17780,U 17910,U 17920,U 17920,J 17930,U 17940,U 17940,U 18060,S 18070,U 18080,U 18320,U 18330,U
KK	INTEGER	18100,S	18110,U	18120,U 18320,U 18330,U
KMI	INTEGER	18330,S	18370,U	18390,U 19410,U 18410,U 18430,U 18430,U
KML	INTEGER	18120,S	18130,U	18130,U 19260,U 18270,U 18270,U 18300,U 18310,U 18310,U
KPJ	INTEGER	18320,S	18360,U	18380,U 18400,U 18400,U 18420,U 18420,U
KPL	INTEGER	18110,S	18130,U	18130,U 18240,U 18250,U 18250,U 18280,U 18290,U 18290,U
LI	INTEGER	18020,S	18110,U	18120,U 19340,U 18350,U
NFLEMS	INTEGER	17620,D		
NFO	INTEGER	17620,D		
NFQT	INTEGER	17620,D		
NH	INTEGER	17620,D	17710,U	17730,U 17750,U 18010,U 18030,U 18050,U 18090,U
NHNS	INTEGER	17620,D		
NHP	INTEGER	17640,D		
NN	INTEGER	17620,D		
NNODES	INTEGER	17620,D		
NPRNTF	INTEGER	17630,D		
NPRNTL	INTEGER	17630,D		
NPRNTQ	INTEGER	17620,D		
NC17F	INTEGER	17620,D		

TRI40R

VARIABLE	TYPE	INITIAL VAL IF	DIMENSION	WHERE/HOW USED
P102	REAL*8			17600,S 17950,U 17960,U 17970,U
P104	REAL*8			17990,S 18440,U 18450,U 18460,U 18470,U
SCCS	REAL*8	625		17610,D 18470,U
SSC	REAL*8	125		17600,D 17960,S
SSCC	REAL*8	625		17610,D 18460,S
SSSS	REAL*8	625		17610,D 18450,S
TRI40R	REAL*8			17580,D

COMMON MAP

COMMON BLOCKS	ROUTINES														
	MAIN	INPUT	SETUP	NLTERM	QPRIME	HQBQ1	HQBQN	NRESTR	MATMUT	SOLVEQ	STRESS	FRCES	THCOE	TFORCE	TRI4OR
CHALS	X	X		X	X	X		X		X	X	X	X	X	X
CONST	X	X	X	X	X	X	X	X						X	X
CS															X
CS4															X
CYCLE	X	X			X	X				X	X				
EES												X	X		
FRCE													X		
GCD													X		
GEOM													X		
HARM	X	X	X	X	X	X	X				X	X	X	X	X
NLTRMS	X	X	X	X	X	X									
PRINT	X	X	X	X						X					
PS	X	X													
QS	X	X	X	X	X	X	X				X	X		X	
QUES															
RESTR	X	X	X			X	X	X	X						
RSTRNT															
RZ															
SLVEEQ	X	X	X		X	X	X	X		X		X	X		
TAPES															
THCON															
THER															
THETAS															
TMFT	X	X	X	X	X	X	X				X	X		X	

EQUIVALENCES

FRCES

EQUIVALENT VARIABLES

NONE

HOUHQN

EQUIVALENT VARIABLES

NONE

HOUHQ1

EQUIVALENT VARIABLES

NONE

INPUT

EQUIVALENT VARIABLES

DUM(1),XN(1)
XN(1),COMENT(1)

MAIN

EQUIVALENT VARIABLES

QN(1),CARD(1)

MATMUT

EQUIVALENT VARIABLES

NONE

NLTERM

EQUIVALENT VARIABLES

NONE

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EQUIVALENCES (continued)

NRESTR

EQUIVALENT VARIABLES

NONE

QPRIME

EQUIVALENT VARIABLES

NONE

SETUP

EQUIVALENT VARIABLES

NONE

SOLVEQ

EQUIVALENT VARIABLES

NONE

STRESS

EQUIVALENT VARIABLES

NONE

TFORCE

EQUIVALENT VARIABLES

NONE

THCOE

EQUIVALENT VARIABLES

NONE

EQUIVALENCES (continued)

TRI40R

EQUIVALENT VARIABLES

NONE

FRCES

FORMAT STATEMENT MAP

LOCATION	STATEMENT NUMBER	SPECIFICATION
15980	160	1H1,35X,49HFOURIER COEFFICIENTS OF APPLIED PRESSURE LOADINGS,//,20X, 10HMERIDIONAL,20X,6HNORMAL,20X, 10HTANGENTIAL,10X,12HHARMONIC NO.,// WRITE (6,160)
16010	170	2I5/(3F10.0) READ(ND,170)IELM1,IELM2,(P(I),R(I), S(I),I=1,NH)
16020	180	/60X,11HELEMENT NO.,I3,1H-,I3, //(2X,3D28.7,15X,I2) WRITE(6,180)IELM1,IELM2,(P(I),R(I), S(I),I,I=1,NH)
	190	1H1,51X,30HAPPLIED LOADS ON THE STRUCTURE//56X,19HPRESSURE COMPONENTS //20X,10HMERIDIONAL,20X,6HNORMAL, 20X,10HTANGENTIAL,11X,19HFROM THETA TO THETA,9H(DEGREES) WRITE(6,190)
16060	200	3I5/(4F10.0) READ(ND,200)IELM1,IELM2,NDP,(THETB(I), P(I),R(I),S(I),I=1,NDP)
16070	210	/60X,11HELEMENT NO.,I3,1H-,I2//(2X, 3F28.3,12X,2F10.3) WRITE(6,210)IELM1,IELM2,(P(I),R(I), S(I),THETB(I),THETB(I+1),I=1,NDP)
16070	220	2X,3F28.3,12X,2F10.3 WRITE(6,220)(P(I),R(I),S(I),THETB(I-1), THETB(I),I=NDPP2,ND2)

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INPUT

FORMAT STATEMENT MAP

LOCATION	STATEMENT NUMBER	SPECIFICATION
05050	730	1H1,38X,65HDYNASOR-II - DYNAMIC NONLINEAR ANALYSIS OF SHELLS OF REVOLUTION// WRITE(6,730)
05070	740	2I5 READ(ND,740)NCARDS,NT
05080	750	20A4 READ(ND,750)(COMENT(J),J=1,20)
05090	760	2F10.0,4I5,/,10I5 READ(ND,760)TOTIME,DELTE,IRSTRT,INCRST, NCLOSE,IITLEF,NPRNTQ,IPRINT,NCLCST, NSTRSS,NPRNT,NPRNTI,NPRNTL,NPRNTF, NPRNTH,NPRNMS
05100	770	I5,/, (8F10.0) READ(ND,770)NTHETA,(THETA(I),I=1,NTHETA)
05110	780	16I5 READ(ND,780)NODRES READ(ND,780)NP,NDIRECT READ(ND,780)IQN,IQNT
05120	790	///,2X,46H**SHELL IDENTIFICATION COMMENTS FROM SAMMSOR** WRITE(6,790)
05130	800	/5X,20A4 WRITE(6,800)(COMENT(J),J=1,20)
05140	810	1H1,50X,33HCONTROL CONSTANTS AND COMMENTS//35X,8HTOTIME =,F12.9,22X, 7HDELTE =,F13.9/35X,8HIRSTRT =,I12, 22X,8HINCRST =,I12/35X,7HNPRNT =, I13,22X,8HNPRNTI =,I12/35X,8HNPRNTQ =, I12,22X,8HNPRNT =,I12/35X,8HNCLCST =, I12,22X,8HNSTRSS =,I12/35X,8HNPRNTL =, I2,22X,8HNPRNTF =,I12/35X,8HNPRNTH =, I12,22X,4HNT =,I16/35X,4HNS =,I16,22X, 4HND =,I16,/35X,8HNCLOSE =,I12,22X, 7HITLEF =,I13/35X,8HNELEMS =,I12,22X, 8HNPRNMS =,I12/35X,4HNH =,I16,/35X, 7HIHARM =,5I11//

INPUT

FORMAT STATEMENT MAP

LOCATION	STATEMENT NUMBER	SPECIFICATION
		WRITE(6,810)TOTIME,DELTE,IRSTR,INCRST,NPRNT,NPRNIT,NPRNTQ,IPIR,NCLCST,NSTRSS,NPRNTL,NPRNTF,NPRNTF,NPRNTH,NT,NS,ND,NCLOSE,ITELF,NELEMS,NPRNMS,NH,(IHARM(I),I=1,NH)
05210	820	35X,8HNTHETA =,I12,/35X,7HTHETA =, 5F10.2,(/,42X,5F10.2) WRITE(6,820)NTHETA,(THETA(I),I=1,NTHETA)
05220	830	////50X,29HNUMBER OF NODAL RESTRAINTS ISI5//52X,9HDIRECTION,12X,7HAPPLIES, //,57X,1H1,10X,15HAXIAL RESTRAINT,/, 57X,1H2,10X,20HTANGENTIAL RESTRAINT, /,57X,1H3,10X,16HRADIAL RESTRAINT,/, 57X,1H4,10X,17HANGULAR RESTRAINT,/, 58X,15HNODE DIRECTION/ WRITE(6,830)NODRES
05260	840	58X,I3,7X,I1 WRITE(6,840)NP,NDIRCT
05270	850	2I5,4F10.0 READ(ND,850)IN1,IN2,Q1,Q2,Q3,Q4 READ(ND,850)IN1,IN2,Q1,Q2,Q3,Q4
05280	860	1H1,7X,7HINITIAL,29X,10HVELOCITIES,22X, 3HAND,19X,13HDISPLACEMENTS//4X, 124HNODE HARMONIC AXIAL TANGENTIAL RADIAL ANGULAR AXIAL TANGENTIAL RADIAL ANGULAR // WRITE(6,860)
05320	870	5X,I2,6X,I2,3X,8D14.4 WRITE(6,870)II,IHARM(I),QN(IQ+IX+1), QN(IQ+IX+2),QN(IQ+IX+3),QN(Q+IX+4), QN1(IQ+IX+1),QN1(IQ+IX+2),QN1(IQ+IX+3), QN1(IQ+IX+4)
05330	880	2I5,2F10.0 READ(ND,880)IELM1,IELM2,ALSI1,ALTI1

INPUT

FORMAT STATEMENT MAP

LOCATION	STATEMENT NUMBER	SPECIFICATION
05340	890	1H1,45X,41HELEMENT ELASTIC AND GEOMETRIC PROPERTIES,///67HELEMENT ALPHA--S ALPHA--T E1 E2 FNU1 FNU2 G,11X,1HR,11X,1HT,9X,4HARCL,9X,2HPPH, 10X,3HPHP// WRITE(6,890)
05370	900	3X,I2,2X,4D10.2,2F6.3,6D12.4 WRITE(6,900)(I,ALS(I),ALT(I),E1(I),E2(I), FNU1(I),FNU2(I),B(I),R(I),T(I),ARCL(I), PH(I),PHP(I),I=1,NELEMS)
05380	910	1H1,38X,15HHARMONIC NUMBER,I5,37H HAS THE FOLLOWING STIFFNESS MATRIX// WRITE(6,910)IHARM(JH)
05400	920	2X,D16.8,/,2X,2D16.8,/,2X,3D16.8,/,2X, 4D16.8,/,2X,5D16.8,/,2X,6D16.8,/, 2X,7D16.8,/,2X,8D16.8,/,2X,5D16.8,/, 2X,6D16.8,/,2X,7D16.8,/,2X,8D16.8,/ WRITE(6,920)(XN(I+NN),I=1,NSIZE) WRITE(6,920)(XP(I+NN),I=1,NSIZE)
05430	930	1H1,38X,15HHARMONIC NUMBER,I5,32H HAS THE FOLLOWING MASS MATRIX// WRITE(6,930)IHARM(JH)
05450	940	1H1////5X,45HTHIS SOLUTION STARTS AFTER TIME INCREMENT NO.,I5,19H WHERE THE TIME WAS,F12.4,13H MICROSECONDS,/,5X, 27H AND THE TIME INCREMENT WAS,D12.5///// WRITE(6,940)ITP,TPRNT,DELTEP
05480	950	F10.0,4I5,A8 READ(ND,950)T1,NCF,IDEFL,IDCOE,ITCOE,CONSTF
05490	960	40H1FOLLOWING IS LOAD DESCRIPTION AT TIME =, F12.4,13H MICROSECONDS,5X,A8 WRITE(6,960)TPRNT,CONSTF
05510	970	2I5,4F10.0 READ(ND,970)NCF1 READ(ND,970)IN1,IN2,F1,F2,F3,F4

INPUT

FORMAT STATEMENT MAP

LOCATION	STATEMENT NUMBER	SPECIFICATION
05520	980	//20X,30HCONCENTRATED FORCES HARMONIC , I5//6X,8HNODE NO.,6X,5HAXIAL,10X, 10HTANGENTIAL,10X,6HRADIAL,13X, 7HANGULAR/ WRITE(6,980)IHARM(IH)
05540	990	I10,4D20.8 WRITE(6,990)IN,F1,F2,F3,F4
05550	1000	2I5,/, (2F10,0) READ(ND,1000)IELM1,IELM2,(TH1(IH),DTH1(IH), IH=1,NH)
05560	1010	1H1,25X,39HTEMPERATURE COEFFICIENTS, HARMONIC NO. I3//10X,11HELEMENT NO., 17X,12HTEMP. COEFF.,12X,18HTEMP. GRAD. COEFF./// WRITE(6,1010)IHARM(IH)
05580	1020	I20,2D30.5 WRITE(6,1020)IELM,TH(IELMIN,IBP1), DTH(IELM,IH,IBP1)
05590	1030	1H1,25X,32HGENERALIZED FORCES, HARMONIC NO.,I3,//6X,8HNODE NO.,6X,5HAXIAL, 13X,10HTANGENTIAL,11X,6HRADIAL,13X, 7HANGULAR/// WRITE(6,1030)KYP
05610	1040	I9,4D19.8 WRITE(6,1040)I,FORCE(K+1),FORCE(K+2), FORCE(K+3),FORCE(K+4)
05620	1050	1H1////5X,42HRESTART INFORMATION FOR TIME INCREMENT NO.,I5,/,10X,22H CORRESPONDING TO TIME,F12.4,13H MICROSECONDS,/,2X,51H HAS BEEN PLACED ON TAPE FOR USE IN SUBSEQUENT RUNS// WRITE(6,1050)ITAM,TPRNT

MAIN

FORMAT STATEMENT MAP

LOCATION	STATEMENT NUMBER	SPECIFICATION
00790 00200	110	3I5 READ (5,110) NCASES,ND,NS
00800 00210	120	1H1,///,30X,31H THE NUMBER OF CASES TO BE RUN=I5 WRITE (6,120) NCASES
00810 00300	130	20A4 READ (5,130) CARD
00820 00350	140	//8H1 NCASE=,I1//,28X,22H PRINTOUT OF INPUT DATA,/br/> WRITE (6,140) NCASE
00830 00360	150	13X,2H10,8X,2H20,8X2H30,8X2H40,8X,2H50, 8X,2H60,8X,2H70,8X,2H80/5X,80H1234567 8901234567890123456789012345678901234 567890123456789012345678901234567890,/ WRITE (6,150)
00860 00390	160	5X,20A4 WRITE (6,160) CARD
00870 00430	170	72H THE NUMBER OF INPUT CASES DOES NOT AGREE WITH THE VALUE OF NCASES INPUT WRITE (6,170)
00890 00760	180	1H1//10X,18H ALL DATA PROCESSED//10X, 11H...STOP WRITE (6,180)

SETUP

FORMAT STATEMENT MAP

LOCATION	STATEMENT NUMBER	SPECIFICATION
06430	110	1H1,30X,6HITAM =,I5,5X,6HTIME =,F12.4, 13H MICROSECONDS// WRITE(6,110)ITAM,TPRNT WRITE(6,110)ITAM,TPRNT
06440	120	36X,22HDISPLACEMENTS OF NODES/38X, 9HHARMONIC ,I5//6X,8HNODE NO.,6X, 5HAXIAL,13X,10HTANGENTIAL,11X, 6HRADIAL,13X,7HANGULAR// WRITE(6,120)KY
06460	130	I10,4D20.8 WRITE(6,130)I,(QN(K+J),J=1,4) WRITE(6,130)I,(QLOAD(K+J),J=1,4)
06470	140	25X,34HDISPLACEMENTS OF NODES AT THETA =, F8.3,9H DEGREES/38X,13HALL HARMONICS/2X, 8HNODE NO.,9X,5HAXIAL,12X,10HTANGENTIAL, 12X,6HRADIAL,13X,7HANGULAR// WRITE(6,140)THETA1
06500	150	1H1,5X,4HITAM,I5,5X,4HTIME,E12.5//6X, 55HEXECUTION TERMINATED - DISPLACEMENTS GREATER THAN 1.E+4 WRITE(6,150)ITAM,TIME

STRESS

FORMAT STATEMENT MAP

LOCATION	STATEMENT NUMBER	SPECIFICATION
14740	50	$1H1,3X,6HITAM = ,I5,3X,6HTIME = ,F12.4,$ $13H \text{ MICROSECONDS}, //, 47X, 33H\text{STRESSES}$ $\text{AND STRESS RESULTANTS}, /, 25X, 17H\text{FORCE}$ $\text{RESULTANTS}, 31X, 18H\text{MOMENT RESULTANTS},$ $18X, 17H\text{SHEAR RESULTANTS}, /, 19X,$ $109HN(S)$ $N(T) \quad N(ST) \quad M(S) \quad M(T)$ $M(ST) \quad Q(S) \quad Q(T), //, 12H \text{ELEM THETA},$ $/, 104H$ $\text{NO (DEG)} \quad \text{***** OUTER SURFACE STRESSES *****}$ $\text{INNER SURFACE STRESSES *****}, /, 15X, 88H^* \text{SIGMA}(S) S$ $GMA(T) \quad SIGMA(ST) \quad SIGMA(S) \quad SIGMA(T) \quad SIGMA(ST)$ $) */)$ $\text{WRITE}(6,50)ITAM1,TPRINT$
14830	60	$I4,F8.2,6(1PD15.4),30H XXXX XXXX ,/, 12H$ $\text{STRESSES **}, 6(1PD15.4)$ $\text{WRITE}(6,60)I1,THETA1,STRNS,STRNT,STRNST,$ $STRMT,STRMST,BSU,BTU,BSTU,BSL,BTL,BSTL$
14850	70	$I4,F8.2,8(1PD15.4),/, 12H \text{STRESSES **},$ $6(1PD15.4)$ $\text{WRITE}(6,70)I1,THETA1,STRNS,STRNT,STRNST,$ $STRMS,STRMT,STRMST,SHRS,SHRT,BSU,BTU,$ $BSTU,BSL,BTL,BSTL$

THCOE

FORMAT STATEMENT MAP

LOCATION	STATEMENT NUMBER	SPECIFICATION
16780	110	1H1,41X,47HTEMPERATURES AND THERMAL GRADIENTS ON STRUCTURE//27X, 11HTEMPERATURE,10X,16HTHERMAL GRADIENT,10X,29HFROM THETA TO THETA (DEGREES)//
16810	120	3I5/(3F10.0) READ(ND,120)IELM1,IELM2,NDP,(THETB(I), P(I),R(I),I=1,NDP)
16820	130	/,60X,11HELEMENT NO.,I3,1H-,I2,,/ (28X,F9.3,15X,F10.3,16X,1F7.2,2X, F7.2) WRITE(6,130)IELM1,IELM2,(P(I),R(I), THETB(I),THETB(I+1),I=1,NDP)

LABEL CROSS REFERENCE MAP

There is a label or statement number cross reference map listed for each routine. This listing gives an ascending statement number listing with corresponding references to that number. The listing gives the statement number being referenced, sequence number of referencing statements, and a corresponding letter value for each statement reference. The letter values for each reference are one of the following:

L - this letter indicates that the referencing statement is a DO LOOP and the statement number given is the lower bound for the loop.

B - this indicates that the referencing statement is a branch to the given statement number.

R - an R indicates that the statement number listed is the label for a READ statement.

W - this indicates that the statement number listed is the label for a WRITE statement.

FRCES

LABEL CROSS REFERENCE MAP

STATEMENT NUMBER	REFERENCES
10	15050,B
20	15190,L
30	15330,L
40	15040,B 15110,B
50	15400,L
60	15470,B
70	15440,B
80	15560,B
90	15510,B 15550,B 15600,B
100	15430,L
110	15390,B
120	15720,B
130	15880,L 15900,L
140	15920,L
150	15360,L
160	15050,L
170	15080,R
180	15090,W
190	15130,W
200	15170,R
210	15210,W
220	15310,W

HQBQN

LABEL CROSS REFERENCE MAP

STATEMENT NUMBER	REFERENCES
10	9920,L
20	9990,L
30	10120,L
40	10110,B
50	10190,L

HQBQ1

LABEL CROSS REFERENCE MAP

STATEMENT NUMBER	REFERENCES
10	9210,B
20	9180,L 9230,B
30	9320,B
40	9300,L 9340,B
50	9380,L
60	9600,B
70	9470,L
80	9520,L
90	9460,B
100	9630,L
110	9670,L

INPUT

LABEL CROSS REFERENCE MAP

STATEMENT NUMBER	REFERENCES
10	1180,B
20	1250,L
30	1240,B
40	1760,B
50	1480,L 1500,B
60	1460,B
70	1580,L
80	1630,B
90	1620,L 1650,B
100	1720,L
110	1540,B
120	1930,L
130	2020,L
140	2140,L
150	2130,B
160	2370,B
170	2310,L
180	2270,L
190	2260,B
200	2510,B
210	2450,L
220	2410,L
230	2400,B
240	2550,L 2570,L
250	2060,B
260	2640,L
270	2710,B
280	2700,L 2730,B
290	2780,L
300	2910,B
310	2880,L
320	2820,B
330	2930,L
340	2920,B
350	3050,L
360	3060,B
370	3040,L 3100,B 3150,B
380	3350,B
390	3370,L
400	3220,B

INPUT

LABEL CROSS REFERENCE MAP

STATEMENT REFERENCE
NUMBER

410	3570,L
420	3610,L 3620,L
430	180,B
440	3710,B
450	3730,L
460	3750,L 3760,L
470	3720,B
480	3830,L
490	3870,L 3880,L
500	4830,B
510	4010,B
520	1130,B 4250,B
530	1170,L
540	4080,L 4120,B
550	4070,B
560	4300,L
570	4280,B
580	4470,S
590	4430,L 4440,L
600	4400,B
610	4500,B
620	4480,L
630	4550,L 4570,L
640	4540,L
650	4610,B
660	4620,L 4080,L
670	4630,B
680	4730,L
690	4730,L
700	4720,B
710	4710,L
720	4700,L
730	4600,R
740	4610,R
750	4620,R
760	4630,R
770	4640,R
780	2110,L 2160,R 2250,R
790	1510,R

INPUT

LABEL CROSS REFERENCE MAP

STATEMENT
NUMBER

810	1780,W
820	1810,W
830	2120,W
840	2170,W
850	2300,R 2440,R
860	2540,W
870	2590,W
880	2870,R
890	3010,W
900	3020,W
910	3160,W
920	3170,W 3190,W
930	3180,W
940	3510,W
950	3980,R
960	4060,W
970	4110,R 4160,R
980	4140,W
990	4230,W
1000	4420,R
1010	4560,W
1020	4580,L
1030	4670,W
1040	4700,W
1050	5020,W

MAIN

LABEL CROSS REFERENCE MAP

STATION NUMBER	REFERENCES
10	410,B
20	400,B
30	340,B
40	310,B
50	750,B
60	510,L
70	330,B
80	640,B 650,S
90	620,L
100	700,B
110	200,R
120	210,W
130	300,R 330,W
140	350,W
150	360,W
160	390,A
170	460,W
180	750,L

MATMUT

LABEL CROSS REFERENCE MAP

STATEMENT NUMBER	REFERENCES
10	10940,L
20	11010,L 11010,L
30	11160,L
40	11110,L 11140,L

NLTERM

LABEL CROSS REFERENCE MAP

STATEMENT NUMBER	REFERENCE
10	6730,L
20	6910,B
30	6950,L
40	6760,L
	6970,L

NRESTR

LABEL CROSS REFERENCE MAP

STATEMENT NUMBER	REFERENCES
10	10430,L
20	10420,L
30	10410,B
40	10560,L
50	10610,L
60	10690,L
70	10520,B 10660,B
80	10380,L
90	10370,B
100	10800,L

QPRIME

LABEL CROSS REFERENCE MAP

STATEMENT NUMBER	REFERENCE
10	7590,L
20	7980,L
30	8010,L 8030,L 8070,B
40	7910,L
50	8370,L 8390,L 8430,L 8470,B
60	8330,L
70	8720,L 8740,L 8780,B
80	8680,L
90	8650,B

SETUP

LABEL CROSS REFERENCE MAP

STATEMENT NUMBER	REFERENCE
10	5900,B
20	5960,L
30	6060,L
40	6170,B
50	6080,L 6130,L 6160,L 6190,B
60	6250,L
70	6050,L
80	6000,B 6010,B
90	5830,L 5910,B 5920,B 6330,B
100	6380,B
110	5940,W 6220,W
120	5950,W
130	5980,W 6270,W
140	6240,W
150	6350,W

SOLVEQ

LABEL CROSS REFERENCE MAP

STATEMENT NUMBER	REFERENCES
10	11390,L
20	11420,L
30	11640,B
40	11640,B
50	11710,B
60	12590,B
70	12590,B
80	12670,B
90	
100	11440,B
110	13090,L
120	13040,B
130	13310,B
140	13310,B
150	13280,L 13400,B
160	13500,L
170	13530,L

STRESS

LABEL CROSS REFERENCE MAP

STATEMENT NUMBER	REFERENCES
10	13960,L
20	14530,B
30	14560,B
40	13820,L
50	13810,W
60	14540,W
70	14640,W

TFORCE

LABEL CROSS REFERENCE MAP

STATEMENT NUMBER	REFERENCES
10	17130,B
20	17140,B
30	17180,B
40	17200,B 17440,B
50	17460,L
60	17450,B
70	17480,L 17500,L
80	17520,L
90	17240,L 17270,B

THCOE

LABEL CROSS REFERENCE MAP

STATEMENT NUMBER	REFERENCES
10	16320,L
20	16420,L
30	16240,B
40	16520,L
50	16510,B
60	16580,L
70	16500,B
80	16660,B
90	16570,B 16650,B 16690,B
100	16450,L
110	16250,W
120	16300,R
130	16390,W

TRI40R

LABEL CROSS REFERENCE MAP

STATEMENT NUMBER	REFERENCES
10	17710,L 17730,L 17750,L 17790,B
20	18010,L 18030,L 18050,L 18090,L 18130,B

FRCES

SUBROUTINES CALLED

NAME	LOCATION
NONE	

CALLED BY ROUTINES

INPUT

HOUHQN

SUBROUTINES CALLED

NAME	LOCATION
MATMUT(IH,QN2,XP,QLOAD,NEQ)	09960
SOLVEQ(IH)	10180

CALLED BY ROUTINES

SETUP

HOUHQ1

SUBROUTINES CALLED

NAME	LOCATION
MATMUT(IH,QN,XP,QLOAD,NEQ)	09170
MATMUT(IH,QN,XP,QLOAD,NEQ)	09280
NRESTR(KY)	09430
SOLVEQ(IH)	09450
NRESTR(KY)	09740

CALLED BY ROUTINES

SETUP

INPUT

SUBROUTINES CALLED

NAME	LOCATION
TRI40R	03210
NLTERM(0)	03360
FRCES(IELM,ALPHK,IB)	04320
THCOE(IELM,IB)	04510
TFORCE(IELM,IB)	04520

CALLED BY ROUTINES

MAIN
SETUP

MAIN

SUBROUTINES CALLED

NAME	LOCATION
INPUT(1)	0470
INPUT(2)	0670
NLTERM(ITAM)	0740
SETUP(ITAM,TIME,LARGE)	0690

CALLED BY ROUTINES

NONE

MATMUT

SUBROUTINES CALLED

NAME	LOCATION
NONE	

CALLED BY ROUTINES

HOUHQ1

HOUHQN

NLTERM

SUBROUTINES CALLED

NAME	LOCATION
QPRIME(I1)	06870
STRESS(I1,ITAM)	06930

CALLED BY ROUTINES

MAIN
INPUT
SETUP

NRESTR

SUBROUTINES CALLED

NAME	LOCATION
NONE	

CALLED BY ROUTINES

HOUHQ1

QPRIME

SUBROUTINES CALLED

NAME	LOCATION
NONE	

CALLED BY ROUTINES

NLTERM

SETUP

SUBROUTINES CALLED

NAME	LOCATION
NLTERM(ITAM)	05820
HOUBQN(KY,IH)	05870
HOUBQ1(KY,IH)	05880
INPUT(3)	06400

CALLED BY ROUTINES

MAIN

SOLVEQ

SUBROUTINES CALLED

NAME	LOCATION
NONE	

CALLED BY ROUTINES

HOUBQ1

HOUBQN

STRESS

SUBROUTINES CALLED

NAME	LOCATION
NONE	

CALLED BY ROUTINES

NLTERM

TFORCE

SUBROUTINES CALLED

NAME	LOCATION
NONE	

CALLED BY ROUTINES

INPUT

THCOE

SUBROUTINES CALLED

NAME	LOCATION
NONE	

CALLED BY ROUTINES

INPUT

TRI40R

SUBROUTINES CALLED

NAME	LOCATION
NONE	

CALLED BY ROUTINES

INPUT

FRCES

SUBROUTINE CALLING ARGUMENTS

VARIABLE	SUBROUTINE	LOCATION
NONE		

HOUHQN

SUBROUTINE CALLING ARGUMENTS

VARIABLE	SUBROUTINE	LOCATION
IH	MATMUT	09960
IH	SOLVEQ	10180
NEQ	MATMUT	09960
QLOAD	MATMUT	09960
QN2	MATMUT	09960
XP	MATMUT	09960

HOUHQ1

SUBROUTINE CALLING ARGUMENTS

VARIABLE	SUBROUTINE	LOCATION
IH	MATMUT	09170
IH	MATMUT	09280
IH	SOLVEQ	09450
KY	NRESTR	09430
KY	NRESTR	09740
NEQ	MATMUT	09170
NEQ	MATMUT	09280
QLOAD	MATMUT	09170
QLOAD	MATMUT	09280
QN	MATMUT	09170
QN	MATMUT	09280
XP	MATMUT	09170
XP	MATMUT	09280

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INPUT

SUBROUTINE CALLING ARGUMENTS

VARIABLE	SUBROUTINE	LOCATION
ALPHK	FRCES	04320
IB	FRCES	04320
IB	THCOE	04510
IB	TFORCE	04520
IELM	FRCES	04320
IELM	THCOE	04510
IELM	TFORCE	04520
0	NLTERM	03360

MAIN

SUBROUTINE CALLING ARGUMENTS

VARIABLE	SUBROUTINE	LOCATION
ITAM	SETUP	00690
ITAM	NLTERM	00740
LARGE	SETUP	00690
TIME	SETUP	00690

MATMUT

SUBROUTINE CALLING ARGUMENTS

VARIABLE	SUBROUTINE	LOCATION
NONE		

NLTERM

SUBROUTINE CALLING ARGUMENTS

VARIABLE	SUBROUTINE	LOCATION
ITAM	STRESS	06930
I1	QPRIME	06870
I1	STRESS	06930

NRESTR

SUBROUTINE CALLING ARGUMENTS

VARIABLE	SUBROUTINE	LOCATION
NONE		

QPRIME

SUBROUTINE CALLING ARGUMENTS

VARIABLE	SUBROUTINE	LOCATION
NONE		

SETUP

SUBROUTINE CALLING ARGUMENTS

VARIABLE	SUBROUTINE	LOCATION
IH	HOUHQN	05870
IH	HOUHQ1	05880
ITAM	NLTERM	05820
KY	HOUHQN	05870
KY	HOUHQ1	05880
3	INPUT	06400

SOLVEQ

SUBROUTINE CALLING ARGUMENTS

VARIABLE	SUBROUTINE	LOCATION
NONE		

STRESS

SUBROUTINE CALLING ARGUMENTS

VARIABLE	SUBROUTINE	LOCATION
NONE		

TFORCE

SUBROUTINE CALLING ARGUMENTS

VARIABLE	SUBROUTINE	LOCATION
NONE		

THCOE

SUBROUTINE CALLING ARGUMENTS

VARIABLE	SUBROUTINE	LOCATION
NONE		

TRI40R

SUBROUTINE CALLING ARGUMENTS

VARIABLE	SUBROUTINE	LOCATION
NONE		

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SECTION III

PROGRAM INPUT

The DYNASOR II code has been written so that the code can be employed by researchers who are not familiar with the inner workings of the program. Utilizing the guidelines and adhering to the limitations presented in the previous section, it is believed that most users will find it relatively easy to employ the code.

The code is available in the FORTRAN IV language using double precision or single precision arithmetic. This double precision version requires a storage space of about 330K bytes on IBM 360/65 system while the single precision storage space is about 200K bytes. Efforts have been made to make this code compatible with a large number of computing systems. In particular, adaption of the code for use on a CDC 6600 computer requires only minor changes.

The input data for a run consists of one card I (card types will be explained on the following pages) followed by a complete set of data (cards II-X) for each case. The set of cards II-X is the input data required to generate the response of a shell for a given number of harmonics due to a particular loading. The cards comprising the data deck for both an initial run and a restart are schematically represented in Fig. 1. The cards specifying the Fourier harmonics, the initial conditions, and the boundary conditions are omitted from the input deck when using the restart mode. If more than one case is to be run, include a set of data for each of the cases. There is no limit on the number of cases which may be included in a run. A card must be placed at the end of the data for the final case.

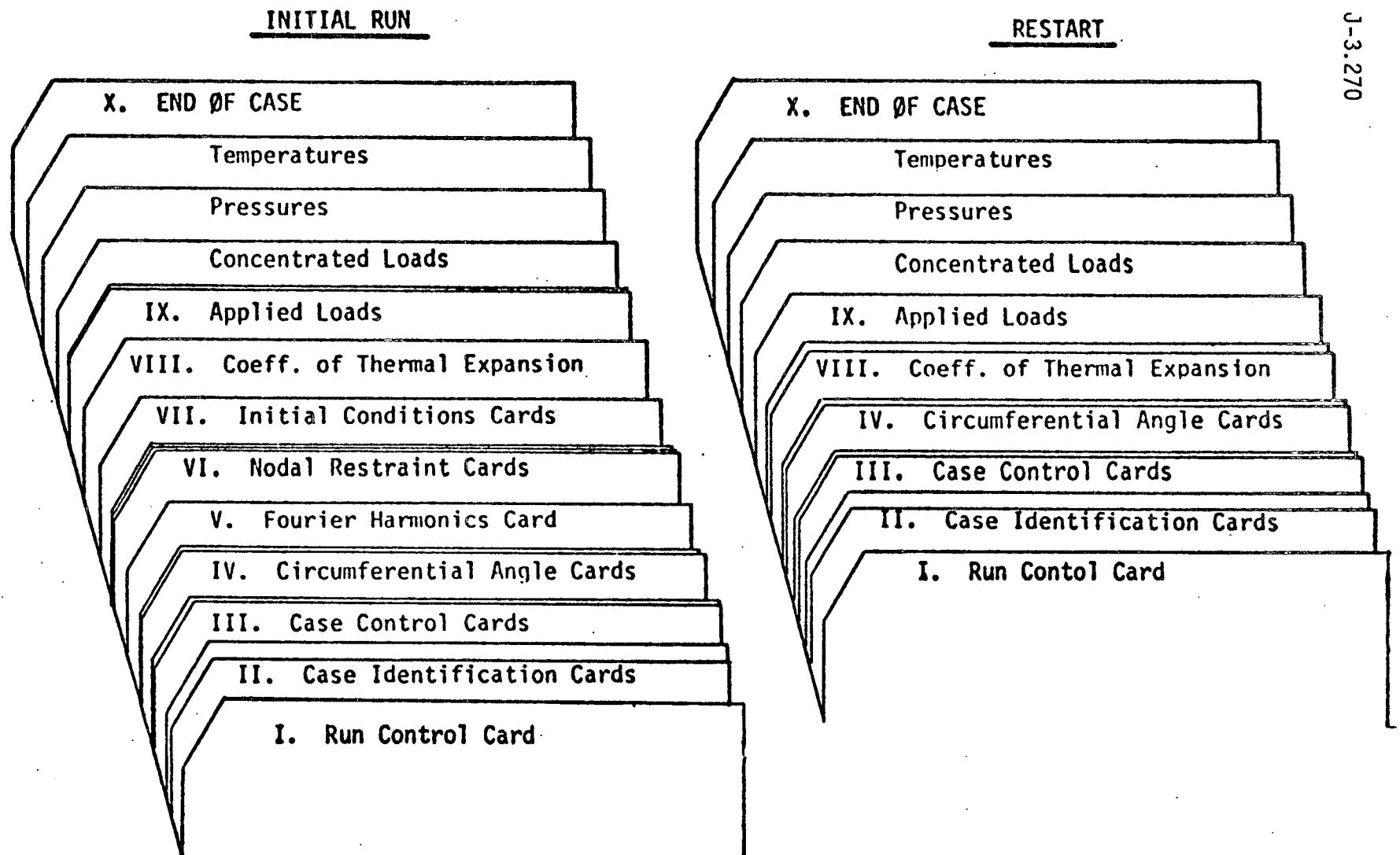


FIG. 1 CONSTITUTION OF DATA DECKS - INITIAL RUN AND RESTART MODES.

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I. RUN CONTROL CARD

This card is used to identify the number of cases to be run and the logical unit numbers of the scratch tapes used in the run. (ONLY ONE CARD I IS USED PER RUN.)

Card Type I Format (3I5)		
Columns	Variable	Description
1-5	NCASES	The number of different data sets utilized for this run.
6-10	ND	Logical unit number of the scratch tape onto which all the data is read at the start of the run.
11-15	NS	Logical unit number of a second scratch tape used by the program.

II. CASE IDENTIFICATION CARDS

These cards allow the user to print out comments which identify the problem being run.

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A. Control Card (ONE CARD II-A PER DATA SET)

Card Type II-A Format (2I5)		
Columns	Variable	Description
1-5	NCARDS	Number of comment cards (TYPE II-B) which follow.
6-10	NT	Logical unit number of the tape (prepared by SAMMSOR) from which the stiffness and mass matrices, element properties, and restart information, if needed, will be read.

B. Identification Cards - The information punched on these cards is printed as output and should identify the problem being run. These comments should not duplicate those of the SAMMSOR case since the SAMMSOR comments will also appear as output. (IF NCARDS=0, OMIT CARDS II-B, OTHERWISE INCLUDE NCARDS OF TYPE II-B.)

Card Type II-B Format (20A4)		
Columns	Variable	Description
1-80	COMENT	Any desired alphanumeric information may be printed on these cards.

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III. CASE CONTROL CARDS

- A. Control Constants - Time parameters, restart information, and other miscellaneous control constants are input on this card. (INCLUDE ONE CARD III-A PER DATA SET.)**

Card Type III-A Format (2F10.0,4I5)		
Columns	Variable	Description
1-10	TOTIME	The maximum time (seconds) for which the calculations are to be performed.
11-20	DELTE	Time increment (seconds) used in solving the equations of motion.
21-25	IRSTRRT	Control constant which indicates if the solution is being restarted. If the solution is being restarted set IRSTRRT = 1. If not, set IRSTRRT = 0.
26-30	INCRST	The number of the time increment at which the solution is to be restarted. INCRST must be an integer multiple of the value of NPNRNT used in the previous run. If IRSTRRT = 0, set INCRST = 0.
31-35	NCLOSE	For a closed shell (such as a spherical cap or a hemisphere) where node 1 is at the apex, set NCLOSE = 1. Radial and rotational restraints will then be applied for the zeroth harmonic to aid the numerical stability of the solution. If the shell does not fit the above description, set NCLOSE = 0.
36-40	ITELF	If thermal loads are to be applied in the program, set ITELF = 1. Otherwise, set ITELF = 0.

- B. Print Control Card - The constants used to control the program output are punched on this card. (INCLUDE ONE CARD III-B PER DATA**

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SET.)

Card Type III-B Format (10I5)

Columns	Variable	Description
1-5	NPRNTQ	If the displacements are to be printed, set NPRNTQ = 1. If not, set NPRNTQ = 0.
6-10	IPRINT	If NPRNTQ = 1, the displacements will be printed every IPRINT time increments beginning with the first time step. If NPRNTQ = 0, set IPRINT = 0.
11-15	NCLCST	If the stresses and stress resultants are to be calculated, set NCLCST = 1. If not, set NCLCST = 0.
16-20	NSTRSS	If NCLCST = 1, the stress and stress resultants will be calculated and printed every NSTRSS time increments beginning with the first step. If NCLCST = 0, set NSTRSS = 0.
21-25	NPRNT	If restart information is to be placed on tape, set NPRNT = 1. If not, set NPRNT = 0.
26-30	NPRNIT	If NPRNT = 1, the restart information will be written on the output tape every NPRNIT time increments. If NPRNT = 0, set NPRNIT = 0. It is suggested that relatively large values of NPRNIT be used, say 200, 400, etc., if the total number of time steps is relatively large.
31-35	NPRNTL	If a printout of the applied loads is desired, set NPRNTL = 1. Otherwise, set NPRNTL = 0.
36-40	NPRNTF	If a printout of the generalized forces is desired, set NPRNTF = 1. Otherwise, set NPRNTF = 0.

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41-45	NPRNTH	If the Fourier coefficients for the temperature and temperature gradient are to be printed, set NPRNTH = 1. Otherwise, set NPRNTH = 0.
46-50	NPRNMS	If the mass and stiffness matrices are to be printed, set NPNRMS = 1. If not, set NPNRMS = 0.

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IV. CIRCUMFERENTIAL ANGLE CARDS

The circumferential angles at which the displacements and stresses are to be calculated are read from these cards.

A. Control Card - (ONE CARD IV-A PER DATA SET.)

Card Type IV-A Format (I5)		
Columns	Variable	Description
1-5	NTHETA	The number if circumferential angles at which the displacements and possibly stresses are to be calculated. ($1 \leq NTHETA \leq 20$)

B. Circumferential Angles - (INCLUDE 1-3 CARDS IV-B PER DATA SET, DEPENDING UPON THE VALUE OF NTHETA.)

Card Type IV-B Format (8F10.0)		
Columns	Variable	Description
1-10	THETA(1)	Circumferential angles at which the displacements and possible stresses will be calculated.
11-20	THETA(2)	(If it is desired to calculate the displacements only along the line = 0, then include one card IV-B and set THETA(1) = 0.0)
"	"	
"	"	
"	THETA(NTHETA)	

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V. FOURIER HARMONICS CARD

This card provides the number of Fourier cosine harmonics to be employed for this analysis and enumerates the specific harmonics to be used. (IF IRSTRT = 1, OMIT CARD V. OTHERWISE, INCLUDE ONE CARD V PER DATA SET.)

Card Type V Format (6I5)		
Columns	Variable	Description
1-5	NH	The total number of Fourier cosine harmonics to be utilized in this analysis ($1 \leq NH \leq 5$).
6-10	IHARM(1)	Specific harmonics numbers to be employed. NH
11-15	IHARM(2)	values must be given and the zero harmonic
16-20	IHARM(3)	must always be specified as one of the input
21-25	IHARM(4)	harmonic numbers. The user should check to be
26-30	IHARM(5)	certain that the information for each of these harmonics has been created and stored on tape by the SAMMSOR code.

Example: Consider a case where it is desired to utilize harmonics 0, 2, 3, and 4. The input data for card V would then utilize the following values:

NH = 4

IHARM(1) = 0 NOTE: IHARM(1) should always be set equal to zero.

IHARM(2) = 2

IHARM(3) = 3

IHARM(4) = 4

Columns 26-30 corresponding to IHARM(5) should be left blank for this example since only four harmonics are being run.

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VI. NODAL RESTRAINT CARDS (Boundary Conditions)

The displacement constraints applied to the shell are described utilizing these cards. (IF IRSTRT = 1, OMIT CARDS VI-A AND VI-B.)

A. Control Card - (ONE CARD VI-A PER DATA SET, UNLESS IRSTRT = 1.)

Card Type VI-A Format (I5)		
Columns	Variable	Description
1-5	NODRES	Total number of displacement constraints to be applied to the shell ($0 \leq \text{NODRES} \leq 204$)

B. Boundary Conditions - (THE NUMBER OF CARDS OF TYPE VI-B MUST EQUAL NODRES, UNLESS IRSTRT = 1. IF NODRES = 0, OMIT CARDS VI-B.)

Card Type VI-B Format (2I5)		
Columns	Variable	Description
1-5	NP	Number of the node where the restraint is to be applied.
6-10	NDIRCT	Key used to indicate the degree of freedom which is restrained. NDIRCT = 1 applies axial restraint NDIRCT = 2 applies circumferential restraint NDIRCT = 3 applies radial restraint NDIRCT = 4 applies rotational restraint

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VII. INITIAL CONDITIONS CARDS

The initial velocities and displacements of the nodes are specified on these cards. (IF IRSTRT = 1, OMIT CARDS VII-Z, VII-B, AND VII-C.)

- A. Control Card - Utilization of this control card greatly simplifies the specification of the initial conditions if either the initial velocities or the initial displacements, or both, are equal to zero. (ONE CARD VII-A PER DATA SET)**

Card Type VII-A Format (2I5)		
Columns	Variable	Description

1-5	IQN	If the initial velocities at all the nodes are zero, set IQN = 0. If not, set IQN = 1.
6-10	IQN1	If the initial displacements at all the nodes are zero, set IQN1 = 0. If not, set IQN1 = 1.

- B. Initial Velocities - The initial nodal velocities must be specified for each node of the shell for each harmonic to be run. The logic used to input the nodal velocities is essentially the same as the procedure used to specify the element properties in the SAMMSOR code. The initial velocities for each of the nodes are specified for the first of the input harmonics, then for the second input harmonic, etc. This process is repeated until the nodal velocities for the first of the input harmonics, then for the second input harmonic, etc. This process is repeated until the nodal velocities for each harmonic have been specified. (IF IQN = 0, OMIT CARDS**

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VII-B.)

Card Type VII-B Format (2I5, 4F10.0)

Columns	Variable	Description
1-5	IN1	First node to which the velocities specified on this card are applied.
6-10	IN2	Last node to which the velocities specified on this card are applied.
11-20	\dot{q}_1	Initial nodal velocity in the axial direction for a particular harmonic.
21-30	\dot{q}_2	Initial nodal velocity in the circumferential direction for a particular harmonic.
31-40	\dot{q}_3	Initial nodal velocity in the radial direction for a particular harmonic.
41-50	\dot{q}_4	Initial nodal rotational velocity in the meridional direction for a particular harmonic.

- C. Initial Displacements - In identically the same manner as is utilized for the initial velocities, the initial displacements are

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specified for each harmonic. (IF IQN1 = 0, OMIT CARDS VII-C)

Card Type VII-C Format (2I5, 4F10.0)		
Columns	Variable	Description
1-5	IN1	First node to which the displacements specified on this card are applied.
6-10	IN2	Last node to which the displacements specified on this card are applied.
11-20	q 1	Initial nodal displacement in the axial direction for a particular harmonic.
21-30	q 2	Initial nodal displacement in the circumferential direction for a particular harmonic.
31-40	q 3	Initial nodal displacement in the radial direction for a particular harmonic.
41-50	q 4	Initial nodal rotation in the meridional direction for a particular harmonic.

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VIII. COEFFICIENTS OF THERMAL EXPANSION

If the thermal effects are to be included in the analysis, the coefficients of thermal expansion must be specified using these cards. These coefficients are assumed to be constant for a given element but may vary from element to element. These coefficients are read in the same manner as the element properties in the SAMMSOR code. (THE NUMBER OF CARDS VIII MUST BE ≤ NELEMS FOR ANY GIVEN DATA SET. IF ITELF = 0, OMIT CARDS VIII.)

Card Type VIII Format (2I5, 2F10.0)

Columns	Variable	Description
1-5	IELM1	Number of the first element to which the properties on this card apply.
6-10	IELM2	Number of the last element to which the properties on this card apply.
11-20	ALSI1	Coefficient of thermal expansion in the meridional direction (in/in/deg).
21-30	ALTI1	Coefficient of thermal expansion in the circumferential direction (in/in/deg).

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IX. APPLIED LOADS, TEMPERATURES, AND TEMPERATURE GRADIENTS

Since the concentrated nodal loads, distributed pressures, temperatures, and temperature gradients may vary in time; it may be necessary to specify these loads at a number of points in time. If these loads and temperatures are input at times T_{1j} and T_{1j+1} , the program will calculate generalized forces due to these loads at each of the input times. A linear variation of the generalized forces is then assumed between the times the loads are input. As soon as the value of the time reaches T_{1j+1} , a new set of loads is read in at T_{1j+2} and the process of calculating the generalized forces is repeated. The time increment, DELTE (CARD III-A), used in the solution of the equations of motion must be less than the difference between any two of the times at which the loads are specified. If the loads and/or temperatures propagate in and direction (moving loads), it is advisable to specify the loads at more times than is necessary if they vary in intensity only.

Ring loads can be applied at the nodes and must be input for each of the harmonics. The ring loads utilize the same sign convention employed for the shell nodal displacements.

The pressure loadings, temperatures and temperature gradients are assumed constant over the meridional length of the element but variations in the circumferential direction are allowed. These loadings may be input in one of two ways. Either the Fourier coefficients can be specified for each harmonic or the values of the loads may be specified at a number of circumferential angles around the shell elements. Utilizing this second procedure a step function variation is assumed in the circumferential direction. That is, the load is assumed constant from O_j to O_{j+1} with the value of the loads being equal to those specified at O_j . Sign conventions for the pressure loading are given in Figure 2.

A control card (Card Type IX-A) containing several key variables is used to guide the reading of the loading conditions. Proper selection of the values of these key variables results in a highly efficient procedure for specifying a wide variety of loading conditions. The key words and their meanings are explained in Figure 3.

Before attempting to input loads to the code the user is advised to study the guidelines presented in Section II, the example problems of Section II, and Appendix 6 which presents a thorough discussion of the various procedures necessary for specifying the loads.

A. Load Control Card

This control card is utilized to direct the input of the loads for a given time. This card indicates the presence or absence of concentrated

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forces and distributed pressure loadings and indicates the procedure to be utilized for creating the generalized thermal forces. (ONE CARD IX-A IS NECESSARY FOR EACH TIME AT WHICH THE LOADS ARE BEING INPUT.)

Card Type IX-A Format (F10.0, 4I5, A8)		
Columns	Variable	Description
1-10	T1	The time for which the loads are being input (sec).
11-15	NCF	If concentrated ring loads are applied to the structure at time T1, set NCF = 1. If not, set NCF = 0.
16-20	IDELF	If distributed loads are to be applied to the shell at time T1, set IDELF = 1. If not, set IDELF = 0.
21-25	IDCOE	If the Fourier cosine coefficients for the distributed loadings are to be read in at time T1, set IDCOE = 1. If not, set IDCOE = 0.
26-30	ITCOE	If the Fourier cosine coefficients for the temperatures and temperature gradients are to be read in at time T1, set ITCOE = 1. If not, set ITCOE = 0.
31-38	CONSTF	If the applied loads, temperatures and temperature gradients are constant from time, T1, to the final time, TOTIME (CARD III-A), punch the word CONSTANT in columns 31-38. If these parameters are not constant, leave columns 31-38 blank.

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B. Concentrated Ring Loads

The concentrated ring loads must be specified for each harmonic. (IF NCF = 0, OMIT CARDS IX-B.)

1. Control Card - This card indicates the presence or absence of concentrated ring loads for a particular harmonic. (ONE CARD IX-B-1 FOR EACH HARMONIC.)

Card Type IX-B-1 Format (I5)		
Columns	Variable	Description
1-5	NCF1	If there are concentrated ring loads for this particular harmonic, set NCF1 = 1. If not, set NCF1 = 0.
.....		

1-5 NCF1 If there are concentrated ring loads for this particular harmonic, set NCF1 = 1. If not, set NCF1 = 0.

.....

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2. Concentrated Ring Loads - For harmonics having ring loads associated with them, the loads are specified using these cards. (IF NCP1 = 0, OMIT CARDS IX-B-2 FOR THE HARMONIC BEING CONSIDERED.) ONE OR MORE CARDS IX-B-2 MAY BE USED, BUT NEVER UTILIZE MORE THAN 51 PER HARMONIC.

Card Type IX-B-2 Format (2I5, 4F10.0)

Columns	Variable	Description
1-5	IN1	First node to which this loading applies.
6-10	IN2	Last node to which this loading applies.
11-20	F1	Axial ring load applied at a node (lb).*
21-30	F2	Circumferential ring load applied at a node (lb).*
31-40	F3	Radial ring load applied at a node (lb).*
41-50	F4	Concentrated moment applied at a node (in-lb).*

Examples: The use of cards IX-B should become clear after considering the following examples:

1. Consider the case where a uniform tensile ring loading of 100 psi is being applied in the axial direction to the first node of a cylinder. The solution for this problem has been presented in Figure 20 of Reference 31. The thickness of the cylinder is 0.1

* The total value of the ring load for each harmonic is input, not the load per unit length of circumference. For complicated ring loads the value of the load input for each harmonic is obtained by integrating the product of the load and the corresponding displacement function around the circumference.

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inches with the radius being given as 6 inches. Consider that harmonics 0 and 2 are being run. The total ring load for the zero harmonic will be $(100) \times 2\pi(6) \times (0.1) = 376.9$ lb.

Five cards of type IX are required to input these loads assuming they are constant from time $T1 = 0.0$ to $TOTIME$ and assuming 50 elements are used to idealize the structure.

CARD	VARIABLE	VALUES
IX-A	$T1 = 0.0$	$NCF = 1$ $IDELF = IDCOE = ITCOE = 0$
IX-B	$NCF1 = 1$	(HARMONIC 0)
IX-C	$IN1=1 IN1=1$	$F1 = -376.9 F2 = F3 = F4 = 0$
IX-C	$IN1 = 2 IN1 = 51$	$F1 = F2 = F3 = F4 = 0$
IX-B	$NCF2 = 0$	(HARMONIC 2)

2. The second example considers a radial ring load of $F \cos\theta$ applied to a cylinder of radius r .

Performing the integration, one obtains the radial ring load for harmonic 1 as

$$F3 = \int_0^{2\pi} (F \cos\theta) r \cos\theta d\theta \\ = \pi r F$$

The Fourier coefficients for the other harmonics are zero.

C. Distributed Loads - (IF IDELF = 0, OMIT CARDS IX-C)

The distributed loadings may be input in one of two ways: the Fourier coefficients may be read in for each harmonic or the loadings may be specified at a desired number of circumferential angles (≤ 37). If the second option is used, the Fourier coefficients will then be generated internally. The user should note that it is possible to input distributed loads in only one of two ways.

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1. Distributed Loads - (Input at various circumferential angles)
Since the choice of the displacement functions utilized in this analysis necessitate the presence of loads symmetric about the meridian $\theta = 0$, it is necessary to specify the distributed loadings for angles from $0^\circ \rightarrow 180^\circ$. The code then assumes that the distribution from $180^\circ \rightarrow 360^\circ$ is the mirror image of the input distribution. (IF IDCQE = 1, OMIT CARDS IX-C-1)
- a. Control Card - Utilize this card to indicate the number of angles for which the loads will be specified.

Card Type IX-C-1-a Format (3I5)		
Columns	Variable	Description
1-5	IELM1	First element to be distributed loading applies.
6-10	IELM2	Last element to which this distributed loading applies.
11-15	NDP	Number of circumferential angles at which the distributed loads are to be specified ($1 \leq NDP \leq 37$). If the loadings are constant in the circumferential direction set NDP = 1.

- b. Distributed Loads at Specified Angles* This card specifies the angle at which the loads are being input and provides the values of the loads at that angle. (INCLUDE NDP CARDS OF

* The first loading must always be given for $\theta = 0^\circ$. The next loading is given at the angle where the load changes in value. If the load is constant with respect to θ , only one card will be necessary to input the load. Do not input values for the loads at $\theta = 180^\circ$ since the load at that angle will be equal in all cases to the load input at the previous value of THETAB.

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TYPE IX-C-1-b FOR EACH CARD IX-C-1-a.)

Card Type IX-C-1-b Format (4F10.0)		
Columns	Variable	Description
1-10	THETB	Circumferential angle (degrees) for which this data is given.
11-20	P	Distributed load in the meridional direction (psi).
21-30	R	Distributed load in the normal direction (psi).
31-40	S	Distributed load in the circumferential direction (psi).

Example: Consider the normal pressure distribution on an element depicted in Figure 4. To input the pressure on this element requires specification of the pressures for four values of θ .

THETB	R(I)
0.0	-Q1
30.0	-Q2
90.0	-Q3
2.0	0.0

2. Distributed Loads - (Fourier Coefficients) The Fourier coefficients for the distributed loads may be specified using these cards. The coefficients must be specified (even though they may be zero) for each harmonic being employed in the analysis. The coefficients are specified for each harmonic of the first group of elements, then for each harmonic of the second group, etc. until the values have been input for all the elements. (IF IDCOE = 0, OMIT CARDS IX-C-2)

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a. Control Card

Card Type IX-C-2-a Format (2I5)

Columns	Variable	Description
1-5	IELM1	First element to which these loads apply.
6-10	IELM2	Last element to which these loads apply.

b. Fourier Coefficients - (NH CARDS OF TYPE IX-C-2-b FOR EACH CARD IX-C-2-a.)

Card Type IX-C-2-b Format (3F10.0)

Columns	Variable	Description
1-10	P	Fourier coefficient of the distributed load in the meridional direction for a particular harmonic (psi).
11-20	R	Fourier coefficient of the distributed load in the normal direction for a particular harmonic (psi).
21-30	S	Fourier coefficient of the distributed load in the circumferential direction for a parti- cular harmonic (psi).

D. Temperature Distribution and Gradients

Essentially the same logic is employed for inputting the temperatures and gradients that was used for the specification of the distributed loads. The explanation of this procedure should therefore not need be repeated.

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The temperatures are specified for the midsurface of the shell. The temperature gradients (through the thickness) are considered positive if the temperature for the outer surface is greater than the temperature on the inner surface. (IF ITEL = 0, OMIT CARDS IX-D.)

1. Temperature Distribution and Gradients - (Input at various circumferential angles)

Again, the requirement of symmetry about the meridian $\theta = 0$, makes it necessary to specify the temperature distribution and thermal gradients only from $0^\circ \rightarrow 180^\circ$. The temperature distribution and gradients are input on the same cards for the various angles. (IF ITGDE = 1, OMIT CARDS IX-D-1.)

- a. Control Card - Utilize this card to indicate the number of angles for which the temperature and gradients will be specified.

Card Type IX-D-1-a Format (3I5)		
Columns	Variable	Description
1-5	IELM1	First element to which this data applies.
6-10	IELM2	Last element to which this data applies.
11-15	NDP	Number of circumferential angles at which the temperature distribution and gradient are to BE SPECIFIED ($1 \leq NDP \leq 37$). If the temperature is constant in the circumferential direction, set NDP = 1.

b. Temperature and Temperature Gradient at Specified Angles -

This card specifies the angle at which the temperature and temperature gradient (through the thickness) is being input and provides the value of the temperature at that angle. (INCLUDE NDP CARDS OF TYPE IX-D-1b)

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FOR EACH CARD IX-D-1-a.)

Card Type IX-D-1-b Format (3F10.0)		
Columns	Variable	Description
1-10	THETB	Circumferential angle for which this temperature and gradient are given.
11-20	P	Distributed temperature at $\theta = \text{THETB}$ ($^{\circ}\text{F}$).
21-30	R	Temperature gradient (through the thickness) at $\theta = \text{THETB}$ ($^{\circ}\text{F/in}$).

2. Temperature Distribution and Gradient - (Fourier Coefficients)

If the user so desires, the Fourier coefficients for the temperature distribution and gradient may be specified for each of the harmonics being used. Again, the coefficients are specified for all harmonics for the first group of elements, then for the second group, etc., until all the element coefficients have been input. (IF ITCOE = 0, OMIT CARDS IX-D-2)

a. Control Card

Card Type IX-D-2-a Format (2I5)		
Columns	Variable	Description
1-5	IELM1	First element to which these properties apply.
6-10	IELM2	Last element to which these properties apply.

b. Fourier Coefficients - (NH CARDS OF TYPE IX-D-2-b FOR EACH

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CARD IX-D-2-a.)

Card Type IX-D-2-b Format (2P10.0)		
Columns	Variable	Description
1-10	TH1	Fourier coefficient of the temperature distribution ($^{\circ}$ F) for a particular harmonic.
11-20	DTH1	Fourier coefficient of the temperature gradient ($^{\circ}$ F/in) for a particular harmonic.

X. FINAL DATA CARD FOR A CASE

Place this card after the last card IX of each data set. This signifies the end of the input data for a case. (ONE CARD X PER DATA SET.)

Card Type X	
Columns	Punch
1-11	END OF CASE

XI. FINAL DATA CARD FOR A RUN

This card must be placed after the card X of the last case to be run.

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It denotes the end of the input data for a run. (ONE CARD XI PER RUN)

Card Type XI

Columns

Punch

1-10

END OF RUN

.....

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EXAMPLE PROBLEMS

The example problems which follow were chosen to demonstrate the versatility of the code and to further acquaint the users with the procedures for inputting the data to the code. The data presented herein is typical for the problems solved by the code and demonstrates many of the input procedures.

Since the most complex portion of the input data is the specification of the loading conditions, a variety of loadings are demonstrated. Response curves are presented so the user may check his output with the previously obtained curves. The first two example problems utilize the shells described in example problems 1 and 2 of the SAMMSOR user's guide (Ref. 1) while the third example problem demonstrates the two procedures for specifying distributed pressure loadings.

Example Problem 1

The first example problem was chosen to demonstrate the procedure for inputting a concentrated ring load and to demonstrate the program's capability to solve highly nonlinear problems. For the forty pound load applied in this problem, the static solution shows that the nonlinear displacement is more than four times as large as the linear solution.

The shell to which the load is applied is the shallow spherical cap ($\lambda=6$) utilized in the first example problem in the SAMMSOR user's guide. The edges of the shell are assumed to be clamped. Since the loading is symmetric, the displacements and stresses will be calculated only along the line $\theta = 0$. Only the response for the zeroth harmonic will be determined. A set of input data for this case is presented in Figure 5 with the displacement response of the apex of the shell being presented in Figure 6. This response curve should allow the user to check his version of the code.

Example Problem 2

The shell described in the second example problem in the SAMMSOR user's guide is now subjected to a 50 psi internal pressure. The load-in is applied at time $T_1 = 0.0$ and remains constant for the duration of the calculation.

Two sets of input data are provided for this example problem. The first set (Figure 7) allows the program to calculate the response for the first 300 time steps. The second set of input data (Figure 8) will

NCASE = 1

PRINTOUT OF INPUT DATA

CARD TYPE	10	20	30	40	50	60	70	80
	12345678901234567890123456789012345678901234567890123456789012345678901234567890							
II - A	6	4						
- B	*****							
- B	EXAMPLE PROBLEM NO. 1							
- B	DYNASOR II USER'S MANUAL							
- B	THE SHELL DESCRIBED IN EXAMPLE PROBLEM 1 OF THE SAMMSOR USER'S GUIDE							
- B	IS SUBJECTED TO A 40 LB. APEX LOADING WITH THE SOLUTION BEING DETERMINED							
- B	FOR 400 TIME STEPS							
- B	*****							
III - A	0.0001	.00000025	0	0	1	0		
- B	1	4	1	8	1	100	1	0
IV - A	1							
- B	0.0							
V	1	0						
VI - A	4							
- B	31	1						
- B	31	2						
- B	31	3						
- B	31	4						
VII - A	0	0						
IX - A	0.0	1	0	0	OCONSTANT			
- B	1	1						
- 2	1	1	40.0	0.0	0.0	0.0		
- 2	2	31	0.0	0.0	0.0	0.0		
X	END OF CASE							

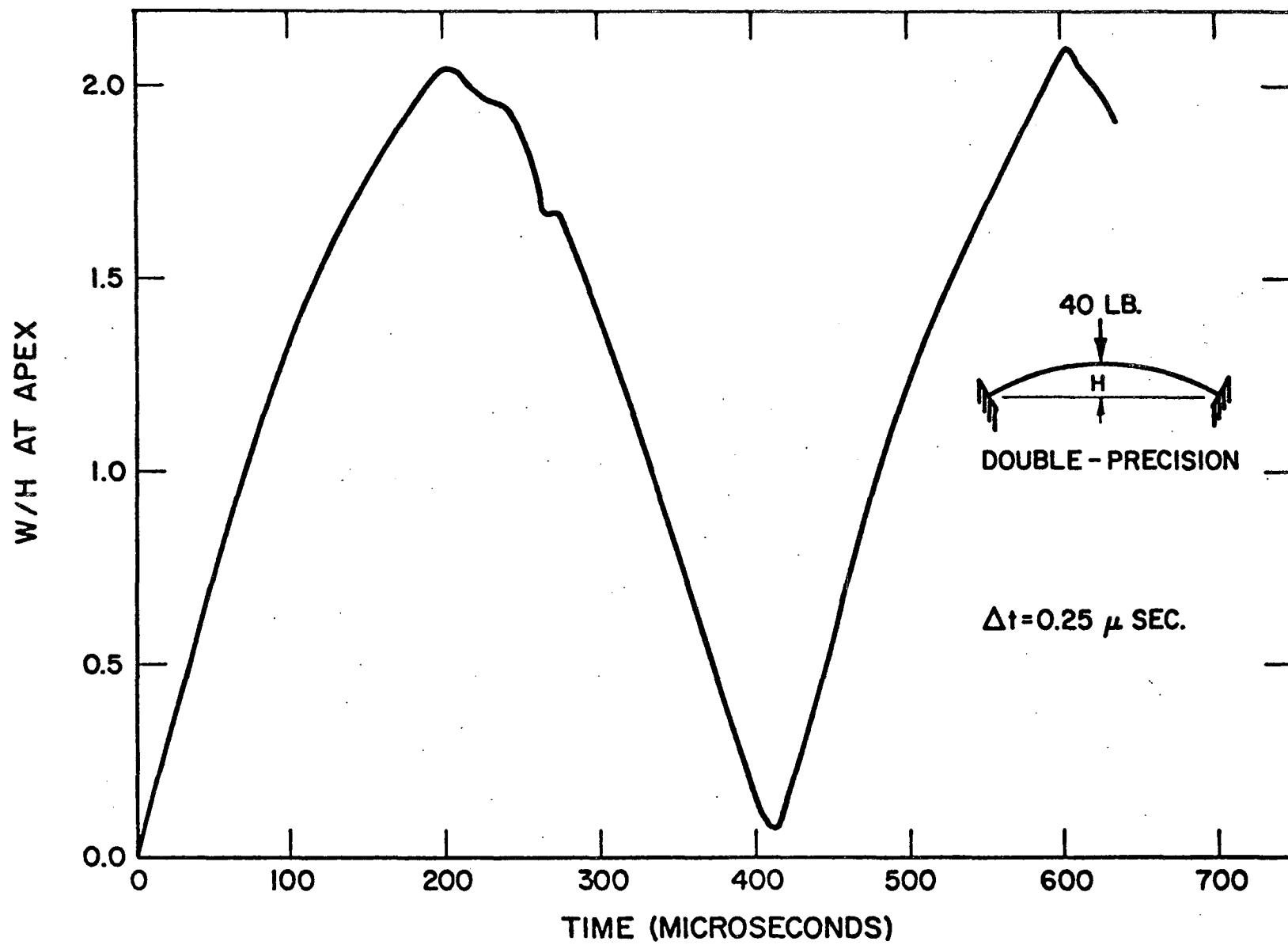


FIG. 6 APEX DISPLACEMENT RESPONSE UNDER CONCENTRATED AXIAL LOAD

NCASE = 2

PRINTOUT OF INPUT DATA

CARD	10	20	30	40	50	60	70	80
TYPE	12345678901234567890123456789012345678901234567890123456789012345678901234567890							
II - A	6	8						
- B	***** EXAMPLE PROBLEM NO. 2 *****							
- B	DYNASOR II USER'S MANUAL							
- B	CAP-TORUS-CYLINDER CONFIGURATION							
- B	THE SHELL DEPICTED IN THE SECOND EXAMPLE PROBLEM OF THE SAMMOSR USER'S							
- B	MANUAL IS SUBJECTED TO A 50 PSI INTERNAL PRESSURE							
- B	*****							
III - A	0.0009	0.000003	0	0	1	0		
- B	1	10	1	20	1	100	1	0
IV - A	1							
- B	0.0							
V - A	1	0						
VI - A	4							
- B	51	1						
- B	51	2						
- B	51	3						
- B	51	4						
VII - A	0	0						
IX - A	0.0	0	1	0	OCONSTANT			
- C -1-a	1	50	1					
- b	0.0		0.0	50.0	0.0			
X	END OF CASE							

Fig. 7 INPUT DATA - EXAMPLE PROBLEM 2

Fig. 8 INPUT DATA - EXAMPLE PROBLEM 2 - RESTART MODE

NCASE= 3

PRINTOUT OF INPUT DATA

CARD TYPE	10	20	30	40	50	60	70	80
	12345678901234567890123456789012345678901234567890123456789012345678901234567890							
II - A	6	8						
- B	*****							
- B	EXAMPLE PROBLEM NO. 2 DYNASOR II USER'S MANUAL							
- B	THE INPUT DATA NECESSARY TO RESTART THE CODE AT TIME INCREMENT 300							
- B	IS PROVIDED TO GUIDE THE USER IN HIS RESTART OPERATIONS. THE PROBLEM							
- B	IS TO BE RUN FOR AN ADDITIONAL 300 TIME INCREMENTS.							
- B	*****							
III - A	0.0018	0.000003	1	300	1	0		
- B	1	10	1	20	1	100	1	0
IV - A	1							
- B	0.0							
IX - A	0.0009	0	1	0	OCONSTANT			
- C - 1 -a ¹	50	1						
- b	0.0	0.0	50.0	0.0				
X	END OF CASE							

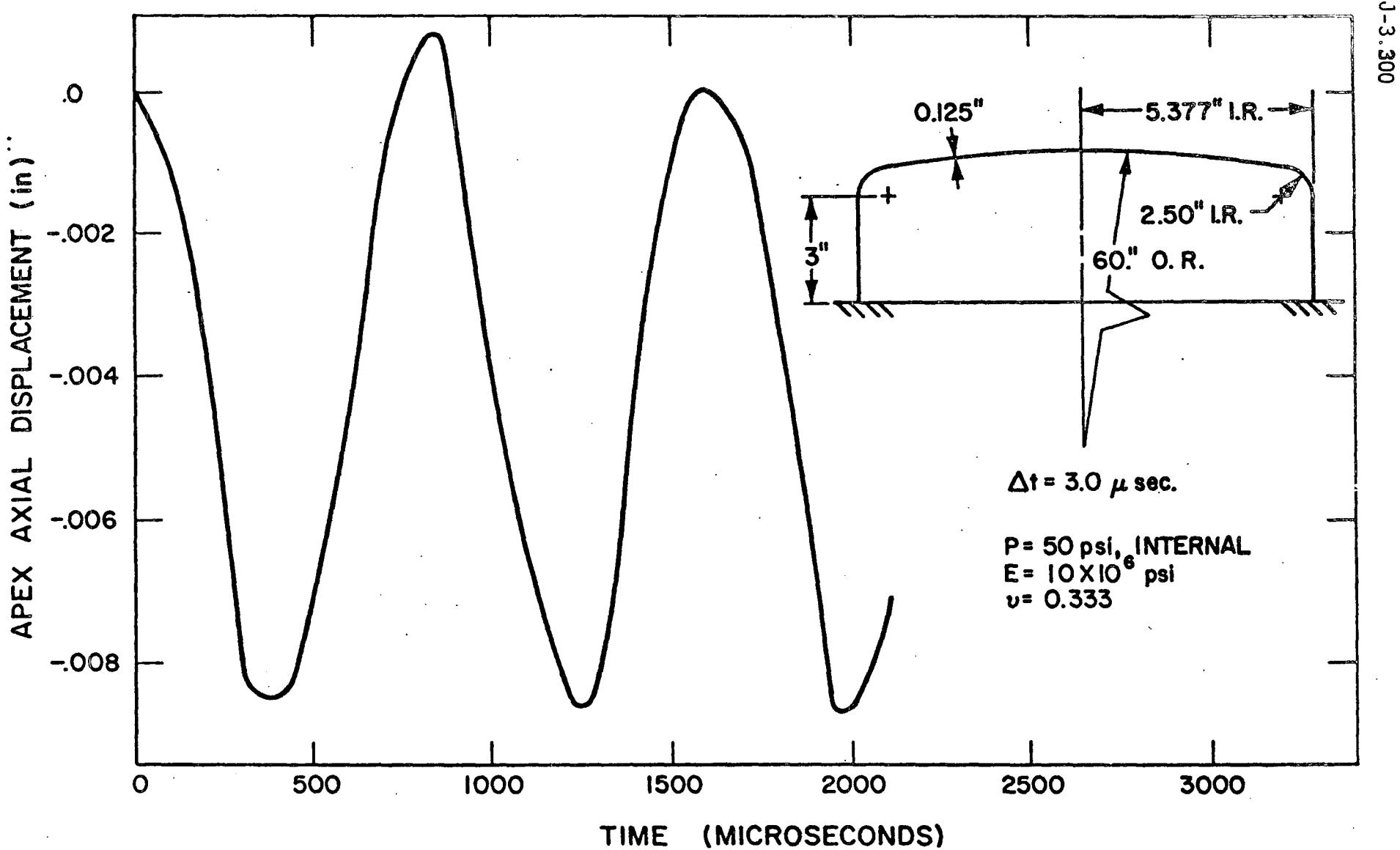


FIG. 9 DISPLACEMENT RESPONSE UNDER INTERNAL PRESSURE

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restart the code at the end of the 300th time step and will then allow the program to calculate the response for an additional 300 increments.

Since this problem is only moderately nonlinear, it is interesting to note that a much larger time step can be used for this problem than was employed in the previous example problem. The displacement response obtained for this problem is presented in Figure 9.

Example Problem 3

This example problem was selected to demonstrate the procedures for inputting the distributed loadings on a shell. A cylindrical shell (figure 10) is subjected to a half cosine loading which is symmetric about the meridian = 0. This load is applied along the entire length of the shell. The pressure loading may be specified in one of two ways:

- 1) The Fourier coefficients may be input for each harmonic.
- 2) The pressure may be specified at various circumferential angles with the Fourier coefficients then being internally generated.

The first set of input data (Figure 11) utilizes the first of the above procedures and inputs the Fourier coefficients. The input data presented in Figure 12 describes the loading by specifying the value of the pressure at the various angles. The same procedure is employed to describe the temperature and temperature gradient distributions.

Considering the symmetry of the loading and the boundary conditions applied to this shell, it can easily be recognized that the displacements and stresses will be symmetric about the center of this cylindrical tube. Therefore, only one-half of the shell needs to be analyzed. The plane of symmetry is assured by applying an axial and a rotational restraint at node one (1).

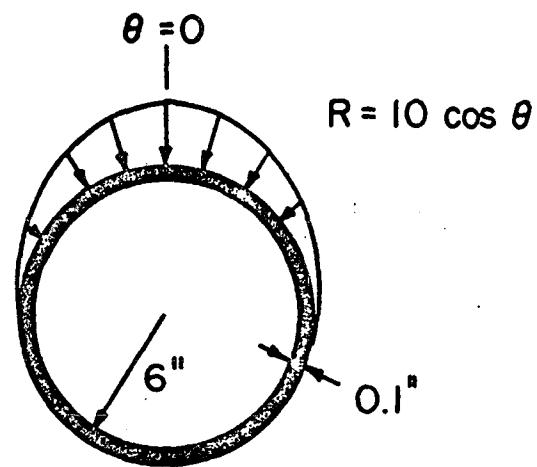
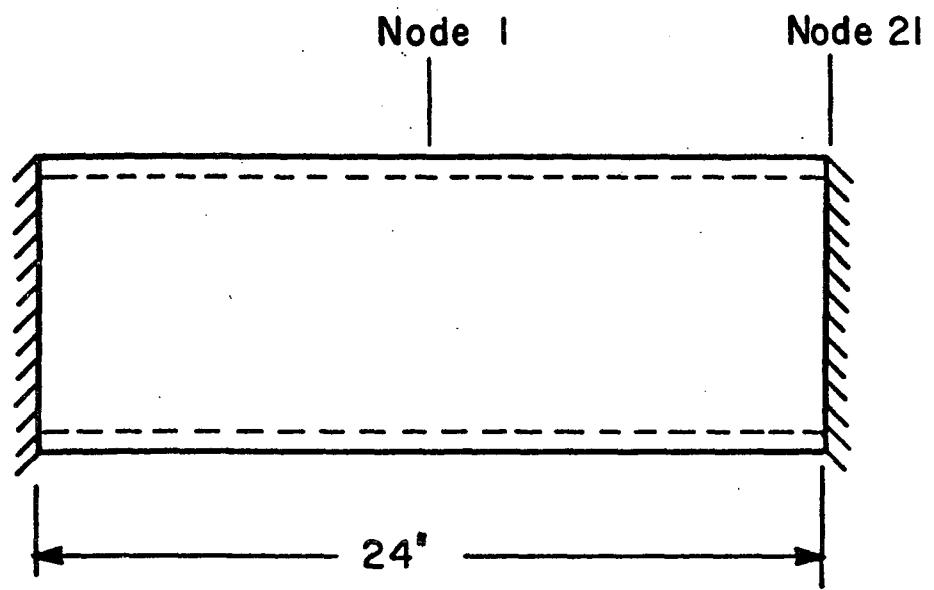


FIG 10 CYLINDRICAL SHELL SUBJECTED TO HALF COSINE PRESSURE LOADING

NCASE= 5

PRINTOUT OF INPUT DATA

CARD TYPE	10	20	30	40	50	60	70	80
	12345678901234567890123456789012345678901234567890123456789012345678901234567890							
II - A	6	4						
- B	*****							
- B	EXAMPLE PROBLEM NO. 3							
- B	DYNASOR II USER'S MANUAL							
- B	CYLINDRICAL SHELL IDEALIZED USING 30 ELEMENTS IS SUBJECTED TO A HALF COSINE							
- B	LOADING TO DEMONSTRATE THE OPTIONS FOR INPUTTING DISTRIBUTED LOADS.							
- B	** IN THIS CASE THE PRESSURE IS SPECIFIED BY INPUTTING THE FOURIER COEFFICIENTS							
- B	*****							
III - A	0.0005	0.00001	0	0	0	0		
- B	1	5	1	10	1	50	1	1
IV - A	2							
- B	0.0	30.0						
V	5	0	1	2	3	4		
VI - A	6							
- B	1	1						
- B	1	4						
- B	21	1						
- B	21	2						
- B	21	3						
- B	21	4						
VII - A	0	0						
IX - A	0.0	0	1	1	OCONSTANT			
- C - 2- a ¹	20							
- b	0.0	-3.1831			0.0			
- b	0.0	-5.0000			0.0			
- b	0.0	-2.1221			0.0			
- b	0.0	0.0000			0.0			
- b	0.0	0.4244			0.0			
X	END OF CASE							

Fig. 11 INPUT DATA - (SET #1) - EXAMPLE PROBLEM 3

J-3.304
NCASE = 4

PRINTOUT OF INPUT DATA

Fig. 12 INPUT DATA - (SET #2) - EXAMPLE PROBLEM 3

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Use of the Restart Option

In order for efficient use to be made of the DYNASOR II code, the user should become familiar with the option provided for restarting the program. Through effective use of this option the dynamic response studies can be completed using a minimum amount of computer time.

Use of the restart option may prove invaluable in a number of situations. Abnormal termination of the program may occur if a numerical instability is noted in the response. If this occurs, the restart option can be used with a different value of the time increment. Another important use of the restart option arises when the user is satisfied with the results previously obtained but desires to extend the response data to a further point in time. In such a case the program is restarted at the last time step for which the restart information was placed on tape. A most effective use of this option can be made when conducting dynamic stability analyses where it is desirable to evaluate the response to see if buckling has occurred. If it has not, the decision can then be made to extend the run to further points in time.

Utilizing large time steps can result in a damping effect upon the solution so it is advisable to run the problem for a couple of oscillations, check to see if the solution is significantly damped, and then run the problem for the desired number of oscillations. If an evaluation of the initial results indicates that a smaller or larger time step should be used, the restart facility might be used to keep from having to repeat the initial calculations.

The displacements, velocities, and forces should be written on tape for almost all of the cases to insure that the restart information will be available if an evaluation of the calculated response indicates that the program should be restarted. The time required to write the restart information on tape is negligible when compared with the amount of time required to obtain the total response.

If it is desirable to decrease the time increment when restarting the program, the user should exercise care in selection the increment (INRST) at which the program will be restarted. The decision to decrease the size of the time step will usually be based upon the observation that the solution has become unstable or that significant damping is present in the response. To restart the program the user must be sure that the increment (INCRST) has been selected small enough to insure that the inaccuracies created by the larger time step can be neglected.

On the other hand, if the results from a previous run indicate that it is possible to increase the size of the time step for the remaining calculations, then care must also be taken in the selection of INCRST. For the numerical extrapolation procedure to produce accurate sets of displacements, it is recommended that the solution be restarted on a

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relatively straight portion of the displacement response curve. Considering the curve presented in Figure 6, it would be recommended that the program be restarted at 500 microseconds rather than at 600 microseconds because of the extrapolation procedure being utilized (i.e. the curve is smoother at 500 microseconds).

When using the restart option, it is possible to specify different values for a number of the control constants and input parameters. The data on cards I-IV may be changed, but the same Fourier harmonics and boundary conditions must be used. It is also required that the coefficients of thermal expansion remain the same when restarting the program. These requirements allow the user to omit card types V, VI, and VII when preparing data for restart operations. The considerations effecting the input of the loads for restart operations are presented in Appendix 6.